

DOCTOR OF PHILOSOPHY

Catalytic intermediate pyrolysis of Brunei
rice husk for bio-oil production

Muhammad Abu Bakar

2013

Aston University

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CATALYTIC INTERMEDIATE PYROLYSIS OF BRUNEI RICE HUSK FOR BIO-OIL PRODUCTION

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SEPTEMBER 2013

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Thesis Summary

Rice husks from Brunei were subjected via intermediate pyrolysis for bio-oil production. Two main objectives were set out for this study. The application of intermediate pyrolysis on Brunei rice husk for the production of bio-oil is the main objective of this experiment. Characterisation of the rice husks was inclusive as a pre-requisite step to assess the suitability as feedstock for production of liquid fuels. Following on from the characterisation results, a temperature of 450 °C was established as the optimum temperature for the production of bio-oil. A homogenous bio-oil was obtained from the pyrolysis of dry rice husk, and the physicochemical properties and chemical compositions were analysed.

The second objective is the introduction of catalysts into the pyrolysis process which aims to improve the bio-oil quality, and maximise the desired liquid bio-oil properties. The incorporation of the catalysts was done via a fixed tube reactor into the pyrolysis system. Ceramic monoliths were used as the catalyst support, with montmorillonite clay as a binder to attach the catalysts onto the catalyst support. ZSM-5, Al-MCM-41, Al-MSU-F and Brunei rice husk ash (BRHA) together with its combination were adopted as catalysts. Proposed criteria dictated the selection of the best catalysts, subsequently leading to the optimisation process for bio-oil production. ZSM-5/Al-MCM-41 proved the most desirable catalyst, which increases the production of aromatics and phenols, decreased the organic acids and improved the physicochemical properties such as the pH, viscosity, density and H:C molar ratios. Variation in the ratio and positioning of both catalysts were the significant key factor for the catalyst optimisation study.

Keywords: Brunei rice husk, Intermediate pyrolysis, Bio-oil, Zeolites, Catalyst optimisation

“In the name of Allah,
The Most Beneficent, the Most Merciful,
All the praises and thanks be to Allah, the Lord of all creation,
The Most Beneficent, the Most Merciful,
The only owner and the only ruling judge of the day of recompense,
You alone we worship, and You alone we ask for help,
Guide us to the straight way, the way of those on whom You have bestowed Your grace,
Not the way of those who have earned Your anger, nor of those who went astray.”

- The Holy Quran (1:1-7)

“Verily, We have given you a manifest victory,
That Allah may forgive you your sins of the past and the future, and complete His favour on
you, and guide you on the straight path,
And that Allah may aid you with a mighty victory.”

- The Holy Quran (48:1-3)

TO MY BELOVED FAMILY AND FRIENDS

Acknowledgements

I would like to address my sincerest gratitude to Dr. James Titiloye for the endless moral encouragement and motivational support you have given me. Your thoughtful guidance during my journey along the completion of this thesis, and as a student will be remembered.

My dearest thanks also go to the Chemical Engineering and Applied Chemistry lecturers and staffs, and both European Bioenergy Research Institute (EBRI) and Bio-Energy Research Group (BERG) members. Under the guidance of leading scholars particularly Prof. Andreas Hornung and Prof. Anthony Bridgwater, I believe that EBRI will keep on growing and extend its reach towards a continuous breakthrough in the bioenergy field.

Financial support from the Brunei Government under the Ministry of Education is gratefully acknowledged.

Special thanks to Asad, Yang, Miloud, Zsuzsa, Janat, Nuch, Kat and the rest of the current and former colleagues in EBRI who have assisted me with the ups and downs of being a research student. Not forgetting my beloved family and friends, especially my mum and dad and those in Brunei for coping with my temporary absence from your daily lives.

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1 INTRODUCTION

1.1 Background

The conversion of biomass into fuels and chemicals is taking a centre stage for most economy with the ultimate aim of reducing dependence on fossil fuels and to increase the potential of energy sources. For the process to be sustainable there must be sufficient biomass available as feedstock in order to satisfy the demand of emerging bioenergy industries. Several biomass feedstocks have been utilised in the past ranging from agricultural wastes and residues to energy crops. Agricultural residues such as rice husks are abundant in rice growing countries. During the production of rice, rice husks are generated on site as a by-product in the milling factory. As rice is considered a staple food in most developing countries including Brunei, the by-products are available in large quantity to provide a source of alternative energy in the form of biofuel in addition to the current energy sector [1]. The aspiration for a renewable energy mix and economic diversification away from oil and gas will favour the encouragement of a new industry.

The production of biofuels from lignocellulosic materials can be achieved from biochemical or thermochemical routes. The thermochemical route can produce a wider range of liquid fuel compared to the biochemical route [2]. Thermochemical conversion of biomass is therefore rapidly becoming an alternative source for renewable energy and fuel production worldwide. The common factor amidst all biomass feedstock thermochemical processing is the quality of the biofuel produced and the need to upgrade the fuel to meet standard specifications for different applications.

Since this project is funded by the Brunei Government, the rice husks investigated were selected from Brunei, based on availability, potential utilisation and together with ease of access. This will be elaborated in the next few section of this chapter.

1.2 Motivations and limitations for biofuels in Brunei Darussalam

Brunei Darussalam aspires to excel in various national strategies towards the Vision 2035, whereby one of the economic strategies is to “create new employment for our people and expand business opportunities within Brunei Darussalam, through the promotion and investment, foreign and domestic, both in downstream industries as well as in economic clusters beyond the oil and gas industries” [3]. Although economic diversification efforts has been geared towards non-reliant on oil and gas industries, this has not been entirely successful over the last decade [4]. This however would be possible through expansion of the non-oil and gas industries, such as from the bioenergy industries.

Biomass feedstock in Brunei consists mainly of agricultural and forestry waste. The land area in Brunei may not be available for growing non-food or dedicated energy crops as feedstock, due to the competition from the agriculture industry and the conservation efforts towards protecting the natural forests.

Although Brunei has a small land area, it is trying to achieve its aim of food security in rice production by growing high yielding variety of rice species. A target has been implemented for the production of rice, which is to increase self-sufficiency from 3.12% in 2007 to 60% by 2015 [5]. With this boost, one can expect that the waste from the rice industry will significantly increase in the near future.

One of the sub-goals of the Energy Department at the Prime Minister’s office is to “ensure safe, secure, reliable and efficient supply and use of energy”. This upholds the need for power generation from renewable sources, which accounts for at least 10% or 50 MW from the total in the energy mix [6]. Energy sources in Brunei are well-established from the oil and gas industries, but they are finite and non-recoverable. A study by a national think-tank, Centre for Strategic and Policy Studies in 2010 revealed that with the current production rate, Brunei has only 17 years and 30 years supply of crude oil and natural gas respectively [7]. Therefore, more efforts are being applied to diversify the economy and energy away from the fossil fuel industries.

1.3 Current and potential projects for alternative energy or waste utilisation

The realisation of the renewable energy mix has been studied and currently being proposed for further implementation. At present, the only major alternative energy project at pilot or industrial scale is a solar power feasibility study plant which aims to generate 1.2MW of nominal output capacity [8] . A potential waste-to-energy facility is also being proposed to generate 16-24 MW from landfill waste which will account to about 5-6% of the energy mix [9].

By coupling the aims and goals from different ministries and departments, the rice industry has a potential to generate a portion of renewable energy mix for Brunei. A study by Malik, referred to biomass as the second most potential alternative energy source in Brunei after solar energy [10].

To present date, the utilisation of biomass from lignocellulosic feedstock has not been done at a pilot or industrial scale. A central rice milling factory is currently being installed at Wasan rice mill centre in Brunei which will replace a 1 tonne/hour with a 3.5 tonnes/hour of milled-rice production [11]. This will in effect more than triple the generation of waste rice husk from the milling process. The idea of a bio-oil production on-site at a central rice milling factory sounds promising, as it will reduce the cost of collection and transporting the waste feedstock [12]. The concept of a biorefinery, which integrates biomass conversion processes and equipment to produce fuel, power and value-added chemicals from biomass [13] is therefore an attractive option for Brunei.

1.4 Brunei Rice Husk

Rice is one of the most important foods of the world, and is grown in over 100 countries. An average lifespan of a rice plant is around 3 to 7 months depending on the climate and variety. A modern variety matures up to 110 days, therefore can be planted multiple times in the field [14]. Table 1-1 below shows the properties of some of the rice variety available in Brunei. Since the rice husk is very much dependent on the yield of rice grain, it will be important to understand the factors influencing the grain yield. Rice yield is significantly influenced by the weather conditions, cultural management and nutrient supply. Understanding their inter-relationships is a key to improvement in the rice yield.

Table 1-1. Properties of some of the local rice variety available in Brunei [15]

	High Yielding	Low Yielding
Variety	Laila (IR67406-6-3-2-3)	Pusu, Bario, Adan
Rice grain yield (t/ha)	5 - 6.8	1.5 - 2.5
Approximate rice husk yield (t/ha)	1 – 1.36	0.3 – 0.5

Rice husk from rice milling factory constitutes about 20% of the weight of the rice grains [16]. The chemical constituent are found to vary from sample to sample which may be due to the different geographical composition, type of paddy, climatic variation, soil chemistry and fertilisers used in the paddy growth [17]. Figure 1-1 shows the different parts of the rice grain.



Figure 1-1. Structure of a rice grain [18]

1.5 Research Objectives

There are two primary objectives to this project. The application of intermediate pyrolysis on Brunei Rice Husk for the production of bio-oil is the main objective of this experiment. Within the scope of the objective is to characterise the feedstock and the liquid bio-oil product generated.

Secondly, the introduction of catalysts into the pyrolysis process aims to improve the bio-oil quality, and maximise the desired liquid bio-oil properties. The reduction of unfavourable components and the increase in high-value chemicals are investigated. This aim is achieved by introducing an alternative way to the catalyst incorporation into the pyrolysis system, and the selection of the ‘best’ catalysts, leading to the optimisation of the process for bio-oil production.

1.6 Organisation of thesis

The remainder of the chapters besides this one are explained as follows.

Chapter 2 deals with the literature review for the biomass feedstock and the pyrolysis of biomass, particularly rice husks. Chapter 3 deals with the literature review for the catalytic pyrolysis of rice husk.

Chapter 4 discusses the characterisation methods of the biomass and bio-oil used in the thesis.

Chapter 5, 6, 7 and 8 are experimental results which include the analyses and discussions. Chapter 5 discusses the biomass characterisation results of Brunei rice husks. The experimental results from the pyrolysis of Brunei rice husks, together with the characterisation results of the bio-oil envelop chapter 6. Chapter 7 highlights the catalytic pyrolysis of Brunei rice husks with mainly zeolite catalysts. Chapter 8 focuses on the catalytic optimisation experiments, based on the 'best' catalyst mixture from the experimental results in chapter 7. Chapter 9 finishes with the conclusion and recommendation for the thesis.

2 BIOMASS AND PYROLYSIS OF BIOMASS

2.1 Biomass

Biomass can be defined as the bio-degradable fraction of products, wastes and residues from biological origin from agriculture or forestry and related industries [19]. Biomass from dedicated energy crops such as switchgrass, poplar, willow and rapeseed, are defined as plants grown specifically for applications other than for food or feed [20].

2.2 Biomass chemical composition

Biomass consists of mainly cellulose, hemicellulose and lignin as its core components. Other components are made up of organic extractives, inorganic matter and water. Figure 2-1 shows the structure of lignocellulosic biomass with a representation of cellulose, hemicellulose and lignin components.

2.2.1 Cellulose

Cellulose is a natural polymer represented by the formula $(C_6H_{10}O_5)_n$ which consists of thousands of glucose molecules. It is a long chain polymer with a high degree of polymerisation ($\sim 10,000$) and a large molecular weight ($\sim 500,000$). It is highly crystalline, water insoluble and resistant to depolymerisation. Cellulose is the primary structural component of cell wall in biomass, and constitutes of approximately 50% of the cell wall material. Cotton is almost pure cellulose, ranging up to 90% by weight [21-24].

2.2.2 Hemicellulose

Hemicellulose, another component in the cell wall has a random, amorphous structure with little strength. They have a generic formula of $(C_5H_8O_4)_n$ and usually carry 50-200 monomeric units and a few simple sugar residues [21]. It is a branched polymer of glucose or xylose, substituted with arabinose, xylose, galactose, fucose, mannose, glucose or glucuronic acid. The amorphous nature of hemicellulose means that it is easily hydrolysed in dilute acid or base.

2.2.3 Lignin

Lignin is a complex, highly branched polymer of phenylpropanoid units and act as the cementing agent for cellulose fibers holding adjacent cells together. The three basic structural units of lignin includes hydroxyl phenyl (H-type), guaiacyl type (G-type) and syringyl (S-type) [25]. Lignin consists of It accounts for 18-25% in hardwood, 25-35% in softwood in dry weight, and 10-40% by weight in various herbaceous species, such as corncobs, rice husks and straws [21]. Lignin is highly insoluble, although the complex can be broken and lignin fraction separated by treatment in strong sulphuric acid [21, 26].



Figure 2-1. Structure of lignocellulosic biomass with cellulose, hemicellulose and lignin represented [27].

2.2.4 Organic Extractives

Organic extractives from the biomass include fats, waxes, alkaloids, proteins, phenolics, simple sugars, pectins, mucilages, gums, resins, terpenes, starches, glycosides, saponins and essential oils. These extractives can be extracted with polar solvents (such as water, methylene chloride, or alcohol) and non-polar solvents (such as toluene or hexane) [28].

2.2.5 Inorganic Matter

Biomass also contains mineral content that ends up in the pyrolysis ash [28]. The elemental constituents present in biomass are potassium (K), calcium (Ca), silicon (Si), sodium (Na), manganese (Mn), phosphorus (P), iron (Fe), magnesium (Mg), aluminium (Al), chromium (Cr) and zinc (Zn).

2.2.6 Water

There are two types of moisture in the biomass, namely bound and unbound water. Water that is adsorbed onto the hydroxyl groups of hemicellulose and cellulose molecules through hydrogen bond is referred to as bound water. Unbound water occupy the voids present within the biomass if the moisture content (including bound water) exceeds the fiber saturation point [29]. Other factors such as humidity and temperature have an effect on the biomass moisture. The hot and wet climate in Brunei would have a limited drying effect on varying the moisture content of the biomass.

2.3 Biomass pyrolysis

Pyrolysis is the degradation or decomposition of biomass under oxygen-free or inert conditions. Products evolved from pyrolysis are liquid bio-oil, solid char and non-condensable gases. Pyrolysis generally can be classified into three; slow, intermediate and fast pyrolysis. The difference between them depends on the vapour residence time, heating rates, temperatures and the yield of the evolved product [30]. Table 2-1 below shows the comparison between the different pyrolysis process and the product yields.

Table 2-1. Comparison between the different processes of pyrolysis and yield of products evolved [30]

Types of pyrolysis	Liquid (%)	Char (%)	Gas (%)
Fast pyrolysis Moderate temperature (~500 °C) Short hot vapour residence time (~2s)	75	12	13
Intermediate pyrolysis Moderate temperature (450-500 °C) Moderate hot vapour residence time (10-20s)	50	20	30
Slow pyrolysis Low moderate temperatures Long hot vapour residence time (300-1800s)	30	35	35

2.3.1 Fast Pyrolysis

Fast pyrolysis process gives high yields of bio-oil up to 80% by weight [31]. The fundamental features of fast pyrolysis is that it has a very high heating and transfer rates; controlled pyrolysis reaction temperature of around 500 °C with a short vapour residence time typically less than 2 seconds; and the rapid cooling of pyrolysis vapours to produce bio-oil. Different fast pyrolysis reactor configurations are available namely ablative, auger, circulating fluidised bed, entrained flow, fluidised bed, rotating cone, transported bed and vacuum moving bed reactor [28, 32-35]. The various reactors have their own advantages and drawbacks and are reviewed quite extensively in literatures. Fluidised beds are the most popular due to the ease of operation and readily scale-up [31].

2.3.2 Slow Pyrolysis

Slow pyrolysis is a conventional pyrolysis process whereby the heating rate is kept slow at approximately 0.1–1 °C s⁻¹. The vapour residence time varies from 5 to 30 min which allows the gas-phase products to continue to react with other products to form char [36]. Slow pyrolysis has been carried out in fixed beds, multiple hearths and rotary kiln reactors [37]. Due to the poor and slow heat transfer, low liquid yields were obtained. Slow pyrolysis gives an approximately equal yield of oils, char and gases.

2.3.3 Intermediate Pyrolysis

Intermediate pyrolysis is a relatively new technology working in contrast to the existing slow and fast pyrolysis techniques. The reaction temperature for this process is typically around 450-500 °C, with a vapour residence time of a few seconds. The solids residence time can be varied accordingly. The reaction occurs under controlled heating rates, therefore avoiding the tar formation. The feedstock can be in any form ranging from powders to chips. Example of intermediate pyrolysis is the HALOCLEAN® process from Karlsruhe and Turin [38] and the Pyroformer which was recently patented by Hornung and Apfelbacher at Aston University [39].

2.3.3.1 HALOCLEAN®

Originally the HALOCLEAN® process (Figure 2-2) has been developed for the pyrolysis of electronic scrap, but it can be used for organic materials such as biomass.

The principle underlying this process is the circulation of hot steel balls which can be fed into the rotary kiln, together with the biomass via a double flap sluice. The rotary kiln is electrically heated from the outside and the inside via the screw up to 600 °C. A homogenous temperature profile along the reactor is achieved by the intensive mixing process of the biomass and the steel balls in the first zone of the reactor. The solid biomass residence time is defined by the screw in the range of several minutes to hours. A side channel blower and a preset negative control the pyrolysis vapour generated and define the vapour residence time in the order of several seconds. A hot gas filtration system is placed after the reactor to clean it from char particles before passing it to a condensation system, where the pyrolysis liquid is collected. The remaining non-condensable gases and the pyrolysis liquid may be burnt for combined heat and power (CHP) in a special diesel engine [38].



Figure 2-2. Schematic setup of the HALOCLEAN® CHP plant [38]

2.3.3.2 Pyroformer

The pyroformer comprises of a twin co-axial rotating screw, where the inner screw conveys the feedstock passing through the reactor, and the outer screw transports the product char backwards for recycling through the reactor for further reaction and heat exchange. The pyroformer is designed to make full use of the contact time of the pyrolysis vapours and the bio-char for further cracking of the high molecular weight organic products.

The pyroformer is able to process a maximum of 20 kg/h. The reactor is purged with nitrogen and is heated up to a range of 300-450 °C depending on the type of feedstock supplied. The feedstock residence time is estimated to be at a range of 7-10 min, but the vapour residence time is around a few seconds. The pyrolysis vapour passes through the hot gas filter candles, which are also heated to 450°C. A cold water shell and tube condenser cools the vapours to form pyrolysis oil, while the non-condensable gases pass through an electrostatic precipitator to either be collected or flared. A schematic diagram of the pyroformer is illustrated in Figure 2-3.

The biomass feedstock that have been used on the pyroformer range from sewage sludge and waste paper sludge [40, 41] to brewer's spent grain [42]. The advantage of this “auger-type” reactor compared to a fluidised bed is that they use lower volumes of carrier gas and can obtain a sand free bio-char [43]. The pyroformer can achieve a sustainable biomass-to-energy concept - the biothermal valorisation of biomass (BtVB) process which offers a carbon negative system, and a closed loop multipurpose application in terms of fertilisers, CO₂, and heat production energy [44].

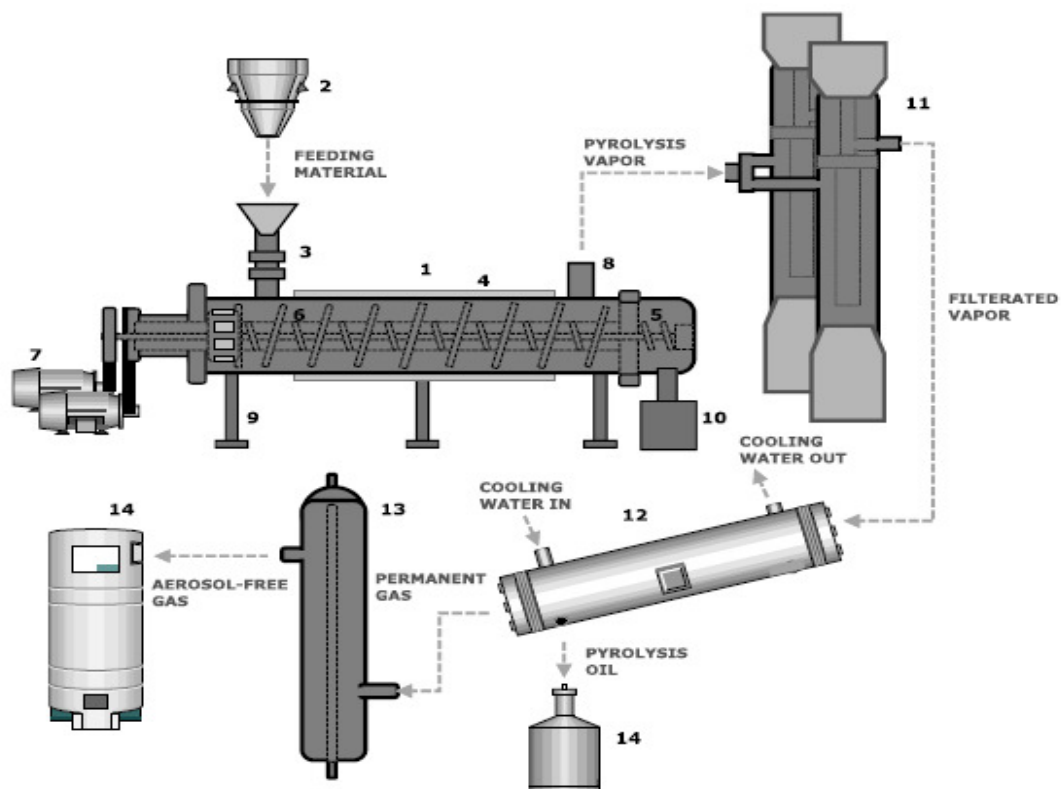


Figure 2-3. Schematic diagram of the pyroformer with the intermediate pyrolysis system [40]; (1) Insulation jacket (2) Biomass feed system (3) Feed entry pipe (4) External heaters (5) Internal screw (6) External screw (7) Electric motors (8) Heated vapour exit line (9) Support stand (10) Char pot (11) Hot ceramic filtration unit (12) Shell and tube condenser (13) Electrostatic precipitator (14) Pyrolysis oil collection pot (15) Gas flare unit

2.4 Factors affecting intermediate pyrolysis

2.4.1 Feedstock composition and preparation

Different biomass species will have varying composition of cellulose, hemicellulose and lignin therefore affecting the pyrolysis product composition. Unusual biomass such as sewage sludge may not have the same composition as biomass such as wood, husks and straw.

High ash content in biomass will lead to high char content, but will decrease the liquid organics yield in the product. Ash constituents such as K, Na and Ca acts as a catalyst for the decomposition process and favour char formation [45]. The removal of these metals via pretreatment may be useful to influence the pyrolysis reaction to produce chemical not normally contained in the pyrolysis yield, or to increase the yield of a selected chemical or groups of chemicals in the pyrolysis liquid [46].

The particle size of the biomass has an effect on the pyrolysis product yield. Shen et. al studied the effects of particle size on the fast pyrolysis oil mallee woody biomass and found that the increase in the average particle size of the biomass from 0.3 to 1.5 mm decreases the yield of the liquid bio-oil [47]. Jalan and Srivastava studied the kinetic and heat transfer effects on the pyrolysis of a single biomass cylindrical pellet and established that the relative importance of heat transfer and secondary reaction increases as the temperature and particle sizes are increased [48].

2.4.2 Moisture content

The moisture present in the biomass ends up as water in the pyrolysis liquid. Therefore, the moisture in the biomass should be low to reduce the water in the bio-oil, in addition to the formation of reaction water during pyrolysis. Westerhof et. al conducted a study on the effects of moisture content on the pyrolysis of pine wood in a fluidised bed reactor and concluded that an increase in the moisture content of the feedstock (between 0-20%), lead to the increase in the char and gas yield, and the decrease in reaction water formation [49]. Therefore drying the feedstock to low moisture content would increase the organic fraction in the pyrolysis liquid yield.

2.4.3 Pyrolysis temperature

As biomass contains mainly cellulose, hemicellulose and lignin as the major constituents, their degradation temperature is vital to ensure that the materials are sufficiently converted into the required products. Figure 2-4 shows a schematic overview of the different thermal stability regimes of each of the main biomass fractions [50]. Five different stages of degradation were shown; with hemicellulose, cellulose and lignin to degrade first and end in that order.



Figure 2-4. Thermal stability regimes for hemicellulose, lignin and cellulose [50]

Another study was also done by Yang et al. [51], which measured the pyrolysis degradation rate of the three major components of biomass. Figure 2-5 shows the mass loss and the mass loss rate of the individual components with a function of temperature. Hemicellulose showed a mass loss between 220-315°C, cellulose between 315-400°C, and lignin with a wide temperature range of 160-900°C.



Figure 2-5. Pyrolysis degradation curves of hemicellulose, cellulose and lignin in TGA [51]

Typically, pyrolysis of biomass is carried out at a low to moderate temperature of 300-500 °C. A further increase in temperature will lead to a secondary cracking of the pyrolysis vapours leading to a decrease the liquid organics and char yield and increase the gases yield [33]. Moreover, the increase in temperature from 400 °C to 550 °C results in higher polycyclic aromatic hydrocarbon (PAH) formation, which may be harmful to health [52].

2.4.4 Residence time

Residence time can be defined as the vapour or solid residence time. Vapour residence time is the time taken for the pyrolysis vapour to travel through the system prior to condensation. Solid residence time can be defined as the time taken for the solids to be fully converted in the reactor. Intermediate pyrolysis suggests that it has a moderate hot vapour residence time, more than ~2s (fast pyrolysis) but less than ~300s (slow pyrolysis). A longer vapour residence time results in the significant reduction of the organic yield from cracking reactions [32].

2.5 Pyrolysis products

2.5.1 Liquid bio-oil

Bio-oils are dark brown, free-flowing organic liquids that are highly oxygenated, viscous, corrosive, relatively unstable and chemically complex [53]. Pyrolysis liquids are formed by rapidly and simultaneously depolymerising and fragmenting cellulose, hemicellulose and lignin with a rapid increase in temperature [28]. The main components are 20-25% water, 5-10% organic acids, 5-10% non-polar hydrocarbons, 5-10% anhydrosugars such as levoglucosan, 25-30% pyrolytic lignin (comprising guaiacyl and syringyl based fragments from the original lignin polymer) and other oxygenated compounds such as aldehydes, ketones, phenols [54].

Liquid bio-oil contain two phases: an aqueous phase containing a wide variety of organo-oxygen compounds of low molecular weight and a non aqueous phase containing insoluble organics (mainly aromatics) of high molecular weight [54]. Ratio of acetic acid, methanol, and acetone of aqueous phase were higher than those of non-aqueous phase.

The chemical and physical properties of fast pyrolysis bio-oil adversely affect their combustion properties and result in difficulties in storage and handling [55]. The most critical properties in the fuel specifications proposed by IEA Pyrolysis project and EU-funded ALTENER II project include homogeneity, stability, heating value, pH, water, flash point, solids, ash, viscosity and lubricity [56, 57] .

2.5.2 Solid biochar

Char or bio-char is the solid residue of pyrolysed biomass. Char contributes to secondary cracking by catalysing secondary cracking in the vapour phase, to reduce the yield of bio-oil. It can also increase the viscosity of the bio-oil during storage; therefore an efficient removal of char is necessary to produce high-quality bio-oil [58]. Char contains elemental carbon, along with hydrogen, together with various inorganic species [59].

2.5.3 Non-condensable gases

Non-condensable gases that are analysed from pyrolysis are carbon monoxide (CO), carbon dioxide (CO₂), hydrogen (H₂), methane (CH₄), and other hydrocarbons such as ethene (C₂H₄), ethane (C₂H₆), propane (C₃H₈), propylene (C₃H₆), butane (C₄H₁₀), and butenes

(C₄H₈) [59]. The higher the reaction temperature leads to a high content of hydrocarbon gases, therefore giving a higher heating value to the product gases [58]. Addition of catalyst in the pyrolysis system also promotes the production of permanent gases [60].

2.6 Pyrolysis of biomass components

Pyrolysis studies on the components of biomass lead to an insight of the chemicals present in the bio-oil which may be traced from the major degradation products or intermediates of biomass. Alen et. al concluded in his study that the pyrolytic degradation of wood is dominated mainly from the behaviour of its main fractions namely cellulose, hemi-cellulose and lignin [61]. The pyrolysis of extractives was rarely mentioned, probably due to the lower % present in biomass, but was found to cause phase separation in bio-oils from extractive-rich wood [62]. Various mechanisms were proposed in literature for the three major biomass components, particularly for cellulose and lignin.

2.6.1 Cellulose degradation mechanism

There are various mechanism proposed from the degradation of cellulose. The pyrolysis of cellulose at a constant heating rate of 10 °C/min occurs in the 315-400 °C temperature zone [51]. Majority of the proposed mechanism quoted anhydrosugars, mainly levoglucosan as the major intermediate product. The proposed mechanism in Figure 2-6 shows that cellulose is depolymerised into activated cellulose. A low reaction temperature will lead to the formation of char, water and gases. A higher degradation temperature proceeds with two competitive reactions from the cracking of glucosidic bond and the ring opening and reforming reaction. The first reaction leads to the formation of levoglucosan and isomeric compounds, and simultaneously the formation of furfural, acetols, organic acids, aldehydes, ketones and heterocyclic compounds. The second reaction leads to the formation of gases such as CO, CO₂, CH₄ and H₂.



Figure 2-6. The global modified Broido-Shafizadeh model [63]

2.6.2 Hemicellulose degradation mechanism

The pyrolysis of hemicellulose at a constant heating rate of 10°C/min occurs in the 220-315°C temperature zone, which is lower than cellulose degradation temperature [51]. Patwardhan et. al studied the product distribution from the pyrolysis of hemicellulose, and suggested the mechanism in Figure 2-7 [64]. Primary products from hemicellulose degradation are thought to produce hydroxyacetaldehyde, formic acids, acetic acids, furfural and acetols.



Figure 2-7. Pyrolysis mechanism of hemicellulose [64]

2.6.3 Lignin degradation mechanism

Lignin, when pyrolysed at a constant heating rate of 10 °C/min shows a weight loss at a wide temperature zone of 160-900 °C, and generates a high solid residue content [51]. The degradation of lignin produces guaiacols and syringols as intermediate chemicals. Figure 2-8 shows the pathways of the intermediates in the formation of chemicals, gas and coke proposed by Asmadi et. al [65]. Chemicals such as phenols, cresols, xylenols, catechols and pyrogallols are formed from the degradation of lignin.



Figure 2-8. Roles of pyrolysis intermediates in tar, gas and coke formation from guaiacols and syringols [65].

2.7 Pyrolysis studies of rice husk for bio-oil production

Pyrolysis of rice husk is extensively researched from literature, where various authors have performed studies on the pyrolysis of rice husks, whether it is analytical [66-73], bench-scale [53, 74-78] and pilot or industrial scale [79-81]. Analytical studies generally analyse the vapour generated from the degradation of the biomass without the condensation of the vapours into bio-oils, unlike for the bench-scale and pilot scale. Normally analytical studies are done as a preliminary assessment prior to the utilisation in a larger scale. Analytical pyrolysis of rice husk was carried out by various authors mostly by altering the heating rate to obtain kinetic parameters for suitable model predictions for the degradation of rice husks.

Worasuwannarak et. al measured the gas formation rates evolved which were found to be governed by the composition of the biomass [67].

Pyrolysis of rice husk have been carried out in a fluidised-bed, fixed-bed, rotary screw kiln and spout-fluid reactor. The process conditions with respect to the maximum liquid yield from literature can be found in Table 2-2. The most important process condition is temperature, where the optimum temperature ranges were around 400-500°C; a further increase in the temperature will decrease the liquid yield. Depending on the type of reactor, process conditions such as feed rate, heating rate, condensation temperature, particle size, holding time and the purge or fluidising gas were mentioned. Heo et. al studied the effects of product gas on the pyrolysis yield, and found that it increases the liquid yield as compared to using the fresh nitrogen gas as the fluidising medium [75].

Table 2-2. Process conditions for the highest rice husk bio-oil yield from literature

	Heo et. al [75]		Tsai et. al [74]	Natarajan et. al [76]	Ji-lu [79]	Roggero et. al [80]	William and Nugranad [53]	Li et. al [81]
Reactor type	Fluidised		Fixed	Fixed	Fluidised	Rotary screw kiln	Fluidised	Spout-fluid
Feed rate	90 – 150 g/h		11 - 21 g	-	7.32 kg/h	86 kg/h	200 g/h	7 kg/h
Optimum Temperature (°C)	400-450		>500	500	465	450	400	460
Heating rate (°C/min)	-	-	>200	60	-	-	-	-
Condensation temperature	-25	-25	< -10	-	-	-	-10	-
Feed particle size (mm)	-	-	< 0.5	1.18-1.80	-	-	0.25-1.00	0.4-0.7
Holding time (min)	-	-	> 2	-	-	-	-	-
Purge/Fluidising gas	Nitrogen	Product	Nitrogen	-	Nitrogen	Nitrogen	Nitrogen	Nitrogen
Purge gas flowrate	5 L/min	5 L/min	0.5-1.5 L/min	-	-	-	-	-
Liquid yield (%)	50	60	>40	31.78	56	41	59	48

Tsai et. al [74] and Li et. al [81] studied the effects of particle size and concluded that mass and heat transfer restrictions were significant for a larger particle size and decreases the bio-oil yield. Natarajan et. al however suggested otherwise; a decrease in the particle size lead to a decrease in the liquid yield, but pointed out that the effect was due to the difference in the vapour residence time [76]. This was initially thought due to the difference in reactor type, but Tsai et. al also studied using a fixed-bed reactor. Natarajan et. al did not mention the effects of the bed height as studied by Phan et. al, whom addressed that a difference in the bed height contributed to the changes in the fixed-bed reactor [82]. A higher bed-depth

corresponds to a lower freeboard volume, which in effect decreases the vapour residence time and increases the liquid yield.

The advantage of fixed-bed over fluidised-bed reactors is the low usage of purge gas flowrate as compared to the flowrate required to achieve the fluidisation of the bed material. Although that said, this is also compensated with the lower yields obtained of about 30-40 % for fixed-bed or rotary-screw kiln as compared to 50-60% yield for a fluidised bed.

2.8 Conclusion

Pyrolysis of biomass can either be fast, slow or intermediate depending on the temperature, vapour residence time, heating rates and product yield. Pyrolysis products evolved are liquid bio-oil, solid char and non-condensable gases. Intermediate pyrolysis of biomass is carried out at a moderate temperature of 450-500°C, a vapour residence time of a few seconds and a moderate heating rate. Product yields from intermediate pyrolysis will normally generate 50% liquid, 20% char and 30% gases. Since bio-oil is the key product, the pyrolysis mechanism of biomass composition (cellulose, hemicellulose and lignin) may explain the chemicals formation in the resulting bio-oil product. The pyrolysis of rice husk for bio-oil production is widely available in literature, therefore providing essential information in terms of the reactor types and various process conditions.

3 CATALYTIC PYROLYSIS OF BIOMASS

3.1 Introduction

Catalysts are defined as materials which accelerate chemical reactions without themselves undergoing changes. The catalyst selection and evaluation are important for higher product specificity and high yields of marketable products, since the products from this process are complex. Most biomass however, contains natural salts that will influence the decomposition products, which is reflected in the ash content. The catalytic effect, therefore, will become a part of the simple degradation process since the salts are not readily removed.

The intended purposes of using catalysts are to [54] :

- (1) Enhance the cracking reactions of the heavy molecules in pyrolysis products resulting in the production of lighter and less viscous bio-oil
- (2) Reduce the formation of carboxylic acids making bio-oils less corrosive
- (3) Enhance the formation of more valuable products like hydrocarbons that can increase the heating value of the bio-oil

Although using catalyst will enhance the bio-oil characteristics, compromises are expected such as the reduction in the bio-oil organics yield and the increase in water content. A reduction in valuable chemical components such as levoglucosan, i.e. an important anhydrosugar will also decrease due to the catalytic depolymerisation of cellulose [83].

3.2 Catalytic pyrolysis arrangement

There are five possible configurations that can be applied to incorporate catalyst into a pyrolysis system: (1) Addition or impregnation of catalyst into the biomass matrix, (2) co-feeding biomass and catalyst, (3) use catalyst as a part or whole of the fluidizing bed, (4) close coupled and in-bed catalysis, and (5) closed-coupled catalysis in a secondary reactor [84].

The first configuration is the pretreatment of biomass via catalyst impregnation. Wet impregnation method is done by mixing the biomass with a metallic aqueous solution for a particular duration, and dried prior to usage as a feedstock for pyrolysis. This involves direct impregnation of the catalyst into the biomass matrix prior to pyrolysis.

The second configuration involves co-feeding the biomass with the catalyst, which is added together into the system before the experiment. A uniform distribution ratio of feed and catalyst is essential to the process, so that the catalyst will not be entrained in the liquid product. With these initial two configurations, it is difficult to recover the catalyst, as it will be mixed together with the char.

Using the catalyst as a whole or part as the fluidizing medium is the easiest way to add the catalyst in to the pyrolysis system. The drawback would be that the catalyst may be rapidly deactivated by coking or deposition of char fines and condensed pyrolysis vapours.

The fourth configuration involves the catalyst being held in a cage at the freeboard as a fixed or fluidized bed. This will lead to accumulation of char in the reactor, which will increase the pressure drop in the system.

Incorporating a secondary reactor allows the catalyst to be heated independently from the main pyrolysis reactor. For a fluidised bed reactor, the catalyst reactor may be coupled after the cyclone to ensure that the chars are removed, thus reducing the catalyst deactivation.

3.3 Catalyst types

The various types of catalyst which can be applied for catalytic pyrolysis of biomass are zeolites, zeolite-like mesoporous catalyst, metal oxides and selected natural catalysts and aqueous metallic solution. Extensive review has been done on the types of catalysts used in biomass pyrolysis for bio-oil production [85].

3.3.1 Zeolite catalysts

Zeolites are water-containing crystalline aluminosilicates of natural or synthetic origin with highly ordered structures. They consist of SiO_4 and AlO_4^- tetrahedral, which are interlinked through common oxygen atoms to give a three-dimensional network through which long channel runs [86]. Different types of zeolite have different structures or frameworks, which results in their different properties and applications. The catalytic activities of zeolites are related to their shape selectivity and acidity, and have various potential and advantages over conventional catalysts.

Zeolite catalysts give higher value transport fuel product similar in content to gasoline (high aromatic content) and also offer the possibility of deriving even higher value chemical intermediates [53, 60] . In the temperature range of 350-450 °C oxygenated compounds in contact with zeolite catalysts have been found to undergo a group of reactions including dehydration, decarboxylation, cracking, aromatization, alkylation, condensation, and polymerization. The product from catalytic pyrolysis using zeolites always produced a two-phase liquid (aqueous and organic) and gas, while coke deposits formed on the catalyst surface [87]. The coke is mostly produced by dehydration of oxygenated organic compounds containing high amounts of oxygen.

The main zeolite catalyst used for upgrading biomass pyrolysis oils has been the hydrogen form of the zeolite, ZSM-5. The advantages of using a zeolite catalyst are that no H₂ is required, atmospheric processing reduces operating cost, and the temperatures are similar to those for bio-oil production. The zeolite ZSM-5 catalysts have a strong acidity, high activities and selectivity which convert the oxygenated oil to a hydrocarbon mixture in the C1 to C10 range [53].

Laboratory prepared ZSM-5 catalysts modified by substituting Al or hydrogen with different metals (Co, Fe, Ni, Ce, Ga, Cu, and Na) has been experimented by French and Czernik. The results were promising, although these catalysts were not fully characterised yet [87]. A new type of multifunctional catalyst which incorporates cerium into HZSM-5 framework was reported by Neumann and Hicks, which show high selectivities of chemicals [88]. Zeolites may also be synthesized from fly ash, although this requires more research [89] .

3.3.2 Zeolite-like catalysts

Zeolite-like catalysts are crystalline micro- or mesoporous materials having zeolite-like structure or layer structure [24]. Zeolite-like catalysts include MCM-41 [90-94], SBA-15 [91] and MSU-S [95], TiO₂ (rutile and anatase) and ZrO₂/TiO₂ [96], and Pd/SBA-15 [97].

3.3.3 Metal Oxides

Metal Oxides that have been used as catalysts in pyrolysis include zinc oxide (ZnO) [98], Criterion-534 [99], DHC-32, HC-K 1.3Q [100], Cu/Al₂O₃ [101], Nano SnO₂ [102] and sulphated metal oxides of Ti, Zn and Sn [103].

3.3.4 Natural catalysts

The alkali metals that naturally occur in ash in many biomass species and some wastes have a catalytic effect on all forms of thermochemical biomass conversion. Rice husk ash is composed of 90-97% silica content, is used as a catalyst support and good synthesis precursor for zeolites catalyst [89]. Rice husk silica can be synthesised into faujasite-type and NaA-type zeolite [104], MCM-41[105] in addition of Fe [106] and Al [107] into the MCM-41 template.

Fly ash, a solid residue obtained from coal, oil and biomass combustion composed of various metal oxides and possesses higher thermal stability [89]. Another type of natural catalysts that could be used for bio-oil upgrading is slate since it was found to improve the bio-oil quality in terms of stability, initial viscosity and heating value with no significant loss in the liquid yield [108].

3.3.5 Aqueous metallic solution

The aqueous metallic solutions are only applicable for the first configuration, i.e. wet impregnation of catalyst into the biomass matrix. The aqueous medium that have been used for this method are nitrates of Ni, Fe [109], Na, Mg, Ca, Zn, Fe(III), Cd and Pb [110]. Leaching with water removes large fractions of alkali metal eg: potassium and sodium, and smaller fractions of sulphur and phosphorus [111], and may be replaced by the metal ions present in the aqueous solution.

3.4 Catalyst's attachment/accessory

Catalysts on its own may not be practical as they may migrate during usage. A support may be used together with or without a binder to reinforce the catalyst. These attachments may or may not be involved in the catalytic reactions.

3.4.1 Catalyst support

The main function of the catalyst support is to increase the surface area of the active components. Typical catalyst support includes silica gel, aluminosilicates, activated carbon and ceramics, presented in the form of pellets, granules, extrudates and rings [86]. Honeycomb-shaped monolithic are the most standard for environmental applications, which

has excellent ratio of pressure drop to geometric surface area, durability and mechanical integrity, and can handle a large volumetric flow rates [112]. Antia and Govind demonstrated in their work that low coking zeolites such as HZSM-5, are ideally suited to a monolithic reactor configuration under gaseous conditions [113].

3.4.2 Catalyst binder

Catalyst binders are used to hold the catalysts in place onto a catalyst support. Binders such as kaolin, bentonite and montmorillonite have been used. Bentonite and montmorillonite are laminar and expandable clays with wet binding properties and are widely available around the world. Their dispersability in aqueous suspension is the reason for the agglomeration properties, in which the zeolite particles are surrounded by the by clay laminae, and when the water is removed, a solid phase is achieved in which the zeolite particles are bound by the clay [114]. It has been shown that the acidic forms of clays do not have binding properties and that their sodium forms exhibit better properties [115]. The presence of binder may enhance or inhibit the catalytic effect on the biomass pyrolysis vapours, depending on the catalyst type. Canizares et. al studied the effects of various concentration of sodium montmorillonite bound to zeolite over n-butane. Results show that no major changes were seen in the product distribution for HZSM-5 compared to the large-pore zeolite such as Mordenite, which shows a lower isomerisation and high disproportionation activity [116].

3.5 Factors affecting catalytic pyrolysis

3.5.1 Catalyst deactivation

All catalysts are subject to deactivation, i.e. a reduction in activity with time. The main processes which can cause deactivation are coking, poisoning and sintering. The deactivation of catalysts such as HZSM-5 may be reversible (coking) or irreversible (via the dealuminating effect of the water in the reaction medium) [117].

Coking or fouling occurs when materials are deposited on the surface of the catalyst, thus blocking the active sites. Coking can be minimised by using high heating rates of biomass with catalyst, high catalyst to feed ratio and proper catalyst selection [118]. The extent of deactivation may be determined by the amount of coke deposited on the catalyst. Aho et al. measured the nature of the coke for various zeolites, in which the highest coking was found with for zeolites with the largest pore size [119]. Another study by Jae et al. found that a

medium pore zeolites with moderate internal pore space and steric hindrance had the least amount of coke and the highest aromatic yield [120]. The usage of a catalytic guard bed such as dolomite may reduce deactivation due to coking, and the addition of dopants such as lanthanum to catalyst may reduce carbon deposition [121].

Poisoning is caused by chemisorptions of compounds in the process stream, which block or modify the active sites on the catalyst. Poisons may be eliminated by physical separation or by chemical treatment. By removing the product at intermediate stages, or operating the reactor at low conversion, catalyst poisoning may be reduced. The presence of sulphur is particularly sensitive to nickel alumina catalyst, due to the strong adsorption on metals [122].

Sintering is caused by the growth of small crystals which makes up the catalyst or its support, which decreases the surface area of the catalyst, resulting in an irreversible reduction in catalyst sites. Sintering of metallic particles in metal-based catalyst and dealumination of zeolite in the presence of water should be prevented. Sintering occurs when the local temperature of the catalyst exceeds approximately one-third to one-half of its melting temperature. Textural or structural promoters, which modify either the support or the metallic phase to stabilize the metallic particles, are commonly employed in the development of industrial catalysts [123].

3.5.2 Ratio of catalyst and biomass

A high catalyst-to-feed ratio improves the product yield by avoiding the undesired thermal decomposition reactions in the homogenous phase [118]. A study by Ma et al. showed that the increase in the catalyst ratio led to an increase in the liquid yield, whilst reducing the solid yield. The increase in the catalyst loading led to an increase in the active species conversion into liquid products, thus reducing the coke formation [124].

3.5.3 Catalyst bed temperature

The catalyst bed temperature for different catalyst varies accordingly. Williams and Nugranad found that increasing the catalyst temperature bed of ZSM-5 from 450-600°C, the yield of liquid bio-oil decreases and the gases increases. As for the composition of the liquid bio-oil, the single-ring aromatic compounds, phenolics and oxygenated compounds were decreased, and the increase in the PAH's were observed [53].

3.6 Catalyst regeneration

The regeneration or disposal of deactivated heterogeneous catalysts depends on chemical, economic and environmental factors [125]. Although regeneration and re-use of catalyst is possible, the catalysts would have to be replaced in a long term. Since coking or fouling is the most common factor for deactivation in catalytic pyrolysis of biomass, the removal of coke on the surface of the catalyst sounds promising. Various authors mention regeneration studies to remove coke deposits on spent zeolite catalysts from biomass pyrolysis by using thermal treatment, i.e. combustion in air for a certain period of time [117, 119, 126, 127]. Chemical treatment by washing in acid or alkali on has been done on organic abatement catalysts and platinum coated monolith catalyst for automotive purposes [128].

Regenerated catalysts may be determined by its surface area. Aho et al. found that for zeolite catalysts, regeneration using a stepwise temperature treatment up to 450 °C for 2 hr was sufficient to remove coke without changing the initial structure [119]. A gradual decrease of the regenerated catalyst activity was observed for prolonged and repeated upgrading-regeneration cycle. Guo et al. found for HZSM-5 that the catalytic activity changes moderately during the first three regeneration cycles, but deteriorates after the next three regeneration cycles [129]. Vitolo et al mentioned that combustion of coke may have caused dehydroxylation of the Bronsted acid sites, causing the loss of activity which were gradually deactivated by the repeated regeneration treatment [126].

3.7 Catalytic pyrolysis of biomass

Catalytic pyrolysis of rice husks is limited from literature as compared to the non-catalytic pyrolysis. In-situ upgrading of the rice husk pyrolysis vapour was done with various zeolites and zeolite-like catalysts [53, 73, 130], metal oxides [77] and clays [81]. The pyrolysis effect of the impregnation of salt metal and removal of ash on rice husk was also studied by Raveendran et al. which found that the decrease in ash content in rice husk led to an increase in the liquid yield and a decrease in the gases yield.[59]. Table 3-1 shows the yields of bio-oil from the catalytic pyrolysis of rice husks from literature.

Table 3-1. Yields of liquid from catalytic pyrolysis of rice husks

Authors		Pyrolysis / Catalytic Temperature	Liquid Yields (%)		
			Organics	Water	Overall
Williams and Nugranad [53]	Non-catalytic	550 / 550	28.5	18	46.5
	ZSM-5		3.8	18.4	22.2
Li et. al [81]	Non-catalytic	460	33.5	15	48.5
	Red brick		27.8	17.2	45
Meesuk et. al [77]	Non-catalytic	650	-	20	46
	Ni/Al ₂ O ₃		-	30	27
	Ni/LY		-	26	34
	Dolomite		-	26	29
	CoMo/Al ₂ O ₃		-	37	25

Li et. al studied the effect of red brick as a fluidising material compared to quartz sand. The overall liquid yield decreased, but the conversion of high MW compounds (substituted phenols and sugars) into lower MW compounds (phenols, acids, carbonyl and furans) increases. An increase in the heating value and the organics yield in the upper phase were seen.

Williams and Nugranad studied the effects of zeolite ZSM-5 on the pyrolysis of rice husks with a fluidised bed, coupled with a fixed-bed catalytic reactor. The yield of the organics in the catalysed oil was drastically reduced, and so does the oxygen content. The increase in the aromatic hydrocarbon and light phenols were significantly increased by ZSM-5.

Meesuk et. al studied the effects of various catalyst (Ni/Al₂O₃, Ni/LY, Dolomite and CoMo/Al₂O₃) mixed with sand in a fluidised bed reactor. The catalytic bio-oils obtained were analysed as a single homogenous phase. The overall liquid bio-oil yield was seen to decrease and the water content increases for all the catalytic runs. The order of catalyst performance under the same condition is CoMo/Al₂O₃ > Ni/LY > Ni/Al₂O₃ > dolomite > sand. Lu et. al studied the catalytic pyrolysis of biomass using on five different catalysts (HZSM-5, HY, ZrO₂ & TiO₂, SBA-15 and Al/SBA-15). No liquid yields were reported, but the effects of the catalyst on the various chemical groups were listed but only for cotton straw. Although the effects of catalyst were not analysed for rice husks, the chemicals quantified from cotton straw were gathered into the chemical groups, which should provide an general idea of the expected chemicals from the catalysts listed. Jeon et. al studied the effects of mesoporous zeolites (Meso-MFI and Pt-Meso-MFI) on rice husks, in particular with the changes in composition of the liquid products.

3.7.1 Mechanisms for catalytic pyrolysis of biomass

Whilst the study is limited for catalytic pyrolysis of rice husk, the usage of catalyst for pyrolysis on other biomasses are however quite extensive. It is therefore analogous to say that the rice husks are comparable with biomasses containing compositions of cellulose, hemicellulose and lignin, especially those of the agricultural wastes. Therefore a general mechanism, where available, particularly on the effects of selected catalysts on the pyrolysis vapours of biomass will be addressed.

Zhou et. al studied the catalytic pyrolysis of cellulose with zeolites and found a reduction of aldehydes, acids, esters with HZSM-5 having the effect on deoxygenation ability [131]. Al-MCM-41 catalyst reduces the acetic acid production [132] and affects the production of chemicals such as furfural, 5-methylfuraldehyde, 1,4:3,6-dianhydro- α -D-glucose and levoglucosan [133]. A similar study also found that yields of light phenols, hydrocarbons and polyaromatic hydrocarbons increased, and those of alcohols, aldehydes, heavy phenols, and heavy compounds decreased [90].

Figure 3-1 shows the reaction pathway for glucose catalytic pyrolysis on zeolite ZSM-5 involving two steps, from the thermal decomposition of glucose and the formation of aromatics. Carlson et. al identified two pathways from the rapid thermal decomposition of glucose. At low temperatures, glucose is converted into small oxygenates; and at high temperatures, into anhydrosugars. Aromatics are typically non-existent in non-catalytic pyrolysis of sugars/cellulosic materials, and usually originate from lignin-based structures. The formation of aromatics proceeds within the pore structure of ZSM-5 from the conversion of furanics or light oxygenates, although the selectivity is correlated to the temperature and catalyst ratio. Coke, which is formed from the intermediate products, has been identified to be the main competing reactions towards the formation of aromatics. Polyaromatic hydrocarbon formation may be reduced by decreasing the reaction time over the catalyst.



Figure 3-1. Reaction pathway for glucose catalytic pyrolysis on ZSM-5 [134]

Another mechanism available from literature is the aromatic formation on ZSM-5 from lignin. Figure 3-2 is the mechanistic pathways of aromatic formation from lignin on ZSM-5, which was reproduced by Ramirez-Corredores from the study of Mullen and Boateng [135].

The depolymerisation of lignin produces guaiacols and syringols, and simple phenols. Partial deoxygenation of lignin aromatic units produces simple phenols, which is a potential source of coke and catalyst deactivation on ZSM-5. The mechanism pathway from Figure 3-2 suggested sources for the formation of aromatics were derived from lignin oligomers which undergoes oligomerisation and cyclisation.



Figure 3-2. Mechanistic pathways of aromatic formation from lignin on ZSM-5 [63] – reproduced from [135]

4 CHARACTERISATION METHODS OF BIOMASS AND BIO-OIL

4.1 Introduction

In this research, Brunei rice husks (BRH) is used as biomass for the intermediate pyrolysis study. This chapter introduces the characterisation methods for the biomass feedstock and the resulting pyrolysis bio-oil.

4.2 Biomass preparation/processing

The rice husk was obtained from Brunei in a dry form before shipping into the UK. Prior to characterisation, BRH was ground using a Fritsh blade grinder with a 4-mm sieve. The samples were sieved and the particle size distribution determined. The standard practice for the preparation of biomass prior to the analyses is according to the ASTM E1757-01 standard [136] ensuring uniformity throughout the analyses and experiments.

4.3 Biomass characterisation methods

The characterisation methods for biomass include proximate analysis, elemental/ultimate analysis, ash/inorganic composition analysis, structural/compositional analysis, heating/calorific value determination and thermogravimetric analysis and derivative thermogravimetric analysis.

4.3.1 Proximate Analysis

The proximate analysis are performed according to the British and European standard test method for measuring the moisture (BS EN 14774-3:2009), volatile (BS EN 15148:2009) and ash contents of solid biofuels (BS EN 14775:2009) respectively [137-139]. Analyses were done in triplicates and the average reported.

Moisture content is determined using a drying oven, where the temperature is held at 105°C for at least 3 hours, with repeated measurements at interval until it achieves a constant weight. Samples were cooled in a dessicator prior to weighing. Crucibles with about 1g of samples each were analysed. The percentage weight loss after the final drying process can be considered as the moisture content.

Volatile matter can be defined as the content released when heating the biomass at a controlled conditions. About 1g of moisture-free biomass sample is placed in a ceramic crucible enclosed with a lid and heated at 900°C for 7 minutes. The crucible was placed in a dessicator and weighed when it cooled to room temperature. The percentage of volatile matter can be calculated from the weight loss of the sample before and after heating.

Ash content is determined by heating the sample up from room temperature to 550°C for a minimum of 3 hours or until all the carbon is eliminated. The residue remaining after the process is classified as the ash content.

The fixed carbon value is obtained by percentage difference [140]. Fixed carbon can be defined as the carbon remaining after heating in a prescribed manner to decompose thermally unstable components and to distill volatiles [141] .

4.3.2 Elemental Analysis

The elemental analysis gives the composition of biomass in wt% of the main elements carbon, hydrogen, nitrogen and sulphur (C, H, N and S). Oxygen was obtained by difference. The ultimate analysis was carried out using a Carlo-Erba 440 elemental analyser by an external company (MEDAC Ltd., Surrey, UK).

4.3.3 Ash/Inorganic Composition Analysis

The inorganic elements that are present in biomass were determined using an inductively coupled plasma-optical emission spectrometer (ICP-OES) which was carried out externally by MEDAC Ltd., Surrey. A semi-quantitative scan was done, and elements such as potassium (K), calcium (Ca), phosphorous (P), magnesium (Mg), sodium (Na), copper (Cu) and silicon (Si) are determined.

4.3.4 Structural/Compositional Analysis

The Fibercap equipment is used for this analysis based on the Van Soest method or the 'food-processing industry' methods for its determination [142-145]. The lignocellulosic contents of the biomass, i.e. cellulose, hemicellulose and lignin are determined from the Neutral Detergent Fibre (NDF), Acid Detergent Fibre (ADF) and the Acid Detergent Lignin (ADL).

For the determination of NDF, 0.5g of biomass samples were placed in 6 dried fibercap capsules and pre-extracted three times with 120 ml acetone to remove fat contents. Pretreatment of the samples is required by soaking with 2 ml working amylase solution (WAS) in 120 ml hot distilled water to remove undesirable starch. Samples were then extracted in 350 ml neutral detergent solution in a Fibretec™ reflux system for 30 mins. After the process has ended the samples were rinsed in hot boiling water three times, followed by a series of similar de-starching and de-fatting process. Samples in the capsules were dried for at least 5 hr at 105°C and then ashing was done at 600°C for 4 hr. The NDF was calculated by the difference in the initial and final weight of the sample.

A similar NDF procedure was followed for the determination of ADF, except that 1g of the biomass sample was put in the capsules, the de-starching process was removed, and an acid detergent solution was used for the extraction reagent. The ashing step in this procedure was omitted for the determination of ADL.

For ADL determination, the dried samples from the previous ADF procedure were consecutively de-fatted, and then extracted with soaking in 72% sulphuric acid solution for 3 hrs. The samples were rinsed in hot boiling water until it is acid-free, followed by drying and ashing procedure. The cellulose, hemi-cellulose and lignin contents can be calculated, and shown in Table 4-1 below.

Table 4-1. Calculation for cellulose, hemicellulose and lignin determination

Composition (%)	Calculations (ash and extractives-free basis)
Hemi-cellulose	NDF - ADF
Cellulose	ADF - ADL
Lignin	ADL

4.3.5 Heating/Calorific Value

The higher heating value (HHV) is determined from a Parr 6100 bomb calorimeter following the ASTM D5865 standard method [146], at a wet or as received basis. The principle behind the bomb calorimeter is that it measures the heats of combustion of a sample in oxygen. A known amount of sample placed in a crucible, positioned in a steel container 'bomb' was burnt in excess oxygen. The heat given off is transferred to a jacket of a fixed volume of water, and the temperature change (ΔT) is measured. The effective heat capacity of the bomb calorimeter (Q) can be obtained by calibrating with a substance (m) of a known heat of combustion (c), such as benzoic acid with 25.43 MJ/kg at 25°C.

$$Q = mc\Delta T \quad (\text{Equation 4-1})$$

The value of Q is therefore constant throughout, unless a different bomb is used. The value of the effective heat capacity of the bomb is then substituted in equation 4-1 to find the unknown heat of combustion for the biomass. The HHV of biomass takes into account the latent heat of vaporisation of water in the combustion products, and assumes that water is in the liquid state after combustion (inclusion of enthalpy change).

The biomass used here is in a wet basis, i.e. taking into account the moisture content. Most values in literature quote values on dry basis, therefore we can use mathematical correlation to consider the moisture content, and express it on a dry basis from equation 4-2 below [147]. Note that the HHV (ar) and HHV (dry) stand for wet basis and dry or moisture-free basis respectively.

$$HHV_{ar} = HHV_{dry} \left(1 - \frac{\text{Moisture}}{100}\right) \quad (\text{Equation 4-2})$$

The Lower Heating Value (LHV) can be calculated from correlation from equation 4-3 [147] below.

$$LHV_{dry} = HHV_{dry} - 2.442 * 8.936H/100 \quad (\text{Equation 4-3})$$

4.3.6 Thermogravimetric Analysis (TGA) and Derivative Thermogravimetric Analysis (DTG)

Thermogravimetric analysis (TGA) is a technique whereby the weight of a substance in an environment heated or cooled at a controlled rate is recorded as a function of time or temperature [148]. The derivative thermogravimetric analysis (DTG) is the curve obtained by plotting the first derivative of TGA curve as a function of temperature. The DTG curve can show the maximum or minimum, which is clearly shown for particular overlapping reactions at a given temperature. The concept of TGA pyrolysis is to study of the decomposition behaviour of biomass under an inert or pyrolytic condition. Essentially, the main information that can be derived from TGA is the pyrolysis onset temperature range, weight loss percentage and the char content, while DTG pyrolysis can illustrate the maximum weight loss for different peak temperatures.

TGA for pyrolysis has been done in duplicates. An automated Perkin Elmer Pyris 1 TGA thermogravimetric analyser was used, with a nitrogen flow of 20 ml/min at 20°C/min heating rate, at up to 900°C. Biomass samples of 2-3 mg were put in a ceramic crucible on an analyser tray. The machine picks the crucible up via a hook which acts as a weighing balance, and is inserted in an enclosed furnace. The sample is then heated up according to the programmed variables, where the weight loss from the thermal degradation is measured.

4.4 Characterisation of bio-oil

The main product produced from the pyrolysis of biomass is bio-oil. The major liquid components yield includes water and organic compounds derived from the degradation of cellulose, hemicellulose and lignin. Characterisation of bio-oil include the determination of the water content, acidity, viscosity, density, elemental analysis, heating value and the gas chromatography-mass spectrometry (GC-MS).

4.4.1 Water Content

The water content of the bio-oil was determined using a Mettler Toledo Karl Fisher V20 compact titrator based on ASTM D1744 [149]. Prior to analysis, the system is calibrated with HPLC-grade water. Hydranal working medium K was used as the solvent and Hydranal Composite 5K as the corresponding titrant. A known weight of the bio-oil is injected into the enclosed titration beaker, and the weight is entered into the system. The result of the water content in the bio oil is then displayed following after the titration is completed. The analyses were done in triplicates and average reported.

4.4.2 Acidity

The acidity of bio-oil can be determined from the pH or the acid number. The pH was obtained using the Sartorius basic meter PB-11. Before the experiment, the pH meter is calibrated with liquid calibration standard pH of 4 and 7. The probe is then dipped into the bio-oil, and analysis was repeated at least three times.

Acid number or Total Acid Number (TAN) was determined using a Mettler Toledo G20 titrator based on ASTM D644-04 with a solvent mixture of toluene, 2-isopropanol and water, and potassium hydroxide solution (KOH) as the titrant. A known weight of bio-oil of less than a gram was dissolved in the solvent mixture. The samples were automatically stirred

throughout the analysis to ensure uniform mixture of the titrant and solution. A potentiometer measures the acidity by determining the end point. The results are displayed with units representing the amount of KOH in milligrams that is required to neutralise the acids in 1g of bio-oil.

4.4.3 Viscosity

Kinematic viscosity was measured according to the ASTM D445. A Cannon-Fenske Routine glass capillary viscometer was filled with the bio-oil at 40°C. A fixed volume of oil was passed through the capillary under gravity and the sample time travelling was recorded. The kinematic viscosity can be calculated from the product of the viscometer calibration constant and the measured time. The dynamic viscosity can also be obtained from the product of the kinematic viscosity and the density of the bio-oil at 40°C.

4.4.4 Density

The density of the bio-oils was measured using a Mettler Toledo 30PX densitometer. The principle behind it is that the device measures the light reflection from the liquid surface. The liquid sample is injected into a measuring cell where the device will automatically produce a reading.

4.4.5 Elemental Analysis

The elemental analysis for bio-oil is the same as section 4.3.2.

4.4.6 Heating/Calorific Value

The calorific value was calculated via correlations using data obtained from elemental analysis derived by Channiwala and Parikh [150] from the equation 4-4 below:

$$HHV_{wet} = 0.3491C + 1.1783H + 0.1005S - 0.1034O - 0.015N - 0.0211A \quad (\text{Equation 4-4})$$

However, there are assumptions that needed to be considered such as the value of A (ash content) is assumed to be 0.5% by weight. The values of C, H, N, S and O can be correlated from the elemental analysis. The HHV obtained takes into account the water content, and therefore converted to dry basis using equation 4-2.

4.4.7 Gas Chromatography – Mass Spectrometry (GC-MS)

GC-MS analysis of bio-oil was conducted using a Hewlett Packard HP 5890 Series II Gas Chromatograph with an Agilent auto sampler and coupled to an HP 5972 MS detector. Helium is used as the carrier gas with a DB 1706 non-polar capillary column. The initial oven temperature was 40 °C and rising up to 290 °C at a rate of 3 °C/min. The injection temperature was held at 310 °C with a volume of 5 µl. Identification of the GC-MS peaks is based on the NIST mass spectra library. The dilution solvent used was HPLC ethanol and the dilution ratio was 5:1 to bio-oil. The analysis was done in duplicates.

5 BIOMASS CHARACTERISATION RESULTS OF BRUNEI RICE HUSK

5.1 Introduction

This chapter focus on the results from the characterisation of Brunei rice husks. In comparison to BRH, other type of rice husk species from West Africa (AFRH) was also characterised. The method employed was from the procedures laid out from previous Chapter 4 for the characterisation of biomass.

5.2 Sieve analysis

The rice husks samples were sieved to different particle size distribution (Table 5-1). For thermochemical reaction, the particle size has an effect on the degradation condition. A large particle size may cause secondary reactions which lead to the formation of char, and a particle size too small may not be retained in the reaction zone and thus entrained elsewhere [151]. Figure 5-1 shows the Brunei rice husk samples (as received) before and after grounded.



Figure 5-1. Ungrounded (left) and ground (right) Brunei rice husks samples

Table 5-1. Sieve analysis results for BRH and AFRH

Particle size (μm)	Content (wt%, as received basis)	
	BRH	AFRH
>1000	24.93	16.64
850-1000	17.02	18.61
600-850	25.81	27.14
500-600	6.96	8.64
355-500	9.65	11.04
0-355	15.63	17.92
Total	100	100

5.3 Biomass characterisation results

The characterisation results from BRH and AFRH samples are given in Table 5-2 and compared with the results of other rice husks values from literature.

Table 5-2. Summary for the experimental (BRH and AFRH) and literature rice husk characterisation data

	EXPERIMENTAL		LITERATURES				
Rice Husk species	BRH	AFRH	Lemont [66]	Pa Potho [66]	ROK 16 [151]	Rice Hull [71]	Rice Husk [68]
PROXIMATE ANALYSIS (wt. %)							
Moisture	8.43	7.88	9.08	10.16	10.44	1.50	6.73
Volatile Matter	68.25	58.22	66.40	67.60	70.20	61.00	61.23
Fixed Carbon	8.49	7.86	13.60	14.20	14.50	24.00	14.96
Ash	14.83	26.04	20.00	18.20	15.30	13.00	17.09
ELEMENTAL/ULTIMATE ANALYSIS (wt. %)							
C	39.48	34.895	37.60	42.6	44.5	45.00	38.45
H	5.71	5.145	5.42	5.10	5.51	5.80	5.22
N	0.665	0.31	0.38	0.51	0.46	0.93	0.45
O	54.12 ^a	59.01 ^a	33.20	33.60	35.20	48.00 ^a	49.15 ^a
S	< 0.10	0.64	0.034	0.025	0.021	0.20	-
Cl	0.025	<0.01	0.01	0.13	0.031	-	-
O:C molar ratio	1.03	1.27	0.66	0.59	0.59	0.80	0.96
H:C molar ratio	1.74	1.77	1.73	1.44	1.49	1.55	1.63
HEATING VALUES (MJ/kg)							
HHV (dry basis)	17.34	14.05	15.90	15.98	18.31	-	-
LHV (dry basis)	16.10	12.92	14.22	14.12	16.20	-	-
COMPOSITIONAL/STRUCTURAL ANALYSIS (wt. %)							
Cellulose	41.52 ± 0.45	37.34 ± 0.14	29.2	35.5	-	-	-
Hemicellulose	14.04 ± 0.53	10.07 ± 0.51	20.1	21.35	-	-	-
Lignin	33.67 ± 0.19	41.08 ± 0.18	30.7	24.95	-	-	-
Extractives	10.77 ± 0.37	11.5 ± 0.45	-	-	-	-	-

^a by difference

As rice is grown throughout different parts of the world, the sample species or regional effects may have an effect towards the characterisation values. Mansaray and Ghaly studied the Lemont, Pa Potho and ROK 16 rice varieties. The rice husks were collected in a polyethylene bag from their respective rice mills and transported to Halifax, Canada. The rice husk samples were dried in an air-forced oven at 105°C for 24 hours to avoid deterioration

from moisture. Prior to analysis, other than the moisture content, the dried samples were ground and sieved. Fine ground samples were used for biomass characterisation.

Lemont rice species was obtained from Broussard Rice Mills, Louisiana in USA. The dehusking process was using rubber roller mills. Pa Potho and ROK 16 species were obtained from West African Rice Research Station, Rokupr in Sierra Leone. The difference between both of them was the processing methods. Pa Potho underwent a parboiling process which involves saturating the rice grain in water and raising the temperature, before dehusking using rubber roller mills. ROK 16 rice variety was dehusked using a large disc sheller mills.

The rice variety studied by Teng et. al was labelled 'rice hull' and did not mentioned the processing conditions. The authors also did not mention specifically the region where it was grown, but pointed out that rice hull is a growing solid and waste disposal problem in the Asian and Pacific region.

The rice species studied by Hu et. al was not mentioned but was obtained from China. The sample labelled 'rice husk' by the author was meshed to small particles sizes with range 25 μ m to 1mm, with an average sizes of biomass close to 300 μ m. The meshing process was done before the biomass was transported from China to Germany for analysis.

5.3.1 Proximate and ultimate analysis

BRH has a moisture content of 8.43 wt. % which is comparable to most rice husks literature values, although some vary slightly due to different storage and environment conditions. Conditions such as humidity do affect the analysis, since the biomass is hygroscopic in nature. The value of 1.50 wt. % moisture content for one of the literature values suggests that the biomass was dried prior to analysis. One crucial condition for pyrolysis process is the amount of moisture content in the feedstock sample. The moisture content should be minimised so that it does not add to the water content in the resulting liquid bio-oil.

The volatile content for BRH was found to be high with 68.25 %. This compares favourably to other rice husk species such as ROK 16 and Pa Potho reported by Mansaray and Ghaly, with a value of 70.2% and 67.60% respectively. Generally, a high volatile content for biomass is favourable for pyrolysis process to indicate a high liquid yield production. As for AFRH, the value for the volatile content of 58.22% is slightly low when compared with other rice husk species.

The ash content for BRH and AFRH are 14.83% and 26.04% respectively. Although comparable to values in literature, they are noticeably high. Typically rice husks species have a higher ash content when compared to other biomass such as willow wood 1.9% [110], wheat straw 4.89% and miscanthus 4.46% [152]. High ash content in the biomass is known to affect the pyrolysis products in terms of lowering the liquid yield and increasing the non-condensable gases due to their catalytic effects. The variation in methods of harvesting, handling and storage techniques can contribute to the difference in the ash values. The ash content may originate from the biomass itself, or from foreign materials e.g. soil, which is collected along with the biomass. Considering that rice husk has high ash content compared to other biomass, this will be a significant factor which will affect the pyrolysis yield.

The ultimate analysis of BRH indicate that it has 39.5 wt% C, 5.7 wt% H, 54.12 wt% O, 0.67% N and traces amounts of sulphur and chlorine. The values of N, S and Cl in rice husks are minute, which accounts for less than 1% of their total compositions. The small amount of nitrogen and sulphur indicates that the sample will produce less pollutant in the form of NO_x and SO_x . The value for sulphur is higher in AFRH with 0.64% as compared to BRH with < 0.10%. A possible explanation of this might be due to contamination of the sample with soil or fertilisers which contain sulphur in the form of sulphates. The amounts of Cl present also indicate a very minute amount of dioxin formation during combustion of the biomass or their products.

The O:C and H:C molar ratios are calculated and compared accordingly. A higher HC molar ratio and a lower OC molar ratio are favourable as fuels. Oxygen values which was obtained by difference tends to be higher, leading to a higher O:C molar ratio. A comparison of the OC ratio for the oxygen values calculated by difference may indicate that the values are affected by the moisture content. The H:C molar values calculated from the literature ranges from 1.44 to 1.73. The values obtained for BRH and AFRH were 1.74 and 1.77 respectively, which were slightly higher than those in literatures.

5.3.2 Compositional Analysis

Majority of the composition from rice husks consists of cellulose and lignin. The compositional or structural analysis of BRH shows that it has 41.52% cellulose, 14.04% hemicelluloses and 33.67% lignin. AFRH shows that it has higher lignin % content, but a lower cellulose and hemicelluloses % content by weight compared to BRH and is therefore expected to generate more lignin-derived pyrolysis products.

Another method of obtaining the compositional values is using the 'wood-industry' method which involves a different set of experimental procedures. The experimental values for BRH and AFRH may not be comparable to the literature values due to the difference in procedures, except for the lignin values which was determined using 72% sulphuric acid. A study by Carrier et. al showed that the values for cellulose is comparable and that the hemicellulose values were generally lower for the 'food-industry' method as compared to the 'wood-industry' method [145]. The lower hemicellulose values for BRH and AFRH as compared to the values for Lemont and Pa Potho species illustrated the difference.

Pyrolysis products can be predicted from the thermal decomposition of the main three components. Besides the formation of water, carbon dioxide and carbon monoxide, the pyrolysis of cellulose and hemicellulose will generate hydrocarbons, aldehydes, ketones, acids and alcohols; whereas the pyrolysis of lignin will generate mostly phenols and alcohols [153].

5.3.3 Heating Values

The heating value determined experimentally from the bomb calorimeter is quite similar to the values from literature. The higher heating value (HHV) on dry basis shows that BRH has a heating value of 17.34 MJ/kg, compared to a value of 14.05 MJ/kg for AFRH. Lemont and Pa Potho reported a lower value of 15.90 and 15.98 MJ/kg, which may suggest that higher ash content in biomass corresponds to a reduction in their heating values. A study by Sheng and Azevedo mentioned that the HHV decreases with an increase in the ash content, and that a trend exists between the HHV and volatile content [154].

Values from Table 5-2 for the volatile content and the HHV were plotted as a function of ash content and illustrated in Figure 5-2. Although volatile matter may not correlate with the HHV, it is an indication of the presence of combustibles in the rice husks. The trend for rice husks shows a decrease in both volatile matter and HHV with the increase in the ash content, which is similar to the study by Sheng and Azevedo on biomass. This shows that the ash content has a major effect on the energy content of biomass.

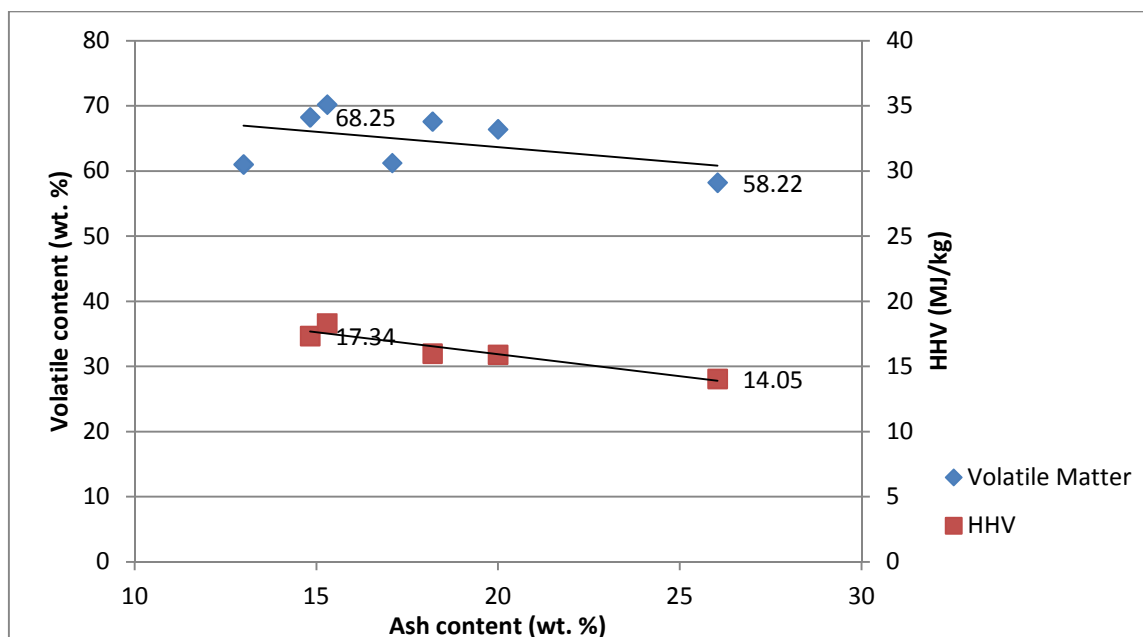


Figure 5-2. Volatile content and HHV as a function of ash content

5.3.4 Ash composition analysis

Ash composition analysis was done only for BRH. The ash composition shows that it has a significant amount of potassium (K), calcium (Ca) and phosphorus (P). The relatively lower content of potassium in BRH as compared to 1.20% in miscanthus and 0.57% in wheat straw [152] is an added advantage, because a higher potassium amount can contribute to slag formation in furnaces and due to a decrease in the ash melting point [155]. As for phosphorus, the added presence may increase the char yield during pyrolytic decomposition of biomass [156]. Table 5-3 shows the comparison of the ash composition analysis for BRH compared with literature. Tsai et. al and Lu et. al measured the ash composition from rice husk as received, but Mansaray and Ghaly measured the ash composition from rice husk ash. It is as expected that silicon (Si) is very high in rice husk ash, but unusual that the Si value for BRH is significantly very low as compared to the other rice husks literature values.

Table 5-3. Ash composition analysis of BRH compared to rice husks from literature

Element	Values (ppm)									
	K	Ca	P	Na	Fe	Si	Mn	Zn	Cr	Mg
BRH	2000	519	605	186	415	223	257	16	90	132
Tsai et. al [74]	1630	94	94	207	202	39000	-	24	-	699
Lu et. al [157]	3600	1600	300	-	55	68200	330	-	-	510
Mansaray and Ghaly [151]	18000	3300	300	800	1600	970000	-	80	-	3000

Some amounts of sodium (Na), iron (Fe), manganese (Mn), chromium (Cr), magnesium (Mg) and zinc (Zn) are also present in BRH. The absence of heavy metal elements such as cadmium, lead or mercury suggests that the biomass and their products can be applied to small-scale combustion systems, due to the strong impact on ash quality and particulate emissions [155].

5.3.5 TGA and DTG

The thermochemical characterisation from the TGA and DTG can be seen in Figure 5-3 below. A comparison of the TGA and DTG derived information of rice husk from the experiment and literature can be found in Table 5-4. The information include the pyrolysis onset temperature range, weight loss and char yield at 500°C, heating rates and the peak and shoulder peak temperatures for the maximum weight loss. Weight losses below 100°C are considered to be the moisture in the sample. The pyrolysis onset temperature range for BRH and AFRH can be seen to range from 200-550°C. The thermal degradation study for both rice husks shows typical biomass degradation behaviour.

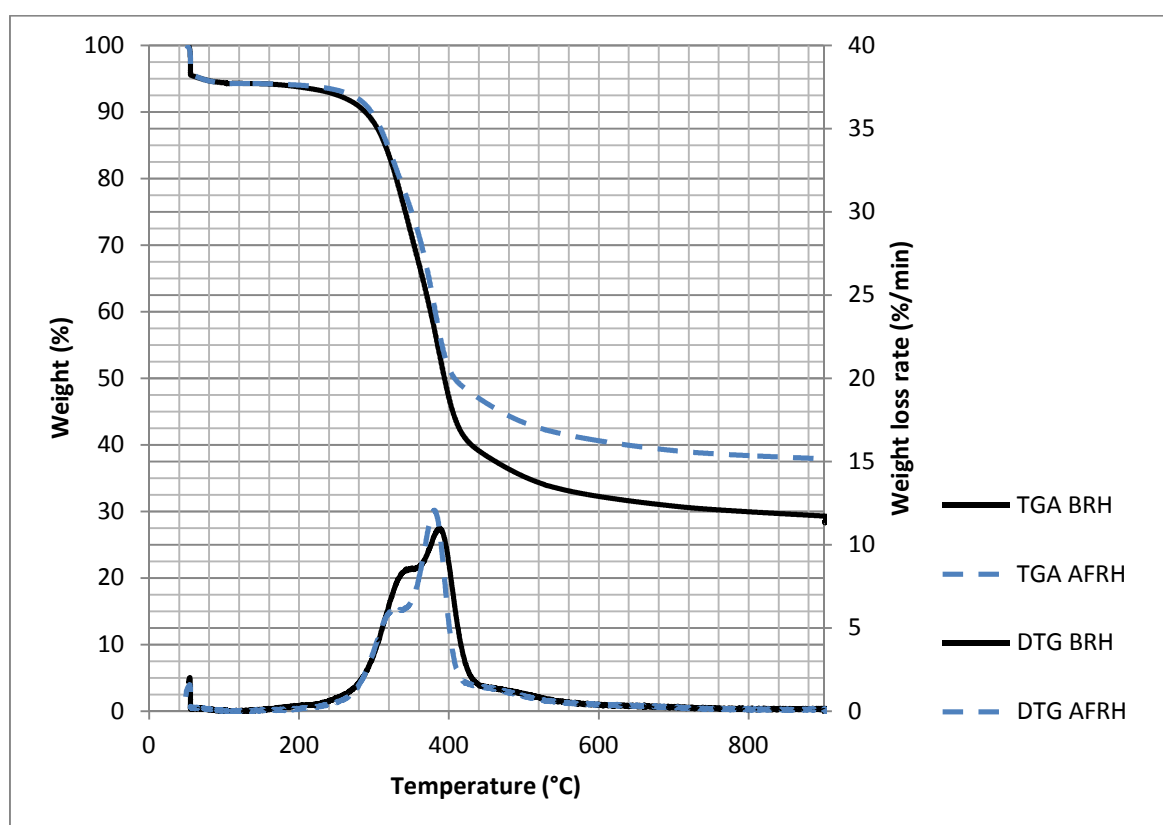


Figure 5-3. TGA and DTG plots for BRH and AFRH

Table 5-4. TGA and DTG pyrolysis derived information of rice husks for the experimental and literature values

	Experimental		Literatures			
	BRH	AFRH	Isa et. al [72]	Worasuwannarak et. al [67]	Mansaray and Ghaly (Pa Potho) [66]	Teng et. al [71]
Pyrolysis onset temperature range (°C)	200-550	200-500	200-550	200-500	200-500	200-600
Weight loss at 500 °C (%)	60	50	58	50	55	57
Heating rate (°C/min)	20	20	20	10	10	100
Peak temperature for maximum weight loss (°C)	380	390	340	340	348	390
Shoulder peak temperature (°C)	340	320	300	300	312	330
Char yield at 500°C (%)	34	44	39	50	40	40

A weight loss is achieved at 60% for BRH, and 50% for AFRH at temperatures below 500°C, which agree with the range of values from the literature. The TGA curves show that most of the weight loss for both of the rice husks occurs between 280°C and 420°C, which indicate essential indication for determining the optimum temperature required for pyrolysis reactions. No significant weight loss can be seen after 600°C for both of the rice husks. The weight loss % at the chosen temperature (500°C) indicates the char yield, i.e. residue at the corresponding temperature. The char yield at 500°C for BRH and AFRH is 34 % and 44 % respectively.

The DTG curve can indicate clearly the temperature where the maximum weight loss occurs. Both rice husks has two major peaks at around 320-340°C and 380-390°C, but BRH has a higher weight loss rate for the first shoulder peak compared to AFRH. The values from literature also indicate two major peaks from rice husks which range from 340-390°C for the main peak, and 300-330°C for the shoulder peak. The variation in the heating rate for most of the literature values may shift the peak temperatures slightly.

The first shoulder peak can be associated with the thermal degradation of hemicellulose, and the second peak is due to the decomposition of cellulose and lignin [66]. As lignin degrades over a wide temperature range, it is difficult to distinguish between both of them. Carrier et. al also concluded in their study and found correlations in the application of TGA with the compositional analysis for obtaining the cellulose and hemicellulose values, but not for lignin [145]. BRH has a higher content of hemicellulose than AFRH, therefore showed a considerable higher weight loss rate for the first shoulder of the DTG peak. The second peak occurs at 380°C for both samples, but a sharper peak is seen for AFRH compared to BRH.

5.4 Summary

Characterisation studies have been carried out for BRH, with AFRH as a comparison according to the standard procedures, together with other rice husk species from literature. TGA and DTG pyrolysis behaviour have also been studied. Results from the thermochemical characterisation shows that BRH is suitable as a feedstock for the potential bio-oil production using pyrolysis technology.

6 PYROLYSIS OF BRUNEI RICE HUSK

6.1 Introduction

This chapter describes the experimental setup and operation of the bench-scale intermediate pyrolysis for BRH. The liquid bio-oil produced was characterised and analysed based on the methods discussed from Chapter 4.

6.2 Bench scale intermediate pyrolysis rig

The rig is made up of two reactors connected in series with condensation train units as shown in Figure 6-1. The primary reactor is made of quartz glass tube with an internal diameter of 60 mm and height of 390 mm. The reactor head has three sockets for a thermocouple, purge gas and a socket connecting the transition tube to the secondary reactor. A thermocouple connected to a temperature controller runs through the middle of the reactor. The purge gas N_2 flows into the reactor, acting as a sweeping gas and is controlled by a flowmeter. The primary reactor tube is heated via a furnace which has a temperature controller unit, which relayed temperature information from the thermocouple. The transition tube together with the reactor head is lagged to ensure a minimal condensation of pyrolysis vapours from the primary reactor.

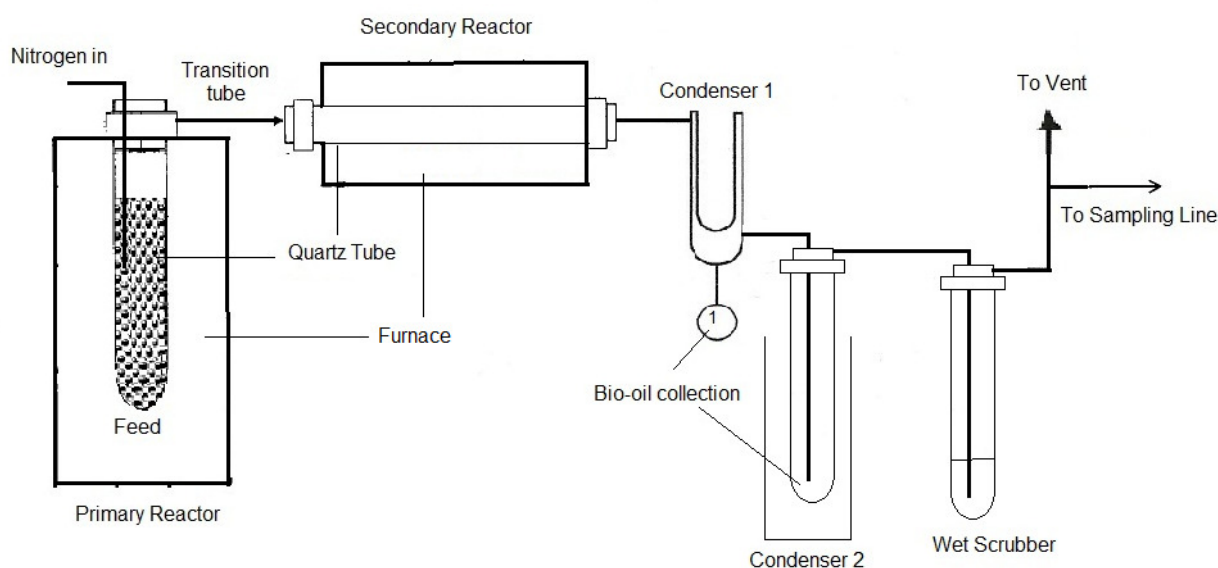


Figure 6-1. A schematic diagram of the pyrolysis rig setup

The secondary reactor is made up of an open tubular quartz glass tube with an internal diameter of 25 mm and a length of 390 mm and is heated by a tube furnace. The secondary reactor temperature is measured by a thermocouple connected to a handheld temperature indicator. The secondary reactor is required to hold and support catalytic material used during catalytic pyrolysis experiments. For non-catalytic pyrolysis experiments, the secondary reactor act as a heated tube to transfer the pyrolysis vapours generated from the primary reactor into the condensation trains. The secondary reactor flexibility ensures a setup that compares non-catalytic and catalytic pyrolysis experiments.

The condensation trains consist of two condensers used for the collection of bio-oil. The first condenser is a cold-finger condenser connected to an oil-pot, followed by a cold trap condenser. The condensation medium for the indirect quenching of the pyrolysis vapours is dry-ice and acetone mixtures, which cools it down to approximately -70 °C.

The non-condensable gases released were scrubbed with cooled isopropanol before sending a stream of the gases to the sampling line and vented out. This ensures the removal of excess condensable vapours and char fines before venting the rest of the gases out into the fume cupboard. The extensive list of experimental set-up specifications for the intermediate pyrolysis rig may be found in Appendix B.

6.2.1 Reaction conditions

BRH amounting to about 100 g of sample is subjected to pyrolysis in the primary reactor. Prior to the pyrolysis run, BRH is weighed and placed into the primary quartz glass tube and the feed bed height measured. The primary reactor head is inserted onto the quartz tube along with the thermocouple, transition tube and the purge gas insert tube. A clamp is attached at the neck of the joints to provide a tight grip and support the quartz tube. The connection from the transition tube leads to the secondary reactor and the condensation trains.

Nitrogen gas flow into the reactor was maintained at a flow rate of 50cm³/min to ensure a constant vapour residence time. The stated flow rate was chosen based on the lowest possible setting for the flowmeter, which is enough to purge the system. This was assured by taking an injection of the gases prior to each pyrolysis run into the GC-TCD. The primary reactor containing the BRH in the quartz glass tube was heated from 25°C to 450°C at a rate of 25°C/min. The pyrolysis temperature of 450°C was selected based on the results obtained

from the TGA, which showed that it is sufficient to remove most of the volatile matter from the biomass sample and the optimum temperature for onset pyrolysis of BRH. Since a temperature of 450 °C is used, the material for the reactor head is borosilicate glass which can withstand a maximum temperature of 500 °C, although a maximum temperature limit of 900 °C may be achieved for the quartz glass tubes. The solid residence time is 30 min, which accounts for the time taken for the biomass to be fully converted in the reactor, and relates to the duration of the pyrolysis runs.

The vapour residence time is not calculated, and can be assumed in the order of seconds. The value was not calculated, but several factors were identified which affect the vapour residence time for a fixed-bed reactor, such as the amount of feed and the flowrate of the purge gas. The amount of feed affects the bed height in the reactor or the freeboard volume, which has a strong influence on properties of pyrolysis products but a small effect on product yield [82]. The purge or sweeping gas affects the pace at which the pyrolysis vapour is removed from the pyrolysis zone. Therefore these factors are ensured to be kept constant throughout for the ground pyrolysis runs to eliminate the effects of vapour residence time on the pyrolysis system.

Figure 6-2 shows the temperature profiles for a typical BRH sample in the reactor. The programme temperature is the temperature profile applied to the primary pyrolysis reactor. The sample temperature shows the actual temperature measured in the reactor. The reaction peaks from ambient temperature to the maximum pyrolysis temperature at around 15 minutes. The sample was held at the maximum temperature for another 15 minutes. This temperature profile is used for the pyrolysis experiments throughout this study.

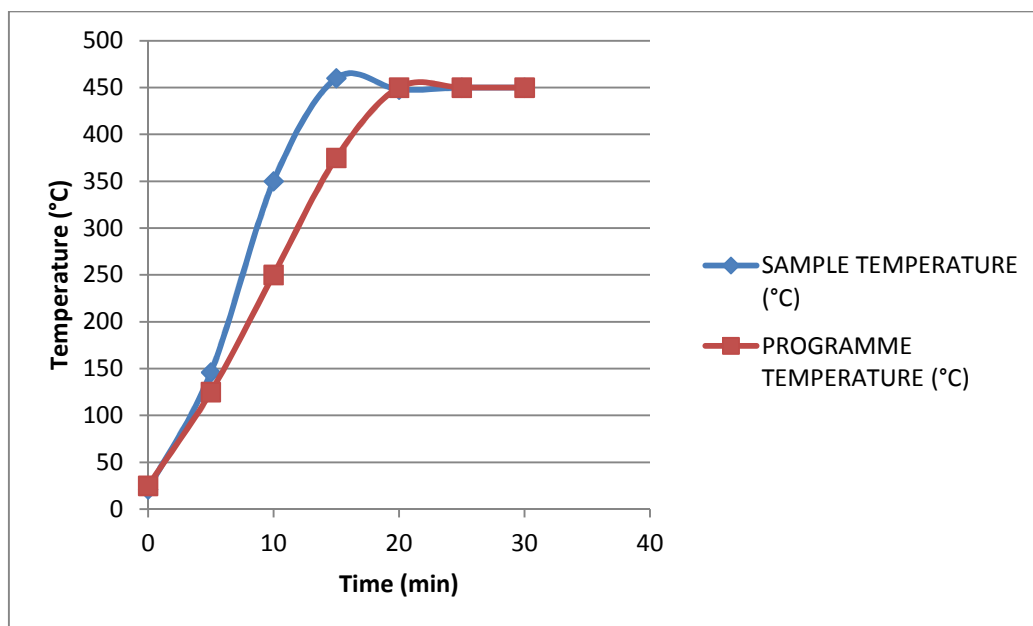


Figure 6-2. Temperature profiles for a typical BRH sample in the primary reactor

6.2.2 Mass balance and product yield

The mass balance was done carefully throughout the experiment. The mass balance sheet can be found in Appendix C. All the glassware apparatus were weighed before and after each pyrolysis experiment. Prior to weighing, the glasswares were ensured to be cleaned and dry. The liquid bio-oil and solid char yield can be obtained by difference before and after pyrolysis. For a typical pyrolysis run, the primary and secondary reactor quartz tubes contain the char, and the condensers and transition tube contain the bio-oils. The non-condensable gases were obtained by difference and the gas composition normalised.

6.2.3 Gas composition

A gas injection is taken from the sampling line at a specific temperature to determine the composition of the uncondensed gases using a gas chromatography-thermal conductivity detector (GC-TCD). The gases analysed were generated after quenching the liquid fraction of the bio-oil. The GC used was HP 5890 Series II Gas Chromatograph with a 60/80 Carboxen-1000, 15' x 1/8" SS (2.1mm I.D) column. Helium is used as the carrier gas with a flowrate of 30 ml/min, and the calibration gases is a mixture of permanent gases which consists of hydrogen (H_2), nitrogen (N_2), methane (CH_4), carbon monoxide (CO) and carbon dioxide (CO_2). A volume of 100 μ l was injected at a single run. The initial oven temperature was held at 35°C for 5 minutes, and then ramped up to 225°C at a rate of 20°C/min.

6.3 Non-catalytic pyrolysis experimental results and discussion

This section discusses and examines the results for the non-catalytic runs for BRH, as well as the characterisation of the pyrolysis bio-oil for wet and dry BRH sample respectively.

6.3.1 Mass balance

Pyrolysis experiments were done on BRH with wet (W), wet and ground (WG), and dry and ground (DG) basis. Table 1 shows the mass balance summary for the non-catalytic pyrolysis of BRH.

Table 6-1. Mass balance summary for non-catalytic runs

Run Name	Units	W	WG	DG
Particle size	Um	> 1000	355-850	355-850
Biomass moisture content	wt %	9.46	8.55	1.18
Feed bed height	cm	15	10	10
Nitrogen gas flow	cm3/min	50	50	50
Pyrolysis temperature	°C	450	450	450
Pyrolysis temperature heating rate	°C/min	25	25	25
Average secondary bed temperature	°C	513	485	488
Product yield	wt % ar basis			
LIQUID		42.17	37.08	39.61
Bottom phase (organic phase)	% of liquid	10.90	7.48	-
Upper phase (aqueous phase)	% of liquid	89.10	92.33	-
CHAR		39.38	40.49	41.92
GASES		18.45	22.43	18.47
H ₂		-	-	-
CH ₄		1.27	1.48	2.06
CO		20.98	13.35	9.14
CO ₂		65.27	73.05	75.4

A liquid bio-oil yield of up to 40 wt. % was recorded for the non-catalytic experiments. The pyrolysis conditions can therefore be classified as intermediate pyrolysis due to the moderate temperature used (450°C) and yield comparable to the patented Haloclean process [80]. A study by Tsai et al. which used a fixed-bed reactor on rice husk pyrolysis also showed a liquid yield of about 40 wt. % for temperatures of 500 to 800°C [74].

The wet BRH sample, either ground or unground show signs of phase separation into two layers and separated via a simple decanting process. The liquid yield decreases and the gas yield increases when the rice husks are ground i.e. smaller particle sizes, showing a similar pattern with the study by Natarajan and Ganapathy [76]. This was due to the difference in the bed height in the primary reactor, which was not addressed by the authors. The bed height varies as to contain 100g of BRH sample, altering the freeboard volume which affected the vapour residence time. A longer vapour residence time lead to more secondary reactions, thus a higher gas yield for WG run compared to W run. Based on the analysis of the liquid sample, about 11 wt. % of the total liquid is at the bottom phase. This value decreased to 7.50 wt. % when the wet feedstock is ground. The demarcations of bio-oil layers from wet samples were clearly seen as compared to the dry sample (Figure 6-3).

For the dry and ground BRH sample, the liquid does not appear to show any clear phase separation. The dry sample produces a semi-homogenous bio-oil, which can be analysed as a whole. It is therefore preferable to dry the feedstock beforehand to minimize the water content in the bio-oil. An increase in the biomass moisture content (from 1.18% to 9.46 %) resulted in the separation of both into organic and aqueous layers. This is in agreement with Lehto et al [158], which stated that a two-phase product with a larger aqueous phase and viscous oily phase may be produced if high-moist (> 10 wt%) feedstock is used. Essentially, the dry feedstock samples are preferred due to the homogeneity of the liquid sample and therefore a suitable representation to compare with other bio-oils from pyrolysis experiments.

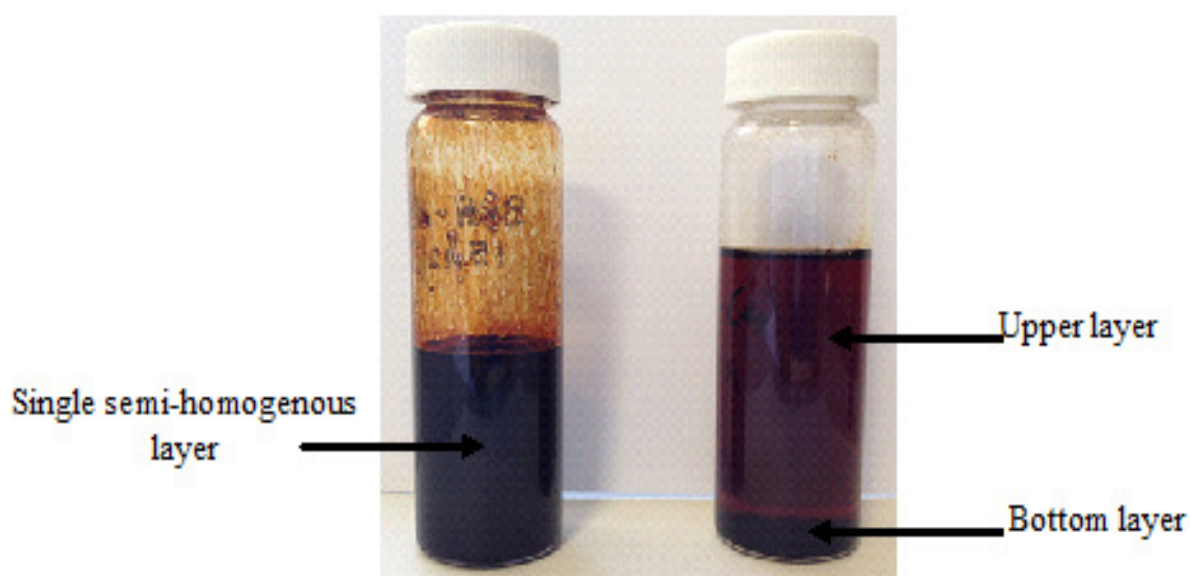


Figure 6-3. Pyrolysis bio-oil from dry BRH feedstock (left) and wet BRH feedstock (right)

The mass balance for the char yield (40 wt. %) is consistent and comparable due to the invariable pyrolysis conditions in the fixed-bed primary reactor. The char yield is quite high due to the high ash content (14.83 %) in BRH, compared to other feedstocks, such as brewer's spent grain which has a char yield of 29% with an ash content of 4.50 % [42], and beech trunkwood with 33.7 % char yield and an ash content of 7.40 % [159].

Apart from nitrogen, the gases analysed from the GC-TCD contained various concentrations of methane, carbon monoxide and carbon dioxide. The composition of the gases was shown to contain mostly carbon dioxide. A comparison between the ground samples compared to the ungrounded sample show that there is an increase in the methane and carbon dioxide, but a decrease in the carbon monoxide composition.

6.3.2 Characterisation of wet BRH bio-oil

The characterisation of bio-oil from the wet pyrolysis of BRH is discussed in this section. Since the BRH pyrolysis bio-oils from the wet sample produced two layers, each layer were characterised separately. Limitations on the sample size especially the bottom layer restricted some of the characterisation to be performed.

6.3.2.1 Acidity, water content and HHV

Table 6-2 shows the chemical properties of bio-oil from the pyrolysis of BRH. The analysis of the wet bio-oil sample (W) shows that the bottom layer is slightly less acidic than the top layer. Values for the acid number for the top phase are around 39 mg KOH/g, and for the bottom organic phase is around 25 mg KOH/g. The pH values also show a difference, with a pH of 2.96 for the top aqueous phase, and 3.36 for the bottom phase. As for the ground and wet bio-oil sample (WG), the pH for the top layer can be observed to be almost similar, but the bottom layer to be more acidic. This was also observed by Li et. al, where the pyrolysis of rice husk produced two layers, which the top layer has a pH of 2.89, and the less acidic bottom layer with 3.81[81].

Table 6-2. Chemical properties of bio-oil from the pyrolysis of wet BRH

Phase	W		WG	
	Top	Bottom	Top	Bottom
Acid number (mg KOH/g)	38.50	24.99	n/a	n/a
pH	2.96	3.36	2.98	3.18
HHV - wet (MJ/kg)	n/a	24.93	n/a	n/a
Water content (%)	71.43	18.53	73.23	12.84

n/a: not available

The heating value using a bomb calorimeter can only be analysed from the bottom phase of the bio-oil where most of the combustible organics are. A HHV of 24 MJ/kg is obtained from the bottom phase of the wet sample. The upper phase for the bio-oil from the wet BRH is non-combustible in the bomb calorimeter, which is due to the presence of high water content.

The Karl-fisher titration shows that for the wet feedstocks for BRH, the top phase is above 70% water content, when compared to the bottom phase of roughly below 20% water content. A study by Song et. al also confirms the high amount of water present in the upper layer as compared to the bottom layer, when the bio-oil was separated by adding a salt solution [160].

This shows that most of the organics are present in the bottom layer, proving that water is not completely miscible with the bio-oil. The water content decreased for the ground and wet bottom layer (WG) which showed that there is an increase in the organic content.

6.3.2.2 GC-MS analysis

The GC-MS analysis was done for both the upper and lower layer of WG pyrolysis bio-oil. Figure 6-4 and Figure 6-5 shows the labelled chromatograph for wet-BRH upper and bottom phase of BRH bio-oil. Table 6-3 and Table 6-4 show the corresponding selected chemicals and average peak area for the wet-BRH upper and bottom phase of BRH bio-oil.

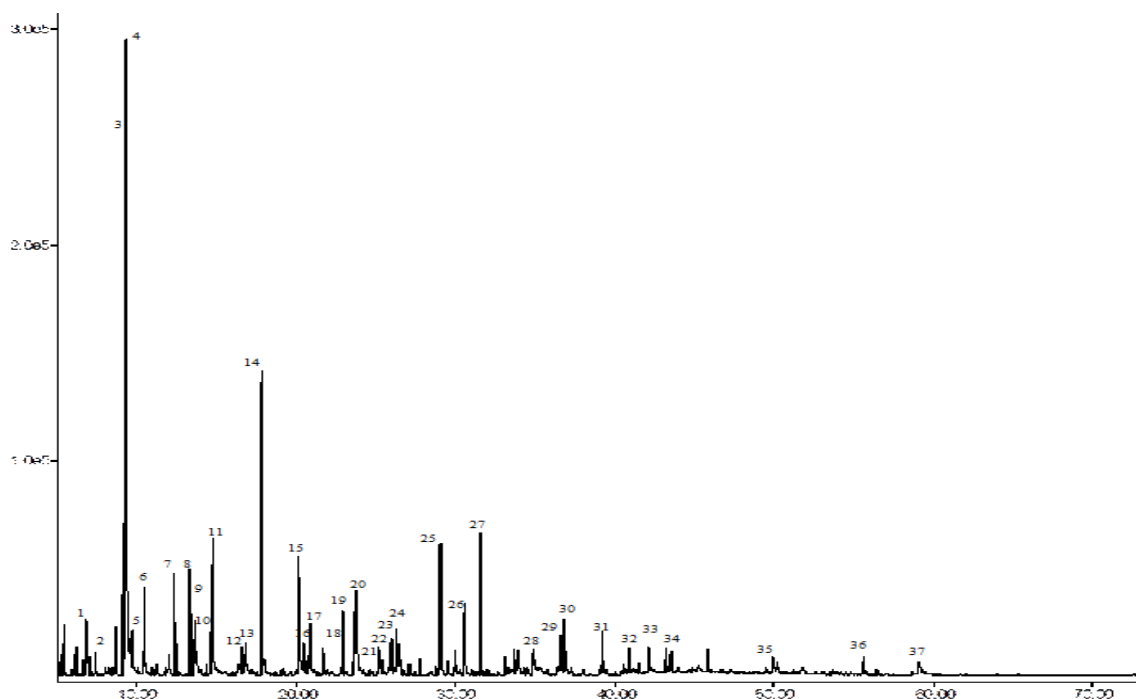


Figure 6-4. A typical chromatograph of wet-BRH upper layer

Table 6-3. Selected chemicals and average peak area for the upper layer of wet-BRH bio-oil

Peak	RT	Chemical name	Average Peak Area (%)	Chemical Formula	RMM	Chemical Group
1	6.802	Methyl acetate / Acetic acid, methyl ester	1.345	C ₃ H ₆ O ₂	74.08	Esters
2	8.654	3-Penten-2-one, (E)-	0.895	C ₅ H ₈ O	84.12	Ketones
3	9.194	1,1-diethoxy-ethane	4.265	C ₆ H ₁₄ O ₂	118.2	Misc. Oxygenates
4	9.286	Acetic Acid	14.225	C ₂ H ₄ O ₂	60.05	Organic acids
5	9.700	2,3-pentanedione	1.215	C ₅ H ₈ O ₂	100.12	Ketones
6	10.505	2-hydroxymethyl, cyclopropacarbonic acid-1, methyl ester	2.49	-	-	Esters
7	12.344	1,1-diethoxypropane	1.975	C ₇ H ₁₆ O ₂	132.2	Misc. Oxygenates
8	13.322	a-butyl-cyclopropanemethanol	2.17	C ₈ H ₁₆ O	128.2	Alcohols
9	13.609	Propanoic acid	2.63	C ₃ H ₆ O ₂	74.08	Organic acids
10	14.563	Cyclopentanone	0.955	C ₅ H ₈ O	84.12	Ketones
11	14.747	1-hydroxy-2-butanone	3.155	C ₄ H ₈ O ₂	88.11	Ketones
12	16.633	2-furanol, tetrahydro-2-methyl-	0.705	C ₅ H ₁₀ O ₂	102.13	Alcohols
13	16.794	3-propoxy-1-propene	0.895	C ₆ H ₁₂ O	100.16	Misc. Oxygenates
14	17.829	Furfural	8.325	C ₅ H ₄ O ₂	96.09	Furans
15	20.163	2-furanmethanol	3.89	C ₅ H ₆ O ₂	98.10	Alcohols
16	20.887	2-methyl-2-cyclopenten-1-one	1.125	C ₆ H ₈ O	96.13	Ketones
17	21.657	2-Furyl Methyl Ketone	0.885	C ₆ H ₆ O ₂	110.11	Ketones
18	22.956	2-hexene-1-ol, acetate	1.10	C ₈ H ₁₄ O ₂	142.20	Misc. Oxygenates
19	23.646	2,5-diethoxytetrahydrofuran	1.205	C ₈ H ₁₆ O ₃	160.21	Misc. Oxygenates
20	23.761	1,2-cyclopentanedione AND 2-hydroxy-2-cyclopenten-1-one	3.055	C ₅ H ₆ O ₂	98.10	Ketones

21	25.175	5-Methylfurfural	0.68	C ₆ H ₆ O ₂	110.11	Furans
22	25.980	3-Methyl-2-Cyclopentenone	1.09	C ₆ H ₈ O	96.13	Ketones
23	26.337	2(5H)-Furanone	0.985	C ₄ H ₄ O ₂	84.07	Furans
24	26.463	Tetrahydro-2-furanmethanol	0.935	C ₅ H ₁₀ O ₂	102.13	Alcohols
25	29.062	3-methyl-1,2-cyclopentanedione	4.5	C ₆ H ₈ O ₂	112.13	Ketones
26	30.579	Phenol	2.405	C ₆ H ₆ O	94.11	Phenols
27	31.626	Guaiacol	3.805	C ₇ H ₈ O ₂	124.14	Guaiacols
28	34.856	p-Cresol	0.79	C ₇ H ₈ O	108.14	Phenols
29	36.558	3-buten-2-ol	1.49	C ₄ H ₈ O	72.11	Alcohols
30	36.834	p-cresol	1.35	C ₈ H ₁₀ O ₂	138.17	Guaiacols
31	39.168	4-Ethylphenol	1.34	C ₈ H ₁₀ O	122.16	Phenols
32	40.927	4-Ethylguaiacol	0.65	C ₉ H ₁₂ O ₂	152.19	Guaiacols
33	42.111	1,4:3,6-dianhydro- α -d-glucopyranose	0.955	C ₆ H ₈ O ₄	144.13	Anhydrosugars
34	43.215	o-Coumaric acid	0.79	C ₉ H ₈ O ₃	164.16	Organic acids
35	49.918	Hydroquinone / 1,4-benzenediol	0.81	C ₆ H ₆ O ₂	110.11	Phenols
36	55.621	1-(4-hydroxy-3-methoxyphenyl)-2-propanone / Vanillyl methyl ketone	0.525	C ₁₀ H ₁₂ O ₃	180.20	Guaiacols
37	59.059	Levogluconan	1.20	C ₆ H ₁₀ O ₅	162.14	Anhydrosugars

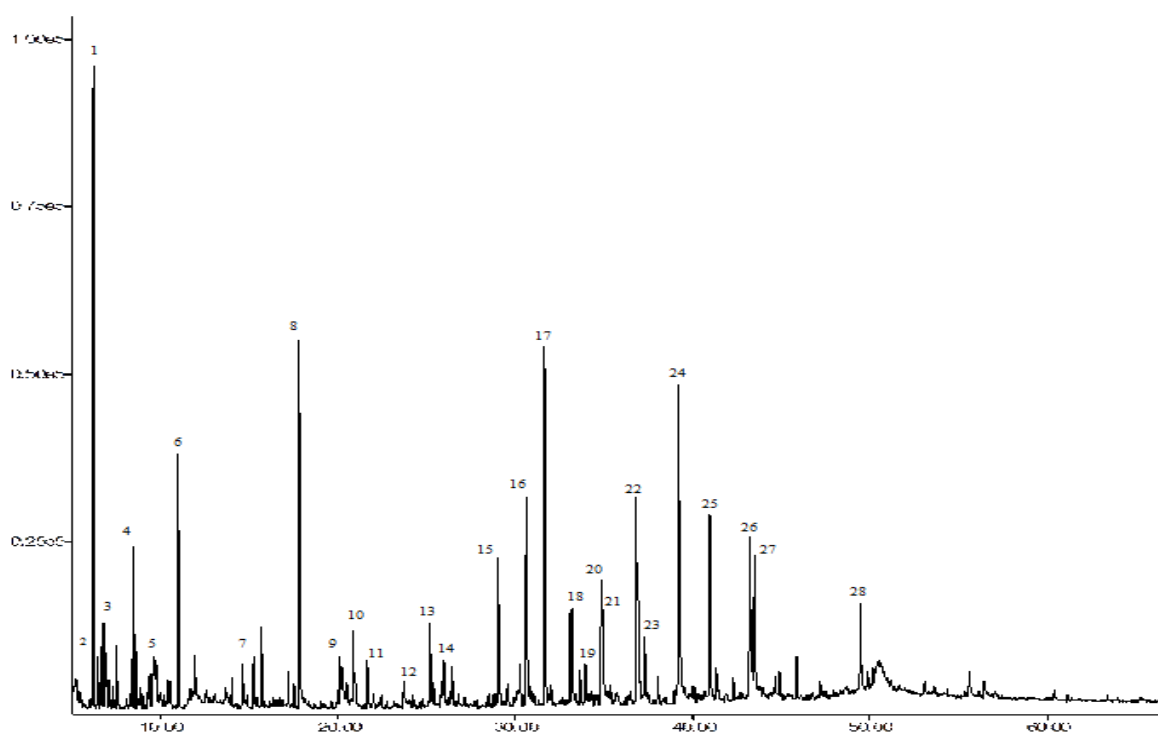


Figure 6-5. Chromatograph of a typical wet-BRH bio-oil bottom layer

Table 6-4. Selected chemicals and average peak area from the wet-BRH bottom layer

Peak	RT	Chemical name	Average Peak Area (%)	Chemical Formula	RMM	Chemical Group
1	6.185	2-methylfuran / Sylvan	4.665	C ₅ H ₆ O	82.10	Furans
2	6.645	1,3-cyclohexadiene	0.86	C ₃ H ₆ O ₂	74.08	Esters
3	6.806	1-methyl-1,3-cyclopentadiene	1.105	C ₄ H ₈ O ₂	88.11	Esters
4	8.507	2,5-Dimethylfuran	1.69	C ₆ H ₈ O	96.13	Furans
5	9.703	2,3-pentanedione	1.05	C ₅ H ₈ O ₂	100.12	Ketones
6	10.991	Toluene	3.07	C ₇ H ₈	92.14	Aromatic Hydrocarbon
7	15.682	m-Xylene	0.97	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon
8	17.820	Furfural	6.34	C ₅ H ₄ O ₂	96.09	Furans
9	20.166	2-furanmethanol	1.41	C ₅ H ₆ O ₂	98.10	Alcohols
10	20.902	2-Cyclopenten-1-one, 2-methyl-	1.225	C ₆ H ₈ O	96.13	Ketones
11	21.683	2-Furyl Methyl Ketone	0.985	C ₆ H ₆ O ₂	110.11	Ketones
12	23.753	1,2-cyclopentanedione	0.735	C ₅ H ₆ O ₂	98.10	Ketones
13	25.202	5-Methylfurfural	1.74	C ₆ H ₆ O ₂	110.11	Furans
14	25.995	3-Methyl-2-Cyclopentenone	0.985	C ₆ H ₈ O	96.13	Ketones
15	29.053	2-cyclopenten-1-one, 2-hydroxy-3-methyl / Maple Lactone	3.25	C ₆ H ₈ O ₂	112.13	Ketones
16	30.617	Phenol	4.535	C ₆ H ₆ O	94.11	Phenols
17	31.663	Guaiacol	8.08	C ₇ H ₈ O ₂	124.14	Guaiacols
18	33.158	2-Methylphenol	2.02	C ₇ H ₈ O	108.14	Phenols
19	33.664	3-Ethyl-2-hydroxy-2-cyclopenten-1-one	0.83	C ₇ H ₁₀ O ₂	126.15	Ketones
20	34.906	p-cresol	2.65	C ₇ H ₈ O	108.14	Phenols
21	34.998	m-cresol	2.12	C ₇ H ₈ O	108.14	Phenols
22	36.860	p-cresol / 2-methoxy-p-cresol	4.51	C ₈ H ₁₀ O ₂	138.17	Guaiacols
23	37.297	2,4-Dimethylphenol	1.41	C ₈ H ₁₀ O	122.16	Phenols
24	39.217	4-Ethylphenol	8.965	C ₈ H ₁₀ O	122.16	Phenols
25	40.965	4-Ethylguaiacol	5.065	C ₉ H ₁₂ O ₂	152.19	Guaiacols
26	43.264	2-Propenoic acid, 3-(2-hydroxyphenyl)-, (E)- / o-Coumaric acid	4.715	C ₉ H ₈ O ₃	164.16	Organic acids
27	43.563	4-Ethenyl-2-methoxyphenol / p-Vinylguaiacol / 2-Methoxy-4-vinylphenol	3.225	C ₉ H ₁₀ O ₂	150.18	Guaiacols
28	49.473	Isoeugenol	2.23	C ₁₀ H ₁₂ O ₂	164.20	Guaiacols

Table 6-5. Comparison of the chemical groups between the peak areas for the top and bottom wet-BRH bio-oil

Chemical Groups	Top (Peak Area, %)	Bottom (Peak Area, %)
Aromatic Hydrocarbon	0.00	4.04
Organic Acids	17.65	4.715
Esters	3.84	1.965
Furans	9.99	14.435
Ketones	16.88	9.06
Alcohols	9.19	1.41
Phenols	5.35	21.70
Guaiacols	6.33	23.11
Anhydrosugars	2.16	0.00
Misc. Oxygenated	9.44	0.00
TOTAL	80.81	80.435

Table 6-5 shows the comparison between the chemical groups present from the top and bottom bio-oil from a wet BRH sample. The analysis showed that the top aqueous layer contained a high amount of organic acids, alcohols, ketones compared to the bottom organic layer. Since the top layer has a high amount of water content, it is expected that polar compounds that contain –OH group such as carboxylic acid and alcohol to be present here. Anhydrosugars, such as levoglucosan and miscellaneous oxygenated compounds were only found in the top layers, showing that they are water soluble compounds. The bottom layer contains high amount of phenols and guaiacols. The result agrees with a study by Song et. al and Li et. al which found that the upper layer contained acetic acids, alcohols and water-soluble compounds, and the bottom layer contained high lignin-derived pyrolysis products [81, 160].

The presence of high organic acid for the top layer explains the low pH value for the top layer, even though the water content is high of up to 70%. The acidity is mostly due to the presence of acetic acid by which showed a peak area of 14.2 % present from the top phase. Although the separation of the wet-BRH bio-oil was carried out by a simple decanting process, the results were comparable to a study by Chen et. al which achieved a separation of rice husk bio-oil by adding salt solutions. The upper layer of the separated rice husk bio-oil obtained by Chen et. al was found to contain 16.2% peak area of acetic acid [161].

As for the bottom layer, the chemical groups present were mostly aromatic hydrocarbon, phenols and guaiacols. Although the bottom layer did not have as much organic acids compared to the top layer, the pH was not far off above 3. This would suggest that the

acidity is derived from phenols and guaiacols which contain acidic functional groups attached to them.

6.3.3 Characterisation of dry BRH bio-oil

Characterisation of dry BRH bio-oil is discussed in this section. BRH bio-oil characterisation data is compared with values from other rice husk species in literature which can be seen in Table 6-6. For the HHV and LHV for wet basis values, even though the experimental sample is stated dry and ground, the bio-oil values obtained were considered to be wet basis due to the inclusion of water in the sample.

Table 6-6. Physicochemical properties of rice husk pyrolysis oil

Physicochemical properties	Experimental	Literature			
	DG bio-oil	Ji-lu et. al [79]	Lu et. al [157]	Heo et. al [75]	Guo et. al [162]
Acidity					
Acid number (mg KOH/g)	55.54	-	-	-	-
pH	3.00	2.80	3.20	-	3.36
Water content (%)	52.60	25.20	28.00	25.20	33.80
Kinematic Viscosity (cSt) @ 40 °C	1.68	128 (20 °C)	13.20	-	82.43
Density (kg/m ³) @ 25 °C	1065	1190	1140	-	1210
Ultimate analysis					
C (%)	23.38	41.70	39.92	55.10	35.63
H (%)	10.39	7.70	8.15	7.20	7.00
N (%)	0.51	0.30	0.61	0.70	0.00
S (%)	<0.10	0.20	0.30	-	-
O (%) *	65.63	50.30	51.02	37.00	57.37
H:C molar ratio	5.33	2.22	2.45	1.57	2.36
O:C molar ratio	2.11	0.90	0.96	0.50	1.21
Higher Heating Value (HHV)					
HHV - wet basis (MJ/kg)	13.61 **	18.42 **	16.50	23.88 **	14.75 **
HHV - dry basis (MJ/kg)	28.71 **	24.62 **	25.34 **	24.80	22.28 **
Lower Heating Value (LHV)					
LHV - wet basis (MJ/kg)	11.34 **	17.42	16.47 **	22.31 **	13.36

* By difference

** Calculated values

6.3.3.1 Acidity and water content

The dry bio-oil sample shows that it has a pH of 3. The acid number has a value of 55 mg KOH/g, which is higher than either of the top and bottom layer of the wet samples. This is likely due to the combination of acidic components which is present in previous both top and bottom layers. The values were in agreement with the rice husk pyrolysis oils from literature which showed to have a pH of around 2-3 [74, 79].

A value of 52.60 wt. % is obtained for the water content from the DG run. Rice husk pyrolysis bio-oil literature values show lower water contents of 25 – 34%. This is due to the fast pyrolysis nature for the literature values, as compared to the DG which was subjected to intermediate pyrolysis. The nature of intermediate pyrolysis tend to produce water and organics at a 50:50 basis in bio-oil liquid [30].

6.3.3.2 Viscosity and density

The density of BRH bio-oil is 1065 kg/m³ which is lower than the values from literature. Oasmaa and Peacocke reported that density of pyrolysis liquid is a function of the water content [163]. Since about 50% of the bio-oil is water, it would suggest that the density of water of 998 kg/m³ [164] in BRH bio-oil has an effect on the density of the bio-oil.

The viscosity of the BRH-oil is low with 1.68 cSt, when compared to literature values for rice husk pyrolysis oils. Viscosity is greatly influenced by the water content in the sample; as the water content increases, the viscosity of the oil approaches the viscosity of water, as suggested by Nolte and Liberatore [165].

6.3.3.3 Elemental analysis and HHV

Elemental analysis for dry-BRH bio-oil can be found in table 6-6. The carbon content of 22.38% for BRH bio-oil is lower compared to other rice husk bio-oils with 40-55%. The fact that the bio-oil contained high water content might have had an influence on the values, due to the higher hydrogen and oxygen contents compared to other rice husk values. The sulphur content is insignificant, and a low nitrogen value of 0.51% was obtained.

The H:C and O:C molar ratios was calculated for DG bio-oil sample and the literature samples. DG bio-oil molar ratios were found to be very high as compared to the literature

values, which were considered due to the high water content in the DG sample. A H:C molar ratio of greater than 2 is possible and occurs frequently in pyrolysis oil when the ratio was calculated with an as-received basis [166]. This can be seen for all the pyrolysis oil, except for the values of Heo et al. which was calculated to be 1.57. The initial deduction was due to the difference in the water content, but this was nullified due to similar water content with the bio-oil samples of Ji-lu et al. Although the temperature for the reaction condition is similar, this may be due to the difference in the thermochemical properties of rice husk which showed a higher volatile content for Heo et. al. Another possible cause was due to the difference in the purge gas and the condensation medium.

Since the heating values for the bio-oil for DG bio-oil was not able to be determined in the bomb calorimeter, an alternative way to obtain the heating values is by using correlations from the elemental analysis of the bio-oils which can be found in Chapter 4, equation 4-4. The calculated HHV in wet basis was expected to be low with a value of 13.61 MJ/kg, as compared to around 15-24 MJ/kg from literature. However, the calculated HHV value in dry basis of 28.71 MJ/kg was calculated for the DG bio-oil. The values were comparable with the literature.

6.3.3.4 GC-MS analysis

The GC-MS analysis was done for dry-BRH pyrolysis bio-oil. More than 100 peaks were detected, but around 86 peaks were identified from GC-MS which can be seen in Table 6-7.

Table 6-7. Chemicals and average peak area for dry-BRH pyrolysis bio-oil

Peak	RT	Chemical Name	Peak Area %	Chemical Formula	RMM	Chemical Group
1	6.103	2-methylfuran / Sylvan	0.44	C ₅ H ₆ O	82.10	Furans
2	6.735	Methyl acetate / Acetic acid, methyl ester	0.71	C ₃ H ₆ O ₂	74.08	Esters
3	7.023	Methyl propionate / Propanoic acid, methyl ester	0.17	C ₄ H ₈ O ₂	88.11	Esters
4	7.448	Benzene	0.15	C ₆ H ₆	78.11	Aromatic Hydrocarbon
5	8.414	2,5-Dimethylfuran	0.36	C ₆ H ₈ O	96.13	Furans
6	8.598	3-pentene-2-one, (E)-	0.59	C ₅ H ₈ O	84.12	Ketones
7	9.104	Acetic Acid	10.74	C ₂ H ₄ O ₂	60.05	Organic acids
8	9.621	2,3-pentanedione	0.59	C ₅ H ₈ O ₂	100.12	Ketones
9	10.323	Methyl urea	1.19	C ₂ H ₆ N ₂ O	74.08	Nitrogen-containing compounds
10	10.426	2-methoxytetrahydrofuran	0.42	C ₅ H ₁₀ O ₂	102.13	Furans
11	10.875	Toluene	0.70	C ₇ H ₈	92.14	Aromatic Hydrocarbon
12	11.587	Pyridine	0.22	C ₅ H ₅ N	79.10	Nitrogen-containing compounds
13	11.886	3-penten-2-one / Methyl propenyl ketone	0.29	C ₅ H ₈ O	84.12	Ketones
14	13.462	Propanoic acid	1.32	C ₃ H ₆ O ₂	74.08	Organic acids

15	14.462	Cyclopentanone	0.52	C ₅ H ₈ O	84.12	Ketones
16	14.588	1-hydroxy-2-butanone	2.06	C ₄ H ₈ O ₂	88.11	Ketones
17	15.152	Ethylbenzene & p-xylene	0.18	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon
18	15.313	2,2-dimethyl-3-hexanol	0.19	C ₈ H ₁₈ O	130.23	Alcohols
19	15.543	m-Xylene	0.24	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon
20	16.462	2-furanol, tetrahydro-2-methyl-	0.28	C ₅ H ₁₀ O ₂	102.13	Alcohols
21	16.635	3-propoxy-1-propene	0.64	C ₆ H ₁₂ O	100.16	Misc. Oxygenates
22	17.026	2,5-furandione / Maleic Anhydride	0.21	C ₄ H ₂ O ₃	98.06	Furans
23	17.716	Furfural	6.54	C ₅ H ₄ O ₂	96.09	Furans
24	17.900	Tetrahydro-2,5-dimethoxyfuran	0.48	C ₆ H ₁₂ O ₃	132.16	Furans
25	20.027	2-furanmethanol	3.80	C ₅ H ₆ O ₂	98.10	Alcohols
26	20.360	1-(acetyloxy)-2-propanone / Acetol acetate	0.58	C ₅ H ₈ O ₃	116.12	Misc. Oxygenates
27	20.601	2-ethylhexanal	0.61	C ₈ H ₁₆ O	128.21	Aldehydes
28	20.774	2-Cyclopenten-1-one, 2-methyl-	0.89	C ₆ H ₈ O	96.13	Ketones
29	21.544	2-Furyl Methyl Ketone	0.71	C ₆ H ₆ O ₂	110.11	Ketones
30	22.660	2-hexene-1-ol, acetate	0.23	C ₈ H ₁₄ O ₂	142.20	Misc. Oxygenates
31	23.614	1,2-cyclopentanedione	2.50	C ₅ H ₆ O ₂	98.10	Ketones
32	25.040	5-methyl-2-furancarboxaldehyde / 5-methylfurfural	0.76	C ₆ H ₆ O ₂	110.11	Furans
33	25.140	2,3-pentanedione / Acetyl acetone	0.61	C ₅ H ₈ O ₂	100.12	Ketones
34	25.292	2-butanone, 1-(acetyloxy)-	0.33	C ₆ H ₁₀ O ₃	130.14	Misc. Oxygenates
35	25.660	2,3-dimethyl-2-cyclopenten-1-one	0.24	C ₇ H ₁₀ O	110.16	Ketones
36	25.833	3-Methyl-2-Cyclopentenone	0.97	C ₆ H ₈ O	96.13	Ketones
37	26.189	2(5H)-Furanone	1.34	C ₄ H ₄ O ₂	84.07	Furans
38	26.327	Tetrahydro-2-furanmethanol	0.63	C ₅ H ₁₀ O ₂	102.13	Alcohols
39	26.994	5-hexen-2-one	0.36	C ₆ H ₁₀ O	98.14	Ketones
40	27.626	2,2-diethyl-3-methyl-oxazolidine	0.55	C ₈ H ₁₇ NO	143.23	Nitrogen-containing compounds
41	28.684	3-methyl-2(5H)-Furanone	0.32	C ₅ H ₆ O ₂	98.10	Furans
42	28.914	3-methyl-1,2-cyclopentanedione AND 2-cyclopenten-1-one, 2-hydroxy-3-methyl / Maple Lactone / Corylon	4.18	C ₆ H ₈ O ₂	112.13	Ketones
43	29.374	2,5-dihydro-3,5-dimethyl-2-furanone	0.44	C ₆ H ₈ O ₂	112.13	Furans
44	29.742	3,4-dimethyl-2-hydroxycyclopent-2-en-1-one	0.18	C ₇ H ₁₀ O ₂	126.15	Ketones
45	30.443	Phenol	2.97	C ₆ H ₆ O	94.11	Phenols
46	31.490	Guaiacol	6.41	C ₇ H ₈ O ₂	124.14	Guaiacols
47	31.881	3-ethyl-2-cyclopenten-1-one	0.30	-	-	Ketones
48	32.984	2-Methylphenol / o-cresol	0.90	C ₇ H ₈ O	108.14	Phenols
49	33.134	Formic acid,2-propenyl ester / Allyl formate	0.21	C ₄ H ₆ O ₂	86.09	Esters
50	33.490	3-ethyl-2-hydroxy-2-cyclopenten-1-one	0.77	C ₇ H ₁₀ O ₂	126.15	Ketones
51	33.674	Maltol / Larixic acid	0.44	C ₆ H ₆ O ₃	126.11	Organic acids
52	34.157	4-methyl-4-Hepten-3-one	0.20	C ₈ H ₁₄ O	126.20	Ketones
53	34.341	4-Methyl-5H-Furan-2-one	0.26	C ₅ H ₆ O ₂	98.10	Furans
54	34.720	p-cresol	1.58	C ₇ H ₈ O	108.14	Phenols
55	34.812	m-Cresol	0.91	C ₇ H ₈ O	108.14	Phenols
56	35.192	4-ethyl-1,3-benzenediol	0.46	C ₈ H ₁₀ O ₂	138.16	Phenols
57	35.629	3-methyl-4-hexen-2-one	0.23	C ₇ H ₁₂ O	112.17	Ketones
58	36.411	3-buten-2-ol	1.36	C ₄ H ₈ O	72.11	Alcohols
59	36.698	p-cresol / 2-methoxy-p-cresol	3.26	C ₈ H ₁₀ O ₂	138.17	Guaiacols
60	36.836	2-ethylphenol	0.32	C ₈ H ₁₀ O	122.16	Phenols
61	37.100	2,4-Dimethylphenol / 2,4-xlenol	0.71	C ₈ H ₁₀ O	122.16	Phenols
62	37.859	2-cyclopenten-1-one, 4-hydroxy-3-methyl-2-(2-propenyl)- / Allethrolone	0.32	C ₉ H ₁₂ O ₂	152.19	Misc. Oxygenates
63	38.871	2,3-dimethylphenol / 2,3-xlenol OR 2,5-dimethylphenol / 2,5-xlenol	0.22	C ₈ H ₁₀ O	122.16	Phenols
64	39.020	4-Ethylphenol	2.78	C ₈ H ₁₀ O	122.16	Phenols
65	40.251	3,4-dimethylphenol / 3,4-Xlenol	0.20	C ₈ H ₁₀ O	122.16	Phenols
66	40.412	2-nonene-1-ol	0.27	C ₉ H ₁₈ O	142.24	Alcohols
67	40.550	1-cyclohexyl-2-buten-1-ol (c,t)	0.22	C ₁₀ H ₁₈ O	154.25	Alcohols

68	40.780	4-Ethylguaiacol	2.27	C ₉ H ₁₂ O ₂	152.19	Guaiacols
69	41.182	4-ethyl-2-methyl-phenol	0.25	C ₉ H ₁₂ O	136.19	Phenols
70	41.331	3,4-anhydro-d-galactosan OR Anhydro-d-mannosan OR 2,3-anhydro-d-galactosan	0.45	C ₆ H ₈ O ₄	144.13	Anhydrosugars
71	41.952	1,4:3,6-dianhydro-α-d-glucopyranose	0.85	C ₆ H ₈ O ₄	144.13	Anhydrosugars
72	43.056	2-Propenoic acid, 3-(2-hydroxyphenyl)- , (E)- / o-Coumaric acid	3.58	C ₉ H ₈ O ₃	164.16	Organic acids
73	43.378	4-Ethenyl-2-methoxyphenol / p- Vinylguaiacol / 2-Methoxy-4- vinylphenol	2.54	C ₉ H ₁₀ O ₂	150.18	Guaiacols
74	44.551	4-allyl-2-methoxyphenol / Eugenol / Caryophyllilic acid	0.35	C ₁₀ H ₁₂ O ₂	164.20	Guaiacols
75	44.723	2-methoxy-4-propylphenol / Cerulignol	0.44	C ₁₀ H ₁₄ O ₂	166.22	Phenols
76	45.080	5-oxotetrahydrofuran-2-carboxylic acid, ethyl ester	0.44	C ₇ H ₁₀ O ₄	158.15	Misc. Oxygenates
77	45.689	2,6-Dimethoxyphenol / Syringol	1.18	C ₈ H ₁₀ O ₃	154.17	Syringols
78	49.276	Isoeugenol	1.53	C ₁₀ H ₁₂ O ₂	164.20	Guaiacols
79	49.748	Hydroquinone / 1,4-benzenediol	1.12	C ₆ H ₆ O ₂	110.11	Phenols
80	50.035	Isovanillin	0.49	C ₈ H ₈ O ₃	152.15	Guaiacols
81	51.610	2-methyl-1,4-benzenediol / 2,5- toluenediol	0.28	C ₇ H ₈ O ₂	124.14	Phenols
82	53.473	1-(4-hydroxy-3-methoxyphenyl)- ethanone / Acetovanillone	0.41	C ₉ H ₁₀ O ₃	166.17	Guaiacols
83	55.462	1-(4-hydroxy-3-methoxyphenyl)-2- propanone / Guaiacylacetone / Vanillyl methyl ketone	0.76	C ₁₀ H ₁₂ O ₃	180.20	Guaiacols
84	56.267	3,4-dihydrocoumarin-6-ol	0.33	-	-	Misc. Oxygenates
85	58.854	Levogluconan	2.35	C ₆ H ₁₀ O ₅	162.14	Anhydrosugars
86	60.268	4-Allyl-2,6-dimethoxyphenol OR Methoxyeugenol	0.24	C ₁₁ H ₁₄ O ₃	194.23	Syringols

Table 6-8. Chemical groups and the peak areas for dry BRH bio-oil

Chemical Groups	Peak Areas (%)
Aromatic Hydrocarbon	1.27
Organic Acids	16.06
Esters	1.08
Furans	11.55
Aldehydes	0.61
Ketones	16.14
Alcohols	6.74
Phenols	13.12
Guaiacols	18.00
Syringols	1.41
Anhydrosugars	3.65
Misc. Oxygenated	2.85
Nitrogen-containing compounds	1.96
TOTAL	94.41

Table 6-7 shows a more thorough selection of chemicals detected from dry BRH bio-oil, with syringols and nitrogen-containing compounds added into the chemical group list. These

chemical compounds are also detected in other pyrolysis bio-oils. Majority of the chemical groups found in the bio-oil are organic acids, furans, ketones, phenols and guaiacols which can be seen from Table 6-8.

The aromatic hydrocarbon detected consists of benzene, toluene and xylenes. The aromatics present in the non-catalytic runs are most likely due to the presence of alkali metals in the feedstock itself, which has a catalytic effect on its own during pyrolysis. Toluene was detected with a peak area of 0.70 %, benzene with 0.15%, ethylbenzene or p-xylene with 0.18% and m-xylene with 0.24 %. Polyaromatic hydrocarbons (PAH) were not detected in the bio-oil, compared to other rice husk bio-oil from literature [53], which might be due to their nature of fast pyrolysis conditions, i.e. short residence time and higher temperatures.

Other notable chemicals present in the oils are acetic acid (10.74%), furfural (6.54%), phenol (2.97%), guaiacol (6.41%) and levoglucosan (2.35%).

6.4 Summary

The separation of the bio-oil phases derived from the pyrolysis of wet BRH, gives the advantage of reducing the acidity of the bio-oil by removing the upper layer. Although that said, analysing the separate phases of the bio-oil restrict the essential characterisation analyses such as viscosity and density due to the limited quantity available, especially the bottom organic-rich phase. Therefore drying the feedstock lead to a single phase bio-oil sample, and was chosen to be the ideal representative sample for comparison in the next sequence of catalytic pyrolysis experiments. Characterisation of the bio-oil from dry-BRH was done, and compared with the values from literature. From this point onwards, the dry BRH bio-oil is referred to as non-catalytic BRH bio-oil.

7 CATALYTIC PYROLYSIS STUDIES

7.1 Introduction

This chapter discusses the results from the catalytic pyrolysis experiments of Brunei rice husks. The experimental setup is a closed-coupled catalytic pyrolysis system which upgrades the pyrolysis vapour directly in-situ after generation. Catalysts include commercial catalysts (ZSM-5, Al-MCM-41 and Al-MSU-F) and a natural catalyst – Brunei rice husk ash (BRHA), which was exploited due to the high ash content. These catalysts, bound onto a ceramic monolith using montmorillonite clay were prepared. A total of 13 experiments were executed, which includes the four main catalysts and the binder alone, two regenerated catalysts (ZSM-5 and Al-MCM-41) and six mixtures of the catalysts stacked in series. The mixtures of catalysts were denoted as ZSM-5/Al-MCM-41 or Al-MCM-41/BRHA, whereby the first catalyst mentioned would be the first catalyst to contact the pyrolysis vapour. These catalysts aim to produce bio-oil liquid with desirable qualities which would be judged from the characterisation results of the bio-oils. Various criteria were proposed for the catalytic runs which were deemed favourable for bio-oil, which includes a reduction in the acidity and maximising the aromatic hydrocarbon contents and phenols content. The selected catalyst run will be utilised for optimisation experiments in the next chapter.

7.2 Catalytic pyrolysis reactor setup and conditions

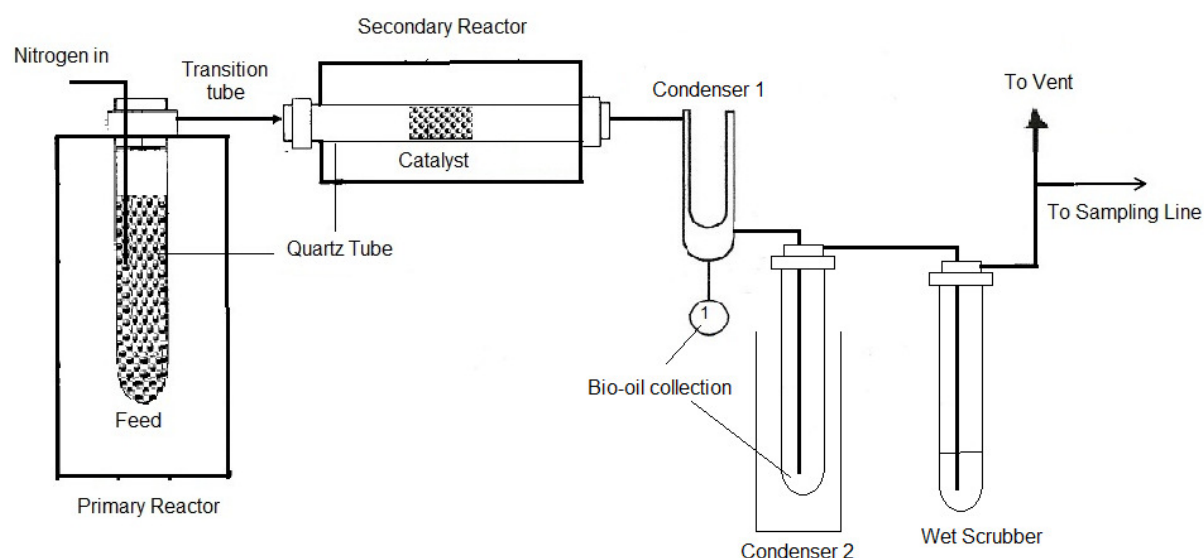


Figure 7-1. Schematic diagram of closed-coupled catalytic pyrolysis rig setup

The setup shown in Figure 7-1 and conditions for the catalytic pyrolysis was similar to the non-catalytic reactor setup in Chapter 6.2, except that the secondary reactor contained the catalyst materials. The catalyst is attached on a monolith ceramic using a binder.

Monoliths catalysts structure are used due to their excellent pressure drop to geometric surface area compared to structures such as pellets and foams, therefore ideal for small reactors [112]. Besides the advantage of low-pressure drop and uniform flow distribution, the ease of scale-up is another benefit [113]. In this study, the monolith is only used as a catalyst support and the catalysts are attached to the monolith using a binder, unlike other studies in literatures where zeolites are formed in-situ and synthesised in the honeycomb structure. Clay binders such as montmorillonite are used due to the wet binding properties and their dispersability features in aqueous suspensions during mixing. The catalysts to binder ratio should also be reasonably high, to prevent a drop in the toluene conversion, which was studied by Uguina et al. [115]. Antia and Govind concluded that low-coking zeolites such as ZSM-5 are ideally suited to monolithic reactor configuration under gaseous conditions [113].

This particular reactor setup is a closed-coupled catalytic pyrolysis system which aims to upgrade the bio-oil online directly after the pyrolysis vapours are formed from the primary fixed-bed reactor. As mentioned in the previous chapter, the catalyst-filled monolith was introduced into the secondary reactor.

7.3 Catalyst preparation

A ceramic monolith was cut into a cylindrical piece with a diameter of 18 mm and length 20 mm, which acts as a catalyst support. Four different catalysts are employed in these experiments, namely ZSM-5, Al-MCM-41, Al-MSU-F and BRHA. Commercial catalysts used in these experiments are ZSM-5 obtained from Acros Organics, while Al-MCM-41 and Al-MSU-F were obtained from Sigma-Aldrich. Brunei rice husk ash (BRHA) was obtained by ashing the rice husk at 550°C for 3 hours. A montmorillonite clay binder (K30) obtained from Sigma-Aldrich is used to attach the catalysts onto the ceramic monolith catalyst support.

The catalysts were grounded and mixed with a montmorillonite clay binder at a ratio of 3:1, and for BRHA a ratio of 2:1 was used. The catalyst and binder were stirred in HPLC grade water at 60°C for 2 hrs, to ensure the catalyst was equally dispersed. The catalyst/binder paste mixture was then coated onto the ceramic monolith support. The catalyst coated

monolith are then dried to remove moisture, and calcined at 550°C for at least 3 hrs. The catalysts were kept in a dessicator throughout to prevent moisture build up. The catalyst weight can be determined by subtracting the weight of the dry catalyst-filled monolith with the weight of the empty dry monolith. The weight of the catalysts on the cordierite support is less than 1g, resulting in a feed-to-catalyst ratio of about less than 100:1.

Regenerated catalysts were employed in the pyrolysis experiments. ZSM-5 and Al-MCM-41, which have shown to be strong catalysts, were re-used after a regeneration procedure. The coked catalysts were subjected to a temperature of 550°C for 3 hrs to remove the surface coking, and put in a dessicator until prior to pyrolysis experiments. The catalysts were utilised in the same manner as the fresh catalyst. Figure 7-2 below shows the empty monolith catalyst support, the catalyst-filled monolith before the experiment and the catalyst coking after the pyrolysis experiments.

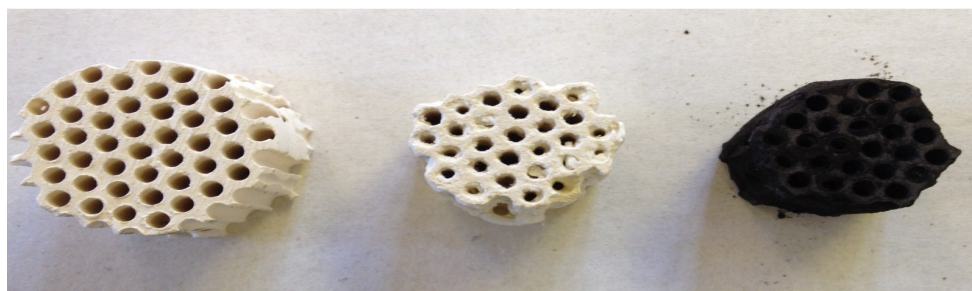


Figure 7-2. Empty monolith catalyst support (left), catalyst-filled monolith (middle) and coking on the catalyst after pyrolysis experiment (right)

7.4 Catalytic pyrolysis experiments

The procedure for the preparation of biomass was similar to Chapter 6. The moisture in the biomass was measured using a Sartorius MA35 moisture analyser prior to pyrolysis to ensure the biomass moisture was comparable. A total of 13 experiments were recorded: four different catalysts and two regenerated catalysts (ZSM-5 and Al-MCM-41), the binder only, and six combinations of the initial four catalysts. The effect of the binder towards the pyrolysis vapour was studied in this experiment. The combinations of the four catalysts were also studied, which involves stacking the monolith catalysts arrangement in series, and not physically mixing the catalysts during the catalyst preparation. The amount of catalysts for the multiple catalysts was adjusted similar to the amount present in a single monolith catalyst.

7.4.1 Mass balance summary

The mass balance for the catalytic pyrolysis experiments can be seen in Table 7-1. The run name, average catalyst bed temperature, product yield (wt. %) and gases composition were noted. The closure for the mass balance was assumed to be 100%. The average catalytic bed temperature was measured at a range of 490 to 540 °C for the various catalytic runs.

Table 7-1. Mass balance for non-catalytic and catalytic pyrolysis experiments

Run Name	Average catalytic bed temperature (°C)	Product yield (wt. %)			Gases composition (vol. %)		
		Liquid	Char	Gases ^a	CH ₄	CO	CO ₂
No Catalyst	488	39.61	41.92	18.47	2.06	9.14	75.40
Binder	523	39.97	43.26	16.77	2.71	17.60	65.89
ZSM-5	499	38.29	42.27	19.44	2.86	3.38	83.19
Al-MCM-41	531	39.98	43.15	16.87	1.72	11.28	74.20
Al-MSU-F	535	39.59	43.31	17.1	1.49	7.03	78.80
BRHA	539	38.29	42.27	19.44	4.65	7.76	76.33
ZSM-5 Regen	529	39.47	43.12	17.41	1.26	8.94	77.24
Al-MCM-41 Regen	523	39.86	42.99	17.15	3.46	15.71	67.51
ZSM-5/Al-MSU-F	517	39.74	43.18	17.08	0.56	3.38	83.08
ZSM-5/Al-MCM-41	518	39.28	42.81	17.91	0.23	1.82	85.50
Al-MSU-F/BRHA	528	39.08	43.18	17.74	2.99	10.52	74.35
Al-MCM-41/Al-MSU-F	513	38.95	43.2	17.85	2.02	12.91	72.95
ZSM-5/BRHA	529	38.85	44.06	17.09	1.43	10.88	75.02
Al-MCM-41/BRHA	532	39.74	43.22	17.04	1.51	10.19	75.55

^a by difference

The char yield is consistent due to the similar pyrolysis conditions in the fixed-bed reactor. The char value was taken as the weight of the rice husk char remained in the primary reactor and the amount of coke on the catalyst. The coke deposit on the char is calculated by subtracting the final weight of the coked monolith catalyst with the initial weight of the monolith catalysts. The amount of coke is very low as compared to the amount of BRH char, but was included in the char yield nevertheless.

The yield for liquids is found to be analogous throughout, but the most decrease was seen for ZSM-5 and BRHA in comparison with the non-catalytic run. The significant change that can be observed is the increase in the gases yield for both of the runs. Most of the gas yield for the catalytic runs decreased as compared to the non catalytic runs.

The volumetric composition of the gases is shown in Table 7-1. The composition of CO, CO₂ and CH₄ is seen to vary with the type of catalyst. Majority of the gases composition detected

was CO₂. An increase in CO₂ is seen to be more pronounced for the ZSM-5, regenerated ZSM-5, ZSM-5/Al-MSU-F and ZSM-5/Al-MCM-41 runs. This can be attributed to the decarboxylation and cracking effects of most catalyst on the pyrolysis vapours. The suppressed value of CH₄ composition for runs such as ZSM-5/Al-MCM-41 and ZSM-5/Al-MSU-F may mean that at the peak temperature of 450°C, the decarboxylation process was more distinct as compared to methane generation.

An increase in CO and a decrease in CO₂ were detected for the binder, Al-MCM-41, regenerated Al-MCM-41, Al-MSU-F/BRHA, Al-MCM-41/Al-MSU-F. This effect for Al-MCM-41 was also established by Antonakou et al. [92] and Iliopoulou et al. [93]. As for the binder, the generation of CO₂ is the lowest compared to the rest of the catalytic run which indicate less activity.

7.4.2 Pyrolysis liquid bio-oil characterisation

The catalytic pyrolysis bio-oil were characterised in the same approach as the procedures in Chapter 4 to compare with the non-catalytic pyrolysis runs. Water content, elemental analysis, heating values (HHV), acidity (pH and acid number), viscosity, density and the chemical composition using GC-MS were determined.

7.4.2.1 Water content

The water content is one of the essential analyses for assessing the bio-oil quality. The water content measured here includes the reaction water from pyrolysis and the moisture from biomass (1.50%). The drying time for the biomass was kept constant to minimise error from additional or losses of water, as biomass is one of the key sources of water.

From Table 7-2, the range of water content produced from the pyrolysis runs are from 51.48% (Binder) up to 57.44% (ZSM-5/Al-MCM-41). The catalytic runs showed an increase in the water content, except for the binder and regenerated Al-MCM-41 runs. These indicate that the catalysts are involved in the formation of water through reactions such cracking and dehydration.

Fresh catalytic BRH pyrolysis bio-oil does not show a phase separation, but will separate into two layers if left for a few weeks in storage. The ageing effect however was not studied, and only fresh bio-oil was used throughout these experiments.

Table 7-2. Water content in catalytic pyrolysis bio-oil

Run Name	Water content (%)
No Catalyst	52.60 \pm 0.51
Binder	51.48 \pm 0.60
ZSM-5	55.56 \pm 0.38
Al-MCM-41	54.66 \pm 0.40
Al-MSU-F	54.64 \pm 0.08
BRHA	55.43 \pm 0.47
ZSM-5 Regen	53.16 \pm 0.37
Al-MCM-41 Regen	52.35 \pm 0.29
ZSM-5/Al-MSU-F	57.42 \pm 0.11
ZSM-5/Al-MCM-41	57.44 \pm 0.21
Al-MSU-F/BRHA	56.96 \pm 0.35
Al-MCM-41/Al-MSU-F	55.15 \pm 0.31
ZSM-5/BRHA	53.51 \pm 0.45
Al-MCM-41/BRHA	52.71 \pm 0.32

7.4.2.2 Viscosity and Density

The change in kinematic viscosity and density of bio-oil for the catalytic runs can be seen in Table 7-3. As the viscosity of bio-oil is influenced by the water content in the sample, the viscosity values are lower when compared with the rice husk pyrolysis bio-oil from literatures. But a change in the values of the viscosity and density can be seen from the various catalysts used for upgrading. All of the values except for ZSM-5/BRHA decrease the viscosity in the bio-oil. The range of values obtained for the kinematic viscosity of the bio-oil is seen to range from 1.49 (Al-MSU-F) to 1.68 (ZSM-5/BRHA).

A higher density value for bio-oil may mean that the bio-oil contain more of the large molecular compounds. With the aid of catalysts, it is hoped that the pyrolysis vapour will break the heavy molecular compounds into smaller ones. It can be deduced that all the catalyst reduced the density of the pyrolysis bio-oil. A study done by Cao et al. showed that the density and viscosity of the bio-oil was reduced by MCM-41 and ZSM-5, but more so for the former catalyst [167]. In this study, both catalysts have shown a reduction in the viscosity and density of the bio-oil, but ZSM-5 was more pronounced compared to Al-MCM-41. A similar trend was found also for the regenerated catalysts.

The regenerated ZSM-5 was found to have a value of 1.62 cSt and 1049 kg/m³, as compared to the regenerated Al-MCM-41 with 1.65 cSt and 1050 kg/m³ for the viscosity and density respectively. The viscosity value for the oil from fresh and regenerated Al-MCM-41

was similar, as compared to the fresh and regenerated ZSM-5 which showed an increase in the viscosity from 1.55 to 1.62 cSt. This might be due to a less cracking activity of the higher molecular compounds, which might suggest a decrease in the catalyst activity.

Table 7-3. Viscosity and density for the non-catalytic and catalytic BRH bio-oil

Run Name	Kinematic Viscosity (cSt)	Density (kg/m ³) @ 25°C
No Catalyst	1.68	1065
Binder	1.66	1052
ZSM-5	1.55	1053
Al-MCM-41	1.65	1058
Al-MSU-F	1.49	1059
BRHA	1.57	1052
ZSM-5 Regen	1.62	1049
Al-MCM-41 Regen	1.65	1050
ZSM-5/Al-MSU-F	1.56	1053
ZSM-5/Al-MCM-41	1.53	1051
Al-MSU-F/BRHA	1.51	1049
Al-MCM-41/Al-MSU-F	1.67	1051
ZSM-5/BRHA	1.68	1053
Al-MCM-41/BRHA	1.63	1055

7.4.2.3 Elemental analysis and heating values

The elemental analysis, molar ratio and the HHV for the catalytic runs can be found in Table 7-4. From the elemental analysis, we can regard the sulphur values are low for BRH pyrolysis bio-oil, therefore eliminating the risks of catalyst poisoning. The nitrogen values were also low when compared to the other elements besides sulphur. All the run decreased the nitrogen, which range from 0.11 wt. % to 0.49 wt. %.

As mentioned in Chapter 6, the carbon values are low as compared to the values in the literature due to the difference in the pyrolysis type. Carbon values range from 19.99 wt. % for ZSM-5 to 33.20 wt. % for ZSM-5/BRHA. Hydrogen values range from 9.15 wt. % for Al-MCM-41/BRHA to 11.38 wt. % for ZSM-5.

The oxygen content is high when compared to other literature values due to the sample analysed in this work included the total liquid fractions, i.e. fresh bio-oil sample. Most authors compare the oxygen content of the bio-oil to explain the catalyst effectiveness of the deoxygenation process. But, the values of oxygen from the elemental analyses are quite indefinite, due to the inclusion of the oxygen value from the water present in the bio-oil from

the aqueous phase. Moreover, the water content varies with each catalyst, making it difficult to compare. The oxygen content would therefore only be comparable if the bio-oil was separated into the organic or aqueous phases.

Table 7-4. Elemental analysis, molar ratio and higher heating value (HHV) for the non-catalytic and catalytic BRH bio-oil

Run Name	Ultimate Analysis (wt. %, dry basis)					Molar ratio		HHV (MJ/kg)	
	C	H	N	S	O	OC	HC	Wet basis	Dry basis
No Catalyst	23.38	10.39	0.51	<0.10	65.63	2.11	5.33	13.61	28.71
Binder	24.26	9.75	0.19	<0.10	65.82	2.04	4.82	13.13	27.07
ZSM-5	19.99	11.38	0.41	<0.10	68.13	2.56	6.83	13.33	30.01
Al-MCM-41	22.51	11.34	0.35	<0.10	65.71	2.19	6.05	14.41	31.79
Al-MSU-F	25.63	10.67	0.49	<0.10	63.12	1.85	5.00	14.98	33.02
BRHA	31.95	10.16	0.38	<0.10	57.42	1.35	3.82	17.17	38.53
ZSM-5 Regen	24.96	10.06	0.18	<0.10	64.81	1.95	4.83	13.85	29.57
Al-MCM-41 Regen	25.58	10.17	0.20	<0.10	64.06	1.88	4.77	14.28	29.96
ZSM-5/Al-MSU-F	23.62	9.65	0.10	<0.10	66.63	2.12	4.90	12.72	29.87
ZSM-5/Al-MCM-41	21.49	9.80	0.12	<0.10	68.60	2.39	5.47	11.94	28.05
Al-MSU-F/BRHA	22.55	9.72	0.11	<0.10	67.62	2.25	5.17	12.33	28.64
Al-MCM-41/Al-MSU-F	26.20	9.53	0.11	<0.10	64.16	1.84	4.36	13.73	30.61
ZSM-5/BRHA	33.20	9.16	0.21	<0.10	57.44	1.30	3.31	16.43	35.35
Al-MCM-41/BRHA	33.19	9.15	0.18	<0.10	57.49	1.30	3.31	16.41	34.71

Therefore, an alternative method of comparison using the OC and HC molar ratio would be much more suitable in this case. A higher HC molar ratio and a lower OC ratio are favourable for fuels. HC molar ratio is an important measure of fuel quality, so a lower hydrogen contents in pyrolysis indicate a lower quality fuel oil and may require additional upgrading [166]. The comparison of biofuels (such as pyrolysis oils) and fossil fuels (such as coals) shows clearly the proportion of oxygen and hydrogen compared with carbon, reduces the energy value of a fuel, due to the lower energy contained in carbon-oxygen and carbon-hydrogen bonds, than in carbon-carbon bonds [168].

The values for HC and OC molar ratio are higher in this study as compared to literature values, which is due to the inclusion of the hydrogen and oxygen values from water. However, the values can be compared with each other due to the similar feedstock and pyrolysis conditions, i.e. temperature and purge gas. A graph of HC and OC molar ratio versus the water content is illustrated in Figure 7-3. As high HC ratio is favourable, we can analyse which catalysts are ideal in this sense. It is interesting to note that the HC and OC molar ratio values do not correlate with the water content. This may suggest that water in the

bio-oil leads to a higher molar ratio values, but do not explain the variation in the molar ratios. As the HC molar ratio was calculated with an as-received basis, a value of greater than 2 is expected and occur frequently in pyrolysis oil [166].

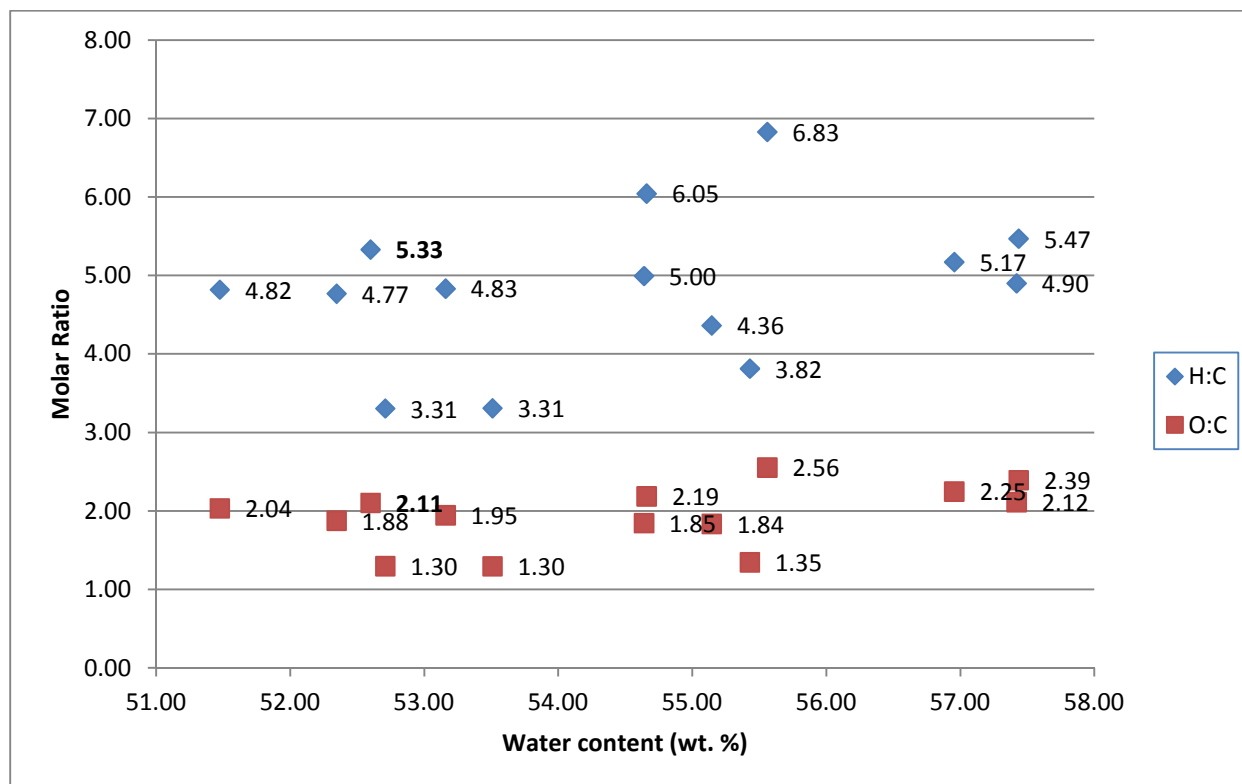


Figure 7-3. Molar ratio vs bio-oil water content

In comparison with the non-catalytic run, the HC molar ratio is seen to increase for the ZSM-5, Al-MCM-41 and ZSM-5/Al-MCM-41 runs with 6.83, 6.05 and 5.47 respectively. The increase in the value of HC suggests the addition of hydrogen into the bio-oil. But the same catalyst runs increases the OC molar ratio for the bio-oil in addition to Al-MSU-F/BRHA, and this is deemed unfavourable. This might mean that oxygen was added into the bio-oil, possibly through cracking and depolymerisation of heavy molecular compounds.

7.4.2.4 Acid number and pH

The acidity of the bio-oil may be determined by its acid number or pH. Acid number was only analysed for the non-catalytic run and the four pure unmixed catalysts. The acid number measured for non-catalytic pyrolysis oil was noticeably high with a value of 55 mg KOH/g but not unexpected. The use of catalyst reduces the value down to a range of 39-47 mg KOH/g, with ZSM-5 and BRHA having the least value. The pH of the bio-oils is noticeably acidic with

a pH range of 2.65 to 3. There seems to be a vague correlation between the acid number and pH in this case. Nolte and Liberatore also concluded there was no correlation between the pH and acid number in their work [165]. Note that in this research we have chosen to analyse the acidity from the pH values, and will not study the correlation between the acid number and pH. Most of the acidity may arise from the presence of acetic acid, but other carboxylic acids, phenols and other acidic compounds will also have a significant contribution.

From the pH values obtained here, we can notice that the upgrading of bio-oil reduces the pH. The highest pH amongst the catalytic runs, which is the less acidic bio-oil was obtained for ZSM/Al-MCM-41 with a value of 2.94, and is the closest to the non-catalytic bio-oil with a pH of 3.

Table 7-5. pH and acid number for the non-catalytic and catalytic BRH bio-oil

Runs	pH	Acid number (mg KOH/g)
No Catalyst	3.00	55.54
Binder	2.73	-
ZSM-5	2.74	39.00
Al-MCM-41	2.83	43.15
Al-MSU-F	2.69	46.74
BRHA	2.79	39.43
ZSM-5 Regen	2.75	-
Al-MCM-41 Regen	2.80	-
ZSM-5/Al-MSU-F	2.65	-
ZSM-5/Al-MCM-41	2.94	-
Al-MSU-F/BRHA	2.80	-
Al-MCM-41/Al-MSU-F	2.74	-
ZSM-5/BRHA	2.80	-
Al-MCM-41/BRHA	2.79	-

7.4.2.5 GC-MS analysis

The effect of catalysis on the individual chemical composition of the BRH pyrolysis bio-oils may be studied using the GC-MS. From the chromatograms, 102 peaks were identified and analysed. The chemical compounds and group, retention times, chemical formula, relative molecular mass (RMM) may be found from Table 7-6. Compared to the previous non-catalytic bio-oil in table 6-7 from the Chapter 6, we have identified more chemical compounds such as 3-methylbutanal (#5), 2-methyl-3-pentanone (#9), o-xylene (#24),

styrene (#26), cyclohexanone (#29), trimethylbenzenes (#35), 2-hydroxybenzaldehyde (#47), trimethylphenols (#70), dimethoxytoluene (#73), 1-indanone (#81), 3-ethyl-5-methylphenol (#82), trans-m-propenyl guaiacol (#89), 2,6-dimethoxybenzaldehyde (#90), chavicol (#91), trimethoxytoluene (#96) and 6-methoxycoumaran-7-ol-3-one (#100). These extra compounds may be present initially but undetectable in the non-catalytic BRH oil due to their minute concentrations, or are evidently chemical products formed from the catalytic reactions.

Table 7-6. Identified chemical compound in bio-oils from catalytic pyrolysis of Brunei rice husks

Peak	RT	Chemical Name	Chemical Formula	RMM	Chemical Group
1	6.103	2-methylfuran / Sylvan	C ₅ H ₆ O	82.10	Furans
2	6.735	Methyl acetate / Acetic acid, methyl ester	C ₃ H ₆ O ₂	74.08	Esters
3	7.023	Methyl propionate / Propanoic acid, methyl ester	C ₄ H ₈ O ₂	88.11	Esters
4	7.448	Benzene	C ₆ H ₆	78.11	Aromatic Hydrocarbon
5	7.933	3-methylbutanal	C ₅ H ₁₀ O	86.13	Aldehydes (CF)
6	8.414	2,5-Dimethylfuran	C ₆ H ₈ O	96.13	Furans
7	8.598	3-pentene-2-one, (E)-	C ₅ H ₈ O	84.12	Ketones
8	9.104	Acetic Acid	C ₂ H ₄ O ₂	60.05	Organic acids
9	9.621	3-pentanone, 2-methyl / Ethyl isopropyl ketone	C ₆ H ₁₂ O	100.12	Ketones (CF)
10	10.323	Methyl urea	C ₂ H ₆ N ₂ O	74.08	Nitrogen-containing compounds
11	10.426	2-methoxytetrahydrofuran	C ₅ H ₁₀ O ₂	102.13	Furans
12	10.875	Toluene	C ₇ H ₈	92.14	Aromatic Hydrocarbon
13	11.587	Pyridine	C ₅ H ₅ N	79.10	Nitrogen-containing compounds
14	11.886	3-penten-2-one / Methyl propenyl ketone	C ₅ H ₈ O	84.12	Ketones
15	13.462	Propanoic acid	C ₃ H ₆ O ₂	74.08	Organic acids
16	14.462	Cyclopentanone	C ₅ H ₈ O	84.12	Ketones
17	14.588	1-hydroxy-2-butanone	C ₄ H ₈ O ₂	88.11	Ketones
18	15.152	Ethylbenzene & p-xylene	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon
19	15.313	2,2-dimethyl-3-hexanol	C ₈ H ₁₈ O	130.23	Alcohols
20	15.543	m-Xylene	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon
21	16.202	3-furaldehyde / 3-furfural	C ₅ H ₄ O ₂	96.08	Furans
22	16.462	2-furanol, tetrahydro-2-methyl-	C ₅ H ₁₀ O ₂	102.13	Alcohols

23	16.635	3-propoxy-1-propene	C ₆ H ₁₂ O	100.16	Misc. Oxygenates
24	16.982	o-xylene	C ₈ H ₁₀	106.17	Aromatic Hydrocarbon (CF)
25	17.026	2,5-furandione / Maleic Anhydride	C ₄ H ₂ O ₃	98.06	Furans
26	17.350	Styrene	C ₈ H ₈	104.15	Aromatic Hydrocarbon (CF)
27	17.716	Furfural	C ₅ H ₄ O ₂	96.09	Furans
28	17.900	Tetrahydro-2,5-dimethoxyfuran	C ₆ H ₁₂ O ₃	132.16	Furans
29	19.774	Cyclohexanone	C ₆ H ₁₀ O	98.14	Ketones (CF)
30	20.027	2-furanmethanol	C ₅ H ₆ O ₂	98.10	Alcohols
31	20.360	1-(acetyloxy)-2-propanone / Acetol acetate	C ₅ H ₈ O ₃	116.12	Misc. Oxygenates
32	20.601	2-ethylhexanal	C ₈ H ₁₆ O	128.21	Aldehydes
33	20.774	2-Cyclopenten-1-one, 2-methyl-	C ₆ H ₈ O	96.13	Ketones
34	21.544	2-Furyl Methyl Ketone	C ₆ H ₆ O ₂	110.11	Ketones
35	22.259	1,2,3-Trimethylbenzene / Hemellitol OR 1,3,5-trimethylbenzene / Mesitylene	C ₉ H ₁₂	120.19	Aromatic Hydrocarbon (CF)
36	22.660	2-hexene-1-ol, acetate	C ₈ H ₁₄ O ₂	142.20	Misc. Oxygenates
37	23.614	1,2-cyclopentanedione	C ₅ H ₆ O ₂	98.10	Ketones
38	25.040	5-methyl-2-furancarboxaldehyde / 5-methylfurfural	C ₆ H ₆ O ₂	110.11	Furans
39	25.140	2,3-pentanedione / Acetyl propionyl	C ₅ H ₈ O ₂	100.12	Ketones
40	25.292	2-butanone, 1-(acetyloxy)-	C ₆ H ₁₀ O ₃	130.14	Misc. Oxygenates
41	25.660	2,3-dimethyl-2-cyclopenten-1-one	C ₇ H ₁₀ O	110.16	Ketones
42	25.833	3-Methyl-2-Cyclopentenone	C ₆ H ₈ O	96.13	Ketones
43	26.189	2(5H)-Furanone	C ₄ H ₄ O ₂	84.07	Furans
44	26.327	Tetrahydro-2-furanmethanol	C ₅ H ₁₀ O ₂	102.13	Alcohols
45	26.994	5-hexen-2-one	C ₆ H ₁₀ O	98.14	Ketones
46	27.626	2,2-diethyl-3-methyl-oxazolidine	C ₈ H ₁₇ NO	143.23	Nitrogen-containing compounds
47	28.353	2-hydroxybenzaldehyde	C ₇ H ₆ O ₂	122.12	Aldehydes (CF)
48	28.684	3-methyl-2(5H)-Furanone	C ₅ H ₆ O ₂	98.10	Furans
49	28.914	3-methyl-1,2-cyclopentanedione AND 2-cyclopenten-1-one, 2-hydroxy-3-methyl / Maple Lactone / Corylon / Cycloten	C ₆ H ₈ O ₂	112.13	Ketones
50	29.374	2,5-dihydro-3,5-dimethyl-2-furanone	C ₆ H ₈ O ₂	112.13	Furans
51	29.742	3,4-dimethyl-2-hydroxycyclopent-2-en-1-one	C ₇ H ₁₀ O ₂	126.15	Ketones
52	30.443	Phenol	C ₆ H ₆ O	94.11	Phenols
53	31.490	Guaiacol	C ₇ H ₈ O ₂	124.14	Guaiacols
54	31.881	3-ethyl-2-cyclopenten-1-one	-	-	Ketones

55	32.984	2-Methylphenol / o-cresol	C ₇ H ₈ O	108.14	Phenols
56	33.134	Formic acid,2-propenyl ester / Allyl formate	C ₄ H ₆ O ₂	86.09	Esters
57	33.490	3-ethyl-2-hydroxy-2-cyclopenten-1-one	C ₇ H ₁₀ O ₂	126.15	Ketones
58	33.674	Maltol / Larixic acid	C ₆ H ₆ O ₃	126.11	Organic acids
59	34.157	4-methyl-4-Hepten-3-one	C ₈ H ₁₄ O	126.20	Ketones
60	34.341	4-Methyl-5H-Furan-2-one	C ₅ H ₆ O ₂	98.10	Furans
61	34.720	p-cresol	C ₇ H ₈ O	108.14	Phenols
62	34.812	m-Cresol	C ₇ H ₈ O	108.14	Phenols
63	35.192	4-ethyl-1,3-benzenediol	C ₈ H ₁₀ O ₂	138.16	Phenols
64	35.629	3-methyl-4-hexen-2-one	C ₇ H ₁₂ O	112.17	Ketones
65	36.411	3-buten-2-ol	C ₄ H ₈ O	72.11	Alcohols
66	36.698	p-creosol / 2-methoxy-p-cresol	C ₈ H ₁₀ O ₂	138.17	Guaiacols
67	36.836	2-ethylphenol	C ₈ H ₁₀ O	122.16	Phenols
68	37.100	2,4-Dimethylphenol / 2,4-xlenol	C ₈ H ₁₀ O	122.16	Phenols
69	37.859	2-cyclopenten-1-one, 4-hydroxy-3-methyl-2-(2-propenyl)- / Allethrolone	C ₉ H ₁₂ O ₂	152.19	Misc. Oxygenates
70	38.125	2,4,6-trimethylphenol / Mesitol OR 3,4,5-trimethylphenol	C ₉ H ₁₂ O	136.19	Phenols (CF)
71	38.871	2,3 ; 2,4 ; 2,5-dimethylphenol / 2,3; 2,4; 2,5-xlenol	C ₈ H ₁₀ O	122.16	Phenols
72	39.020	4-Ethylphenol	C ₈ H ₁₀ O	122.16	Phenols
73	39.861	3,4; 2,6-dimethoxytoluene	C ₉ H ₈ O ₃	152.19	Misc. Oxygenates (CF)
74	40.251	3,4-dimethylphenol / 3,4-Xlenol	C ₈ H ₁₀ O	122.16	Phenols
75	40.412	2-nonene-1-ol	C ₉ H ₁₈ O	142.24	Alcohols
76	40.550	1-cyclohexyl-2-buten-1-ol (c,t)	C ₁₀ H ₁₈ O	154.25	Alcohols
77	40.780	4-Ethylguaiacol	C ₉ H ₁₂ O ₂	152.19	Guaiacols
78	41.182	4-ethyl-2-methyl-phenol	C ₉ H ₁₂ O	136.19	Phenols
79	41.331	3,4-anhydro-d-galactosan OR Anhydro-d-mannosan OR 2,3-anhydro-d-galactosan	C ₆ H ₈ O ₄	144.13	Anhydrosugars
80	41.952	1,4:3,6-dianhydro-α-d-glucopyranose	C ₆ H ₈ O ₄	144.13	Anhydrosugars
81	42.103	2,3-dihydro-1H-Inden-1-one / 1-Indanone	C ₉ H ₈ O	132.16	Ketones (CF)
82	42.805	3-ethyl-5-methylphenol	C ₉ H ₁₂ O	136.19	Phenols (CF)
83	43.056	2-Propenoic acid, 3-(2-hydroxyphenyl)-, (E)- / o-Coumaric acid	C ₉ H ₈ O	164.16	Organic acids
84	43.378	4-Ethenyl-2-methoxyphenol / p-Vinylguaiacol / 2-Methoxy-4-vinylphenol	C ₉ H ₁₀ O ₂	150.18	Guaiacols
85	44.551	4-allyl-2-methoxyphenol / Eugenol / Caryophillic acid	C ₁₀ H ₁₂ O ₂	164.20	Guaiacols
86	44.723	2-methoxy-4-propylphenol / Cerulignol	C ₁₀ H ₁₄ O ₂	166.22	Phenols

87	45.080	5-oxotetrahydrofuran-2-carboxylic acid, ethyl ester	C ₇ H ₁₀ O ₄	158.15	Misc. Oxygenates
88	45.689	2,6-Dimethoxyphenol / Syringol	C ₈ H ₁₀ O ₃	154.17	Syringols
89	47.001	Phenol, 2-methoxy-5-(1-propenyl)-, (E)- / Trans-m-Propenyl guaiacol	-	-	Guaiacols (CF)
90	47.461	2,6-dimethoxybenzaldehyde	C ₉ H ₁₀ O ₃	166.17	Misc. Oxygenates (CF)
91	48.082	4-(2-propenyl)-phenol OR Chavicol	C ₉ H ₁₀ O	134.18	Phenols (CF)
92	49.276	Isoeugenol	C ₁₀ H ₁₂ O ₂	164.20	Guaiacols
93	49.748	Hydroquinone / 1,4-benzenediol	C ₆ H ₆ O ₂	110.11	Phenols
94	50.035	Isovanillin	C ₈ H ₈ O ₃	152.15	Guaiacols
95	51.610	2-methyl-1,4-benzenediol / 2,5-toluenediol	C ₇ H ₈ O ₂	124.14	Phenols
96	52.819	1,2,3-trimethoxy-5-methylbenzene OR 3,4,5-trimethoxytoluene	-	182.22	Misc. Oxygenates (CF)
97	53.473	1-(4-hydroxy-3-methoxyphenyl)-ethanone / Acetovanillone	C ₉ H ₁₀ O ₃	166.17	Guaiacols
98	55.462	1-(4-hydroxy-3-methoxyphenyl)-2-propanone / Guaiacylacetone / Vanillyl methyl ketone	C ₁₀ H ₁₂ O ₃	180.20	Guaiacols
99	56.267	3,4-dihydrocoumarin-6-ol	-	-	Misc. Oxygenates
100	56.820	6-methoxycoumaran-7-ol-3-one	C ₉ H ₈ O ₄	180.16	Misc. Oxygenates (CF)
101	58.854	Levogluconan	C ₆ H ₁₀ O ₅	162.14	Anhydrosugars
102	60.268	4-Allyl-2,6-dimethoxyphenol OR Methoxyeugenol	C ₁₁ H ₁₄ O ₃	194.23	Syringols

The peak area percentages for the catalytic peaks can be seen in Table 7-7. The values stated are an average of two chromatograms obtained. The catalytically formed compounds were denoted with CF in parenthesis next to its chemical group.

Table 7-7. Peak area percentages of the various compounds detected from the catalytic pyrolysis of Brunei rice husks bio-oils

Peak #	No Cat	Binder	ZSM-5	Al-MCM-41	Al-MSU-F	BRHA	Regen ZSM-5	Regen Al-MCM-41	ZSM-5/ Al-MSU-F	ZSM-5/ Al-MCM-41	Al-MSU-F/ BRHA	Al-MCM-41/ Al-MSU-F	ZSM-5/ BRHA	Al-MCM-41/ BRHA
1	0.47	0.46	0.62	1.00	0.47	0.33	0.65	0.90	0.53	1.23	1.35	0.55	1.20	1.09
2	0.75	0.80	0.97	0.92	0.83	0.92	0.98	0.90	0.93	1.09	1.09	0.81	0.90	0.75
3	0.17	0.18	0.15	0.17	0.18	0.21	0.20	0.11	0.22	0.19	0.24	0.15	0.18	0.20
4	0.16	0.16	0.18	0.00	0.13	0.17	0.16	0.10	0.11	0.15	0.15	0.15	0.20	0.14
5	0.00	0.00	0.13	0.00	0.13	0.15	0.13	0.11	0.00	0.14	0.18	0.15	0.09	0.13
6	0.38	0.37	0.40	0.39	0.34	0.32	0.67	0.41	0.34	0.45	0.55	0.30	0.44	0.39
7	0.62	0.63	0.72	0.67	0.75	0.73	0.70	0.57	0.91	0.78	0.92	0.53	0.69	0.55
8	11.37	12.31	10.36	9.17	10.78	11.32	10.27	8.99	11.13	9.72	10.94	10.54	9.52	9.34
9	0.63	0.63	0.61	0.71	0.59	0.65	0.66	0.56	0.66	0.56	0.64	0.42	0.48	0.46
10	1.26	2.18	1.40	1.56	1.38	1.44	1.37	1.45	1.67	1.76	2.03	1.60	1.64	1.65
11	0.44	0.00	0.51	0.49	0.61	0.65	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
12	0.74	0.72	1.12	0.70	0.77	0.71	1.10	0.78	0.74	1.12	1.15	0.63	0.84	0.68
13	0.23	0.24	0.00	0.24	0.14	0.24	0.10	0.07	0.29	0.21	0.23	0.22	0.22	0.11
14	0.30	0.29	0.34	0.31	0.32	0.33	0.28	0.30	0.42	0.31	0.33	0.28	0.30	0.23
15	1.39	1.87	1.52	1.48	1.88	1.85	1.17	1.35	2.45	1.66	1.78	1.47	1.64	1.57
16	0.55	0.65	0.60	0.52	0.69	0.65	0.59	0.59	0.80	0.54	0.76	0.51	0.58	0.56
17	2.18	2.02	1.81	1.77	1.94	2.18	1.45	1.62	2.31	1.88	2.03	1.68	1.70	1.79
18	0.19	0.18	0.23	0.16	0.20	0.16	0.24	0.19	0.18	0.24	0.26	0.15	0.19	0.16
19	0.20	0.34	0.16	0.26	0.19	0.25	0.25	0.26	0.24	0.31	0.35	0.16	0.22	0.22
20	0.25	0.24	0.47	0.24	0.28	0.27	0.34	0.29	0.31	0.42	0.37	0.24	0.28	0.25
21	0.00	0.00	0.00	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.17	0.33	0.32	0.33
22	0.29	0.26	0.23	0.26	0.26	0.31	0.19	0.21	0.28	0.23	0.27	0.21	0.22	0.17
23	0.67	0.62	0.43	0.53	0.46	0.60	0.44	0.50	0.54	0.40	0.60	0.37	0.49	0.51
24	0.00	0.00	0.25	0.30	0.21	0.20	0.33	0.31	0.33	0.31	0.24	0.19	0.31	0.00
25	0.22	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.00	0.39	0.23	0.00	0.54
26	0.00	0.00	0.16	0.11	0.13	0.12	0.11	0.07	0.16	0.15	0.17	0.14	0.15	0.19

27	6.92	7.88	7.71	7.20	7.43	7.28	7.03	7.05	8.50	7.73	8.34	6.68	6.32	6.33
28	0.50	0.57	0.31	0.00	0.57	0.54	0.29	0.25	0.64	0.25	0.19	0.25	0.26	0.28
29	0.00	0.00	0.00	0.00	0.16	0.11	0.00	0.17	0.16	0.00	0.13	0.11	0.12	0.18
30	4.03	4.14	3.45	3.53	3.41	4.04	3.01	2.97	3.85	2.88	3.65	2.79	3.24	2.97
31	0.61	0.77	0.68	0.60	0.67	0.68	0.52	0.55	0.75	0.67	0.71	0.53	0.54	0.54
32	0.64	0.61	0.51	0.58	0.60	0.69	0.41	0.44	0.68	0.49	0.52	0.31	0.46	0.49
33	0.94	1.01	1.07	1.10	1.14	1.09	1.11	1.14	1.45	1.18	1.14	0.95	0.96	1.03
34	0.75	0.80	0.85	0.84	0.85	0.89	0.76	0.79	1.02	0.83	0.95	0.77	0.79	0.74
35	0.00	0.08	0.21	0.14	0.15	0.00	0.15	0.17	0.20	0.18	0.22	0.19	0.21	0.24
36	0.24	0.24	0.24	0.22	0.22	0.22	0.20	0.20	0.26	0.23	0.23	0.24	0.23	0.16
37	2.65	2.49	2.16	2.41	2.64	2.74	1.95	1.96	2.72	2.40	2.52	2.39	2.46	2.51
38	0.81	0.86	0.87	0.96	0.97	0.93	0.94	1.00	1.07	0.86	0.96	0.90	0.90	0.90
39	0.65	0.30	0.00	0.57	0.53	0.62	0.00	0.33	0.00	0.00	0.61	0.58	0.50	0.45
40	0.35	0.35	0.33	0.35	0.36	0.38	0.32	0.00	0.42	0.30	0.34	0.33	0.29	0.30
41	0.25	0.23	0.29	0.29	0.27	0.29	0.16	0.27	0.33	0.29	0.27	0.27	0.23	0.15
42	1.03	0.93	1.04	0.99	0.96	0.98	0.84	0.93	1.10	1.28	1.32	1.15	1.23	1.00
43	1.42	1.21	1.04	1.03	1.01	1.07	0.89	0.94	1.36	0.99	0.96	1.00	0.78	1.31
44	0.67	0.69	0.62	0.75	0.80	0.58	0.63	0.61	1.06	0.66	0.76	0.63	0.63	0.70
45	0.38	0.32	0.29	0.31	0.34	0.29	0.29	0.30	0.41	0.37	0.33	0.30	0.28	0.31
46	0.58	0.38	0.48	0.45	0.48	0.40	0.50	0.55	0.40	0.31	0.38	0.58	0.45	0.53
47	0.00	0.00	0.18	0.13	0.17	0.15	0.07	0.00	0.16	0.16	0.16	0.29	0.20	0.12
48	0.33	0.23	0.35	0.36	0.33	0.34	0.27	0.28	0.32	0.32	0.30	0.36	0.30	0.27
49	4.43	4.25	3.87	4.04	4.08	4.35	3.84	3.93	4.47	3.91	0.74	3.93	4.01	3.61
50	0.47	0.46	0.45	0.49	0.47	0.48	0.43	0.45	0.51	0.42	0.44	0.45	0.43	0.40
51	0.19	0.22	0.21	0.26	0.26	0.24	0.23	0.22	0.29	0.24	0.27	0.64	0.41	0.28
52	3.15	3.29	4.09	3.02	2.97	3.24	3.25	3.45	3.21	3.58	3.28	3.21	3.31	2.70
53	6.78	7.26	5.78	6.77	6.96	6.37	7.82	7.67	6.71	6.28	6.19	6.06	5.64	6.21
54	0.31	0.21	0.35	0.34	0.24	0.37	0.31	0.33	0.36	0.29	0.32	0.32	0.30	0.24
55	0.95	1.15	1.73	1.05	1.02	1.05	1.20	1.36	1.54	1.28	1.08	1.12	1.17	0.86

56	0.22	0.39	0.18	0.12	0.26	0.23	0.13	0.22	0.27	0.21	0.22	0.28	0.31	0.32
57	0.81	0.67	0.72	0.78	0.75	0.81	0.73	0.75	0.80	0.69	0.74	0.76	0.75	0.65
58	0.46	0.49	0.39	0.45	0.39	0.45	0.31	0.39	0.44	0.40	0.44	1.30	0.63	0.60
59	0.21	0.24	0.19	0.21	0.22	0.23	0.20	0.21	0.24	0.19	0.20	0.21	0.22	0.27
60	0.27	0.25	0.25	0.28	0.27	0.30	0.25	0.18	0.28	0.33	0.27	0.27	0.28	0.42
61	1.67	1.76	2.24	1.71	1.64	1.70	1.87	2.02	0.44	1.90	1.69	1.82	2.01	1.51
62	0.96	0.66	1.78	0.78	1.07	1.06	1.14	1.10	0.98	1.33	0.99	0.85	1.12	0.74
63	0.49	0.38	0.44	0.37	0.43	0.49	0.30	0.35	0.18	0.21	0.15	0.25	0.40	0.66
64	0.24	0.23	0.00	0.36	0.18	0.22	0.33	0.43	0.26	0.30	0.34	0.27	0.38	0.38
65	1.44	1.89	0.94	1.39	1.02	1.29	0.99	0.97	1.34	1.33	1.48	1.18	1.26	1.53
66	3.45	3.48	2.86	3.50	3.43	3.10	4.35	4.15	2.70	3.06	2.82	3.69	3.25	3.58
67	0.33	0.00	0.32	0.30	0.27	0.29	0.00	0.13	0.00	0.22	0.24	0.00	0.00	0.05
68	0.75	0.74	1.37	0.78	0.72	0.75	0.79	0.89	0.63	0.90	0.82	0.89	0.98	0.63
69	0.33	0.32	0.32	0.40	0.39	0.36	0.41	0.46	0.39	0.35	0.37	0.38	0.44	0.35
70	0.00	0.04	0.15	0.11	0.00	0.11	0.12	0.14	0.00	0.10	0.07	0.11	0.13	0.10
71	0.23	0.23	0.48	0.26	0.21	0.21	0.30	0.34	0.18	0.33	0.28	0.24	0.25	0.26
72	2.94	3.02	3.01	3.66	3.64	3.49	3.46	3.73	3.08	3.58	2.86	3.30	3.46	3.03
73	0.00	0.00	0.24	0.25	0.24	0.22	0.27	0.00	0.18	0.27	0.23	0.22	0.23	0.25
74	0.21	0.16	0.16	0.30	0.10	0.30	0.06	0.13	0.09	0.11	0.10	0.12	0.12	0.22
75	0.29	0.14	0.29	0.11	0.26	0.00	0.12	0.13	0.35	0.36	0.41	0.38	0.44	0.63
76	0.23	0.07	0.18	0.00	0.11	0.00	0.11	0.12	0.11	0.10	0.12	0.17	0.17	0.16
77	2.40	2.31	2.59	2.79	2.70	2.29	3.56	3.46	1.98	2.44	2.13	2.63	2.42	2.83
78	0.26	0.24	0.51	0.41	0.33	0.31	0.28	0.34	0.31	0.34	0.35	0.49	0.51	0.36
79	0.47	0.51	0.52	0.52	0.45	0.56	0.41	0.46	0.42	0.53	0.48	0.50	0.53	0.49
80	0.90	0.86	0.62	0.75	0.64	0.82	0.49	0.60	0.64	0.76	0.76	0.67	0.78	0.90
81	0.00	0.21	0.26	0.24	0.25	0.26	0.22	0.23	0.24	0.25	0.23	0.34	0.30	0.69
82	0.00	0.10	0.14	0.00	0.00	0.00	0.08	0.10	0.00	0.10	0.13	0.11	0.09	0.08
83	3.79	3.65	4.50	3.90	3.81	3.51	4.58	4.41	3.20	3.35	3.65	4.29	4.21	3.74
84	2.69	2.51	2.73	2.94	2.88	2.23	3.75	3.72	2.14	2.56	2.54	3.08	2.75	2.84

85	0.37	0.36	0.32	0.40	0.38	0.34	0.45	0.39	0.32	0.37	0.31	0.45	0.37	0.40
86	0.47	0.36	0.41	0.51	0.46	0.37	0.60	0.55	0.33	0.46	0.41	0.51	0.49	0.59
87	0.46	0.73	0.40	0.47	0.40	0.54	0.25	0.31	0.35	0.51	0.58	0.65	0.47	0.56
88	1.24	0.93	0.92	1.17	1.00	1.06	1.11	1.09	0.85	1.07	0.95	1.05	0.99	1.04
89	0.00	0.15	0.32	0.33	0.36	0.28	0.54	0.57	0.23	0.33	0.24	0.32	0.29	0.95
90	0.00	0.08	0.15	0.12	0.00	0.12	0.14	0.20	0.00	0.13	0.11	0.14	0.18	0.16
91	0.00	0.10	0.14	0.15	0.00	0.15	0.11	0.10	0.00	0.07	0.09	0.12	0.15	0.44
92	1.62	1.28	1.62	1.75	1.66	1.33	2.40	2.10	1.12	1.49	1.32	1.59	1.49	1.82
93	1.18	1.02	0.91	1.00	0.85	0.96	0.92	1.02	0.81	1.22	1.07	1.10	1.21	1.19
94	0.52	0.42	0.41	0.47	0.45	0.42	0.45	0.48	0.39	0.46	0.42	0.47	0.51	0.52
95	0.30	0.22	0.32	0.28	0.24	0.25	0.21	0.26	0.23	0.40	0.35	0.41	0.41	0.44
96	0.00	0.00	0.25	0.34	0.30	0.28	0.31	0.30	0.23	0.35	0.31	0.42	0.39	0.49
97	0.43	0.40	0.31	0.51	0.38	0.25	0.38	0.39	0.39	0.42	0.53	0.49	0.51	0.68
98	0.80	0.56	0.60	0.86	0.77	0.75	0.70	0.77	0.70	0.86	0.79	0.82	0.84	1.00
99	0.35	0.27	0.44	0.56	0.43	0.41	0.39	0.35	0.41	0.58	0.49	0.31	0.49	0.51
100	0.00	0.05	0.24	0.29	0.22	0.00	0.30	0.36	0.41	0.31	0.31	0.33	0.33	0.36
101	2.49	1.30	1.06	1.78	1.46	1.54	0.91	1.28	1.44	1.86	1.86	2.36	2.65	2.32
102	0.25	0.15	0.24	0.31	0.25	0.23	0.39	0.37	0.21	0.31	0.26	0.37	0.37	0.42
	100.01	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00

7.4.2.5.1 Effects of catalysts on selected chemicals

The effects of catalysts on selected chemicals were analysed. As there are more than 100 peaks detected from GC-MS, it would be tedious to analyse each peaks individually. Chemicals such as toluene (#12), acetic acid (#8), furfural (#27), phenol (#52), o-, p- and m-cresols (#55, #61 and #62), 4-ethylphenol (#72), guaiacol (#53), levoglucosan (#101), syringol (#88) are analysed individually.

Levoglucosan (#101) is one of the major products from the degradation of cellulose, besides water, char, CO and CO₂. All of the catalysts with the exception of ZSM-5/BRHA, reduce the amount of levoglucosan present, but ZSM-5 and its regenerated form shows the most reduction overall. This work confirms previous studies that showed levoglucosan is decreased or eliminated when subjected to catalytic cracking [73, 90].

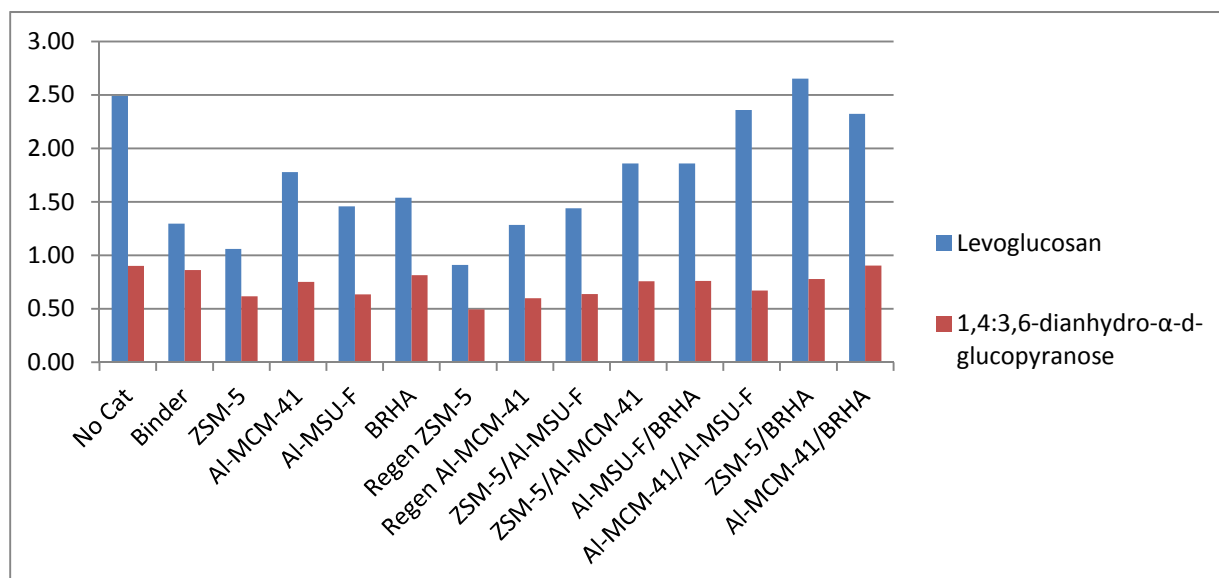


Figure 7-4. Effect of catalysts on selected anhydrosugars

Secondary degradation reactions by the catalysts help in the formation of other anhydrosugars and furans, such as furfural [169]. Furfural (#27) is produced from the pyrolysis of cellulose and hemicellulose [170]. The production of furfural is increased for most of the catalyst compared to the non-catalytic run, except for Al-MCM-41/Al-MSU-F, ZSM-5/BRHA and Al-MCM-41/BRHA. The highest increase for furfural was from ZSM-5/Al-MSU-F with 8.50 % peak area.

A study conducted by Adam et al. shows that Al-MCM-41 catalysts promote the furfural and furan production from pyrolysis of biomass [90]. The peak area for 2-methylfuran (#1)

increases two-fold for Al-MCM-41 and only reduced slightly for the regenerated form, but is still higher than the other single catalysts. As for the multiple catalyst, the combination of Al-MCM-41/Al-MSU-F halved the production of 2-methylfuran compared to Al-MCM-41 alone. But the combination of Al-MSU-F/BRHA showed the highest peak area and positive synergy as compared to their individual run independently, followed by the combination of ZSM-5/Al-MCM-41, ZSM-5/BRHA and Al-MCM-41/BRHA.

Acetic acid (#8) has the highest peak area amongst the other chemical compound identified in the bio-oil. Acetic acid is mainly generated from the degradation of hemicellulose and partly from lignin. The peak area of acetic acid is mostly reduced with Al-MCM-41 catalyst, and BRHA catalyst having almost no effect on the reduction of acetic acid when compared to the non-catalytic run. This agrees with the study from Samolada et al., who reported a reduction in acetic acid content in bio-oil on using fresh Al-MCM-41 catalyst in a fixed bed reactor [132]. Adam et al. also reported that Al-MCM-41 increased the acetic acid production for fast pyrolysis, but observed a decreased for catalytic pyrolysis with a lower heating rate [90]. This result is in agreement with this study, as the heating rate in this work is moderate.

The main chemical reaction in the transformation of biomass to phenols starts with the dehydration of –OH groups in the alkyl chain of the lignin phenylpropane basic unit followed by the cleavage of the inter-aromatic bonds, of which the β -O-4 aryl ether bond is the most frequent linkage [171]. Liu et. al mentioned that the β -O-4 linkage is the most important and most abundant substructure in lignin, probably accounting for 50% of the linkages [25].

A study conducted by Liu et al. found that phenol is mainly produced from the pyrolysis of the H-type lignin, besides cresols and 4-ethylphenol [25]. In this study, the highest peak area for phenol (#52) was obtained for ZSM-5 with 4.09%, followed by ZSM-5/Al-MCM-41 with 3.58%. The regenerated ZSM-5 showed a significant reduction to 3.25%. As for regenerated Al-MCM-41, the peak appears to increase compared to the fresh one, from 3.02 to 3.45%. The significant reduction was obtained for Al-MCM-41/BRHA, which decreased the phenol production to 2.70%.

Cresols in Figure 7-5 include o-, p- and m-cresols (#55, #61 and #62). ZSM-5 appears to increase the production of cresols significantly compared to the rest of the other catalysts. The regenerated form of ZSM-5 however does not generate much cresols with a peak area of 4.21%, as compared with the fresh one with 5.75%. The opposite is true for Al-MCM-41, by which the regenerated form increases more cresols than the fresh one. For 4-ethylphenol

(#72), Al-MCM-41 and its regenerated form increases the most with 3.66% and 3.73% peak area.

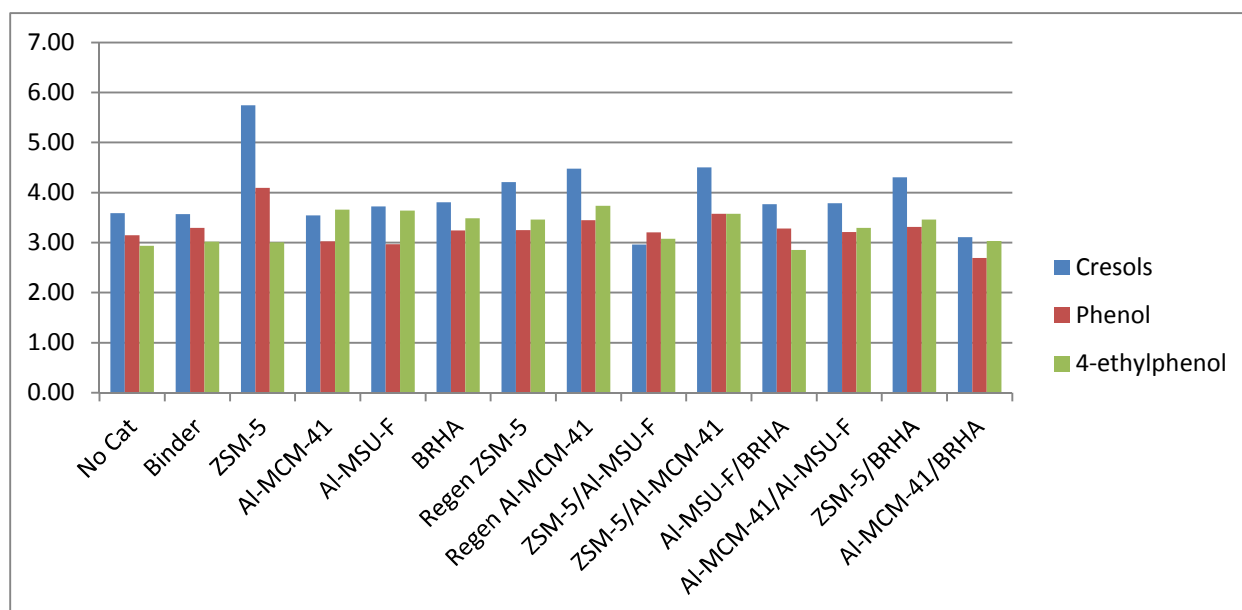


Figure 7-5. Effect of catalysts on selected phenols

Liu et. al conducted a study on the pyrolysis of the G-type lignin models which produce guaiacol and p-vinylguaiacol as the main products [25]. The chemicals were also detected for BRH pyrolysis oil. Aside from that, p-cresol was also a significant chemical detected. Guaiacol (#53) is decreased by ZSM-5 and BRHA, and the combination of both catalysts. As for p-cresol (#66), the peak area was also decreased by ZSM-5 and BRHA, and for combined catalyst ZSM-5/Al-MSU-F and Al-MSU-F/BRHA. But for both chemicals, an increase in peak area for both the regenerated catalyst ZSM-5 and Al-MCM-41 was significant.

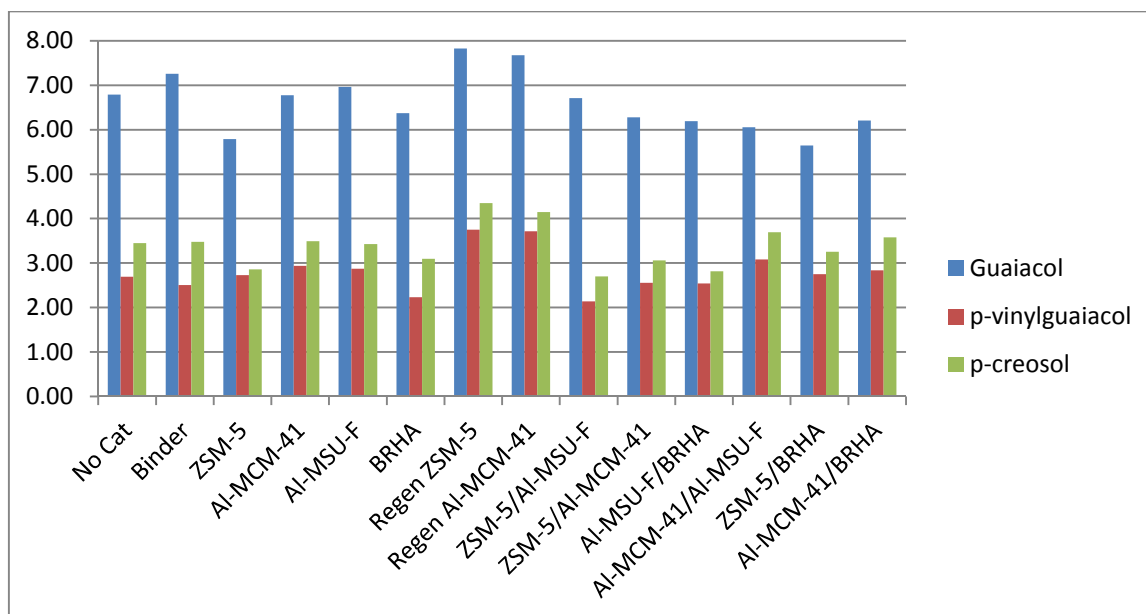


Figure 7-6. Effect of catalysts on selected guaiacols

2,6-dimethoxyphenol (#88) and methoxyeugenol (#102) are the only compounds detected from the S-type lignin. For 2,6-dimethoxyphenol, all the catalysts show a reduction in the peak area.

Aromatic hydrocarbons are formed from a series of dehydration, decarbonylation, decarboxylation, isomerisation, oligomerisation and dehydrogenation in the zeolite catalysts [118]. The effect of catalysts on aromatic hydrocarbons is shown in Figure 7-7. Toluene (#12) and xylenes – which is comprised of p-xylene or ethylbenzene (#18), m-xylene (#20) and o-xylene (#24) was seen to be the most affected by ZSM-5, regenerated ZSM-5, ZSM-5/Al-MCM-41 and Al-MSU-F/BRHA with an increase in the peak areas compared to other catalysts.

Other aromatic hydrocarbon compound such as benzene (#4) was not detected in the non-catalytic bio-oil, but is present in all the catalytic runs except for Al-MCM-41. Catalytically formed aromatic hydrocarbons can be seen, with the formation of styrene (#26) and trimethylbenzene (#35). Styrene production was apparent in all the catalytic runs except for the binder and the non-catalytic run. Apart from the non-catalytic run, trimethylbenzene was present for all the catalytic run except for BRHA. Polyaromatic hydrocarbon compounds were not detected in the rice husk bio-oil.

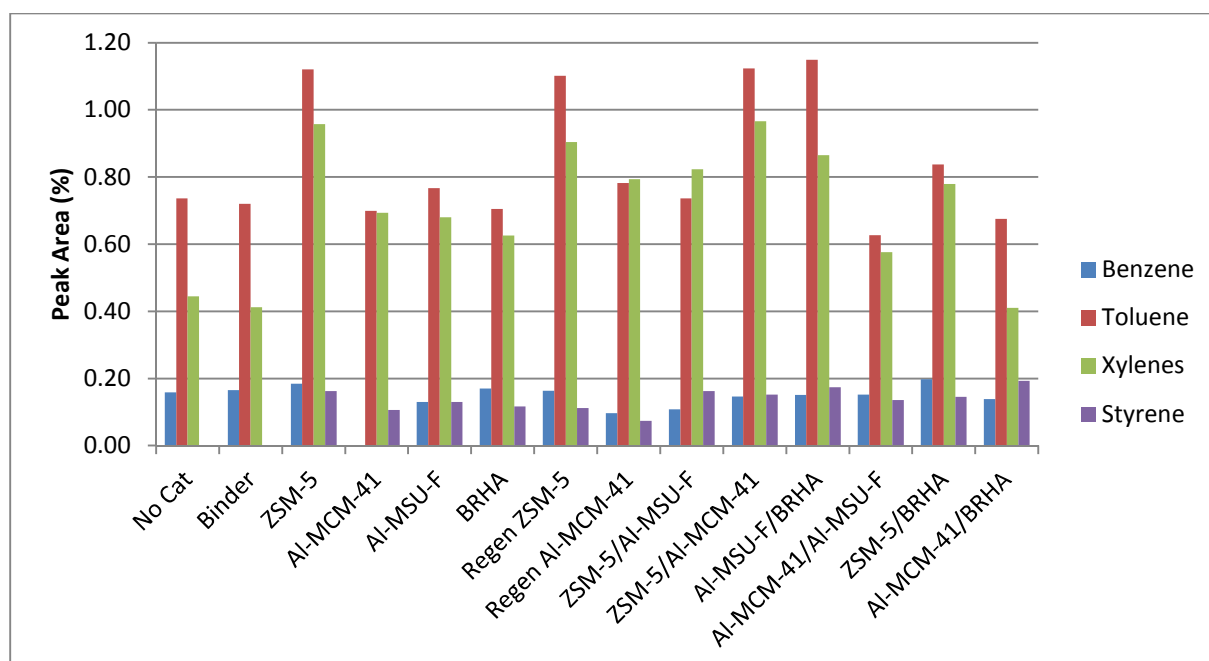


Figure 7-7. Effect of catalysts on aromatic hydrocarbons

7.4.2.5.2 Effect of catalysts on the chemical groups

An overall sense on the effect of catalysts on BRH bio-oils may be analysed clearly based on the chemical groups. The individual chemicals peak area were categorised in their respective chemical groups, namely aromatic hydrocarbons (ARH), organic acids (OA), esters (EST), furans (FUR), aldehydes (ALD), ketones (KET), alcohols (ALC), phenols (PHE), guaiacols (GU), syringols (SYR), anhydrosugars (ANH), miscellaneous oxygenated compounds (MISC) and nitrogen-containing compounds (NCC). The total peak areas of the chemical groups for the non-catalytic and catalytic pyrolysis of Brunei rice husk bio-oil may be found in Table 7-8.

Table 7-8. Total peak areas of the chemical groups for the non-catalytic and catalytic pyrolysis of Brunei rice husk bio-oil

Peak Areas (%)	CHEMICAL GROUPS												
	ARH	OA	EST	FUR	ALD	KET	ALC	PHE	GU	SYR	ANH	MISC	NCC
No catalyst	1.34	17.01	1.14	12.23	0.64	17.10	7.14	13.89	19.07	1.49	3.86	3.02	2.07
Binder	1.37	18.32	1.36	12.33	0.61	16.32	7.51	13.48	18.73	1.09	2.67	3.44	2.79
ZSM-5	2.63	16.76	1.30	12.51	0.82	15.39	5.88	18.19	17.55	1.16	2.20	3.72	1.88
Al-MCM-41	1.64	15.00	1.22	12.48	0.71	16.72	6.31	14.69	20.32	1.47	3.05	4.12	2.26
Al-MSU-F	1.86	16.86	1.27	12.47	0.90	17.17	6.06	13.95	19.97	1.25	2.54	3.70	2.00
BRHA	1.62	17.13	1.36	12.25	0.99	18.01	6.48	14.72	17.37	1.29	2.92	3.80	2.08

Regen ZSM-5	2.43	16.34	1.31	11.42	0.61	14.67	5.30	14.68	24.41	1.49	1.81	3.54	1.97
Regen Al-MCM-41	1.92	15.14	1.23	11.45	0.55	15.62	5.27	16.02	23.69	1.46	2.35	3.23	2.07
ZSM-5/ Al-MSU-F	2.03	17.22	1.42	13.78	0.83	18.94	7.23	12.00	16.69	1.06	2.50	3.94	2.36
ZSM-5/ Al-MCM-41	2.57	15.13	1.48	12.59	0.79	16.28	5.87	16.12	18.26	1.38	3.15	4.11	2.28
Al-MSU-F/ BRHA	2.56	16.80	1.55	13.91	0.86	14.78	7.03	13.97	17.30	1.21	3.09	4.30	2.64
Al-MCM-41/ Al-MSU-F	1.68	17.60	1.23	11.32	0.75	16.39	5.53	14.64	19.60	1.42	3.53	3.91	2.40
ZSM-5/ BRHA	2.17	16.01	1.39	11.23	0.75	16.67	6.18	15.82	18.06	1.37	3.96	4.08	2.31
Al-MCM-41/ BRHA	1.65	15.25	1.27	12.27	0.74	16.09	6.39	13.86	20.81	1.45	3.72	4.20	2.30

From Table 7-8, we can analyse that the dominating chemical groups in the BRH bio-oil are organic acids, furans, ketones, phenols and guaiacols. This was expected, as majority of the BRH contains cellulose and lignin. Numerous model pathways were proposed for cellulose pyrolysis from literature, and one of them is the Broido-Shafizadeh model (Figure 7-9) which shows the formation of ketones, organic acids and furans from the secondary reactions of levoglucosan (anhydrosugars).



Figure 7-8. The global modified Broido-Shafizadeh model (adapted from [63])

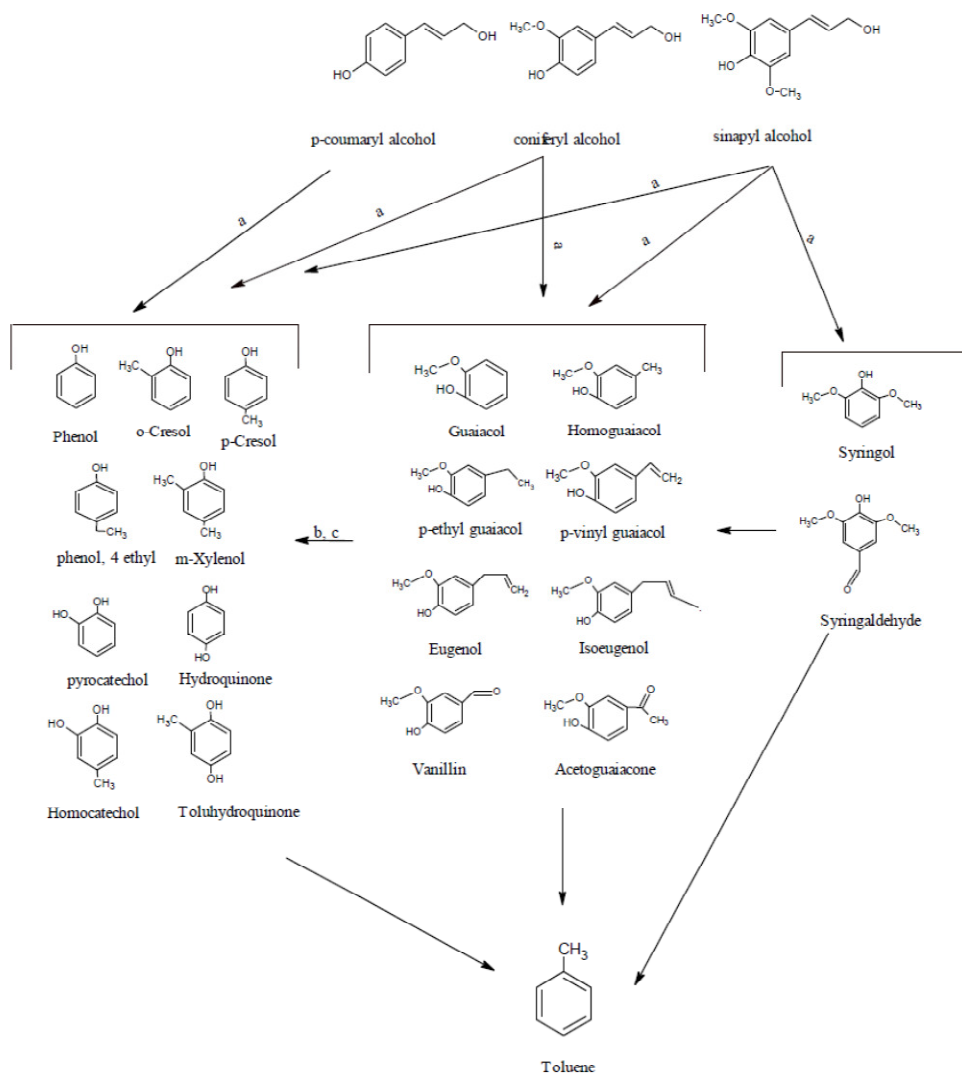


Figure 7-9. Existence of quantified compounds from the pyrolysis of lignin monomers from literature adapted from [172]. Reactions (a)[173] ,(b)[174] and (c) [175].

Since the lignin content of the biomass was reasonably high, the pyrolysis products are expected to contain high phenols and guaiacols content. Lignin is known to have three basic types of structural units, which we can associate the products with the chemical groups. The pyrolysis of p-coumaryl alcohol monomer (H-type) produces mainly phenols, coniferyl alcohol monomer (G-type) produces guaiacols and phenols, and sinapyl alcohol (S-type) produces syringols, guaiacols and phenols. The pyrolysis of BRH lignin components mainly produces phenols and guaiacols. The further degradation of the lignin pyrolysis products suggests the production of toluene, which may explain the highest peak area for aromatic hydrocarbon is toluene.

A closer inspection of the effect of catalysts in comparison to the non-catalytic run on the chemical group may be found in Table 7-9. The change in the peak areas is obtained by subtracting the peak areas from the catalytic runs with the non-catalytic runs. From this table we can evaluate the changes in the catalytic runs with respect to their chemical groups as compared to the non-catalytic run.

Table 7-9. The effect of the catalyst on the chemical groups in comparison to the non-catalytic Brunei rice husk bio-oil

Peak areas (%)	Chemical Groups												
	ARH	OA	EST	FUR	ALD	KET	ALC	PHE	GU	SYR	ANH	MISC	NCC
No catalyst	0	0	0	0	0	0	0	0	0	0	0	0	0
Binder	0.03	1.31	0.22	0.10	-0.03	-0.78	0.37	-0.42	-0.34	-0.41	-1.19	0.42	0.72
ZSM-5	1.29	-0.25	0.17	0.28	0.18	-1.71	-1.26	4.30	-1.51	-0.34	-1.66	0.70	-0.19
Al-MCM-41	0.30	-2.01	0.08	0.25	0.07	-0.38	-0.83	0.80	1.25	-0.02	-0.81	1.10	0.19
Al-MSU-F	0.52	-0.15	0.13	0.24	0.26	0.07	-1.08	0.06	0.90	-0.24	-1.32	0.68	-0.08
BRHA	0.28	0.12	0.22	0.02	0.35	0.91	-0.66	0.82	-1.70	-0.20	-0.95	0.78	0.01
Regen ZSM-5	1.09	-0.67	0.17	-0.81	-0.03	-2.42	-1.84	0.79	5.35	0.00	-2.05	0.53	-0.10
Regen Al-MCM-41	0.58	-1.88	0.09	-0.78	-0.09	-1.47	-1.87	2.12	4.62	-0.03	-1.51	0.21	0.00
ZSM-5/ Al-MSU-F	0.69	0.20	0.28	1.55	0.19	1.84	0.09	-1.89	-2.38	-0.43	-1.36	0.92	0.29
ZSM-5/ Al-MCM-41	1.23	-1.88	0.34	0.36	0.15	-0.82	-1.27	2.23	-0.81	-0.11	-0.72	1.09	0.21
Al-MSU-F/ BRHA	1.22	-0.21	0.41	1.68	0.22	-2.31	-0.11	0.08	-1.77	-0.28	-0.77	1.28	0.56
Al-MCM-41/ Al-MSU-F	0.34	0.59	0.09	-0.91	0.10	-0.71	-1.61	0.74	0.53	-0.07	-0.33	0.89	0.33
ZSM-5/ BRHA	0.83	-1.01	0.26	-1.00	0.11	-0.43	-0.96	1.93	-1.00	-0.13	0.10	1.06	0.24
Al-MCM-41/ BRHA	0.31	-1.76	0.13	0.04	0.09	-1.01	-0.75	-0.03	1.74	-0.04	-0.15	1.18	0.23

The catalyst with most activity can be seen for ZSM-5, due to the changes in the peak areas for the various chemical groups. ZSM-5 is effective for the production of aromatic hydrocarbon and phenols, and the reduction in the peak areas for ketones, alcohols and anhydrosugars.

The binder shows the least deviation compared to the rest of the catalytic runs, which showed that the binder did not take much part on the upgrading of the pyrolysis vapours. Although that said, the run with binder generates more organic acids mainly acetic acid, making the bio-oil more acidic.

The formation of aromatic hydrocarbons is mainly from the degradation of lignin compounds. The production of aromatic hydrocarbons was slightly higher for Al-MSU-F (1.86%) than Al-

MCM-41 (1.64%), which was attributed to the absence of benzene from the peak chromatograph for Al-MCM-41. This was proven from a previous study by Pattiya et al. using cassava rhizome as the pyrolysis feedstock which showed an increase in the aromatic hydrocarbon production particularly benzene and xylenes for Al-MSU-F than Al-MCM-41 [176].

7.4.3 Regenerated catalysts studies

This section discusses the effects of the regenerated catalysts on the chemical group. ZSM-5 regenerated catalysts can be seen to produce more guaiacol compounds with 24.41% as compared to the fresh ZSM-5 with 17.55%. The production of phenolics was compromised with a significant decrease from 18.19% to 14.68%. Since guaiacols and phenolics were formed from the pyrolysis of lignin, we can infer that based on the schematic diagram proposed from Figure 7-9, reactions (a) proceeds as normal and the selectivity towards guaiacol compounds were more, and that reactions (b) and (c) were restricted towards the formation of phenol. However, the ability for the production of aromatic hydrocarbons is retained, although slightly lower than the fresh ZSM-5.

As for the regenerated Al-MCM-41 catalysts, the reduction in the organic acid compounds is still retained, although slightly lower than the fresh one. A further decrease of ketones, alcohols and anhydrosugars, and an increase of phenolics and guaiacols chemical group can be seen. This was similar the ZSM-5 regenerated catalysts, although more phenolics was formed, but the increase in aromatic hydrocarbons was not as significant.

7.4.4 General remarks

The multiple stacked catalysts showed a very interesting synergistic effect for some, when compared with the individual catalytic traits. Some catalysts such as Al-MSU-F/BRHA exhibit a positive amplified effect when combined, compared to their individual respective ability. It is interesting to note that the interaction between Al-MSU-F/BRHA does produce a high amount of aromatics with a peak area of 2.56%, as compared to the peak areas for their individual runs (1.86% and 1.62% respectively). The increase in the hydrocarbon content was attributed to the increase in toluene and xylenes, almost similar to the peak areas obtained from ZSM-5 alone. The combination of both also generated furans, and showed a significant reduction in ketones and guaiacols. This synergy effect is not studied further in this research.

The synergy between ZSM-5/Al-MSU-F showed a significant increase in the ketone chemical group. ZSM-5 alone reduces the ketones, and Al-MSU-F increases the ketone formation slightly. Most of the catalyst show a reduction in the alcohol chemical group in the bio-oil except for the binder alone and ZSM-5/Al-MSU-F. The highest reduction for the single catalysts was for ZSM-5 and both the regenerated ZSM-5 and Al-MCM-41 catalysts.

The interesting feature of the ZSM-5/Al-MCM-41 catalyst is that it adopts the desired properties from its individual single runs, i.e. increase in aromatics and phenols, and the decrease in the organic acids. The commercial catalysts showed a significant reduction of ketones, with ZSM-5 having the most reduction. BRHA on the other hand shows no variation in the amount of ketones.

7.5 Evaluation procedures for the 'best' catalyst

Various different criteria were proposed for the favourable quality of the bio-oil. The top three catalytic runs, aside from the non-catalytic run were chosen from each criterion. The chosen catalyst receiving the most tallies from the criteria will be selected for the optimisation experiments. The first three criteria were obtained from the GC-MS peak areas. The increase in the aromatic hydrocarbon peak and phenols peak areas would mean the production of high-value chemicals. The reduction in organic acids and the increase in pH favour the usage of bio-oils, making them less corrosive. The increase in the heating value and a reduction in the water content of the bio-oil are useful for energy purposes. A lower viscosity bio-oil indicates the ability of the catalysts to crack the heavy molecules from the pyrolysis vapours.

1. Increase in aromatic hydrocarbon
2. Reduction in the organic acid
3. Increase in phenols
4. Increase in pH (lower acidity)
5. Increase in the HHV
6. Lower water content
7. Lower viscosity
8. Lower density
9. High HC molar ratio
10. Low OC molar ratio

Table 7-10. Evaluation of the 'best' catalyst from the various criterions

Catalytic runs	Criterions									
	1	2	3	4	5	6	7	8	9	10
Binder						X				
ZSM-5	X		X						X	
Al-MCM-41		X		X					X	
Al-MSU-F							X			
BRHA					X					X
Regen ZSM-5								X		
Regen Al-MCM-41		X	X	X		X		X		
ZSM-5/Al-MSU-F										
ZSM-5/Al-MCM-41	X	X	X	X			X		X	
Al-MSU-F/BRHA	X			X			X	X		
Al-MCM-41/Al-MSU-F										
ZSM-5/BRHA				X	X					X
Al-MCM-41/BRHA					X	X				X

The combination of ZSM-5 and Al-MCM-41 shows that they are superior as compared to the other catalysts on certain aspects. Individually, ZSM-5 is as expected to be a very active catalyst. Al-MCM-41 is merited being the only catalyst by itself showing a strong reduction in the organic acids in the liquid bio-oil, including in its regenerated form. The arrangement of both the catalysts show a reduction in the acidity of the bio-oil, which can be reflected from both criteria 2 and 4. Due to similar values obtained for criteria 4 (increase in pH), five of the catalytic runs were selected.

ZSM-5/Al-MCM-41 however lacks the ability to lower the water content, increase the HHV and lowering the OC molar ratio. Due to their active catalytic nature, they contain the highest the water content value. This has an effect on the wet-HHV of the bio-oil, as it was the lowest for all the catalytic runs. The OC molar ratio was also high, owing to the fact that more wt. % oxygen was determined for the bio-oils, possibly from the cracking and depolymerisation mechanism.

Regen Al-MCM-41 surprisingly exhibits a better catalyst as compared to the fresh one. Some catalytic runs showed an exceptional behaviour, such as Al-MSU-F/BRHA for increasing the aromatics production, when neither possesses the quality when each acting independently. BRHA, ZSM-5/BRHA and Al-MCM-41/BRHA also can be merited for increasing the heating values. Although the synergies between both various catalysts were interesting, the other favoured qualities were however lacking.

7.6 Summary

The catalytic pyrolysis experiments shows that the catalysts employed in these experiments were able to upgrade the bio-oil to some extent. Although the ratio of catalyst to biomass was low, changes were seen in the bio-oil especially towards the peak areas from GC-MS. ZSM-5, Al-MCM-41, Al-MSU-F and BRHA, collectively with their combinations show various changes towards the bio-oil characterisation results. The regenerated catalysts lost some of the initial catalytic properties, but still maintain its ability to reduce the higher molecular compounds. ZSM-5/Al-MCM-41 catalysts were shown to meet most of the criteria from the evaluation procedures. The combinations of both the catalysts lead to a synergy in which the functions of both of the individual catalysts are adopted and intact, unlike some of the combined catalysts. ZSM-5/Al-MCM-41 catalytic run was evaluated the favoured catalysts and is selected for the next phase of optimisation experiments.

8 CATALYTIC OPTIMISATION EXPERIMENTS

8.1 Introduction

The combination of the two catalysts in series for ZSM-5 and Al-MCM-41 was favoured from Chapter 7 and selected for the optimisation experiments. The optimisation experiments essentially involve altering the ratio of the catalysts into steps of 25%, 50% and 75% and substituting the remaining percentages with the secondary catalyst totalling up to 100%. A run involving the physical mixing of both catalysts for 50% ratio was also included. Catalyst preparation is similar to the procedures from Chapter 7, but the catalyst ratio was adjusted according to the weight of the catalyst and keeping the binder ratio constant. Characterisation of the bio-oils was carried out, and the investigation of both ZSM-5 and Al-MCM-41 as a primary catalyst was analysed and evaluated. Criteria for the selection of favourable bio-oil qualities were adapted from Chapter 7 and evaluated to determine the most suitable optimisation run. Ultimately, the selected optimisation run would conclude the best ratio for the combination of ZSM-5 and Al-MCM-41.

8.2 Catalytic optimisation experiments

The catalytic optimisation experiments involving pyrolysis of BRH using both ZSM-5 and Al-MCM-41 catalysts stacked in series, with different catalyst ratio between them. In this experiment also, the catalyst arrangement or positioning, i.e. ZSM-5 then Al-MCM-41 and Al-MCM-41 then ZSM-5 is investigated. The effect of physically mixing ZSM-5 and Al-MCM-41 was also examined for the 50% ratio. The ratio involves altering the amount of catalysts in the monolith. The concept of a guard catalyst bed which was mentioned by Sutton et al. [121] and Pattiya et al. [24] is applicable in this sense that the primary catalyst protects the secondary catalyst from deactivation.

Catalyst preparation was similar to Chapter 7, although the coating of catalyst was reduced on the monolith for the catalyst with a lower percentage ratio. The catalyst preparation for the physically mixed catalyst was done by mixing a 1.5: 1.5: 1 ratio of ZSM-5, Al-MCM-41 and montmorillonite binder respectively. A total of 7 experiments were recorded with the inclusion of the ZSM-5/Al-MCM-41 results from chapter 7 and stated as ZSM 50%: MCM 50%. The catalyst combination that is mentioned first would be the primary catalyst and followed by the second, as the secondary catalyst. For result comparison purposes where ZSM-5 is mentioned, it is stated as ZSM 100% and Al-MCM-41 stated MCM 100%.

8.2.1 Mass balance summary

The mass balance for the catalytic pyrolysis optimisation experiments can be seen in Table 8-1. The run name, average catalyst bed temperature, product yields (wt. %) and gases composition were noted. The average catalytic bed temperature was measured at a range of 500 to 540 °C for the various catalytic optimisation runs.

Table 8-1. Mass balance for catalytic optimisation experiments

Run Name	Average catalytic bed temperature (°C)	Product yield (wt. %)			Gases composition (wt. %)		
		Liquid	Char	Gases ^a	CH ₄	CO	CO ₂
ZSM 75%: MCM 25%	529	40.07	42.26	17.66	4.01	18.39	65.00
ZSM 50%: MCM 50%	518	39.28	42.81	17.91	0.23	1.82	85.50
ZSM 25%: MCM 75%	538	40.88	43.06	16.06	3.77	17.39	65.48
Mixtures	521	40.03	42.78	17.19	5.43	26.06	55.91
MCM 75%: ZSM 25%	513	39.48	42.06	18.45	2.73	17.76	66.29
MCM 50%: ZSM 50%	525	40.14	41.90	17.96	4.03	26.26	57.51
MCM 25%: ZSM 75%	518	40.40	42.47	17.14	2.15	12.87	72.04

^a by difference

The char yield is deemed consistent due to the invariable pyrolysis conditions in the fixed-bed reactor. The liquid yield was almost analogous throughout, and the lowest was obtained for ZSM 50%: MCM 50% with 39.28 wt. %.

The yield for gases was obtained by difference. For ZSM-5 as a primary catalyst, the yield of gases have a tendency to decrease for runs with the introduction of Al-MCM-41 due to the lower gas yield obtained from the Al-MCM-41 100% run (16.87 wt. %). This trend was the opposite for Al-MCM-41 as a primary catalyst, as ZSM 100% run (19.44 wt. %) increases the gases yield.

The CO₂ yield was the highest for ZSM 50%: MCM 50% with 85.50 wt. %, and the lowest was obtained for the physically mixed catalyst with 55.91 wt. %. A lower generation of CO₂ may indicate a less activity as compared to the other runs. However, for Al-MCM-41 as a primary catalyst, it was expected that the value of CO was higher due to the decarbonylation effect.

8.2.2 Bio-oil characterisation results

Bio-oil characterisation results for water content, viscosity, density, elemental analysis, heating values (HHV), acidity (pH) and the chemical composition using GC-MS were analysed and discussed.

8.2.2.1 Water content

Table 8-2 shows the water contents from the optimisation experiments. The water content ranges from 51.60% (ZSM 25%: MCM 75%) to 57.44% (ZSM 50%: MCM 50%).

Table 8-2. Water content for the optimisation experiments

Catalyst runs	Water content (%)
ZSM 75%: MCM 25%	52.20 ± 0.09
ZSM 50%: MCM 50%	57.44 ± 0.21
ZSM 25%: MCM 75%	51.60 ± 0.02
Mixtures	52.79 ± 0.42
MCM 75%: ZSM 25%	52.07 ± 0.33
MCM 50%: ZSM 50%	54.80 ± 0.27
MCM 25%: ZSM 75%	54.65 ± 0.30

Lower water content may indicate a lesser activity; as the lowest value from the optimisation is almost similar with the value obtained from the binder run. The runs with 25% catalyst indicate lower water contents except for the MCM 25%: ZSM 75% with 54.65%. This may indicate that primary Al-MCM-41 as guard bed increased the water content, thus more activity as compared to primary ZSM-5 with the similar ratio. As for the rest of the 25% catalyst, this might signify that the catalysts are deactivated quickly and affected the activity of the catalyst. The exceptional behaviour for MCM 25%: ZSM 75% indicate that Al-MCM-41 as a primary catalyst may have protected the secondary catalyst ZSM-5 in order for it to function.

8.2.2.2 Viscosity and Density

The viscosity for the optimisation experiments ranges from 1.46 cSt for the MCM 50%: ZSM 50% to 1.70 cSt for the ZSM 25%: MCM 75% run. In general, the values of viscosity for ZSM-5 as a primary catalyst are much higher than Al-MCM-41 as a primary catalyst with the similar ratio. Table 8-3 shows the viscosity and density for the bio-oils from the optimisation experiments.

Table 8-3. Viscosity and Density for the optimisation experiments

	Kinematic Viscosity (cSt)	Density (kg/m ³) @ 25 °C
ZSM 75%: MCM 25%	1.65	1058
ZSM 50%: MCM 50%	1.53	1051
ZSM 25%: MCM 75%	1.70	1056
Mixtures	1.68	1053
MCM 75%: ZSM 25%	1.56	1052
MCM 50%: ZSM 50%	1.46	1049
MCM 25%: ZSM 75%	1.56	1049

The density for the optimisation runs ranges from 1049 to 1058 kg/m³. For ZSM-5 as a primary catalyst, the lowest was obtained for ZSM 50%: MCM 50% with 1051 kg/m³ as compared to two runs from primary Al-MCM-41 catalyst for the 50% and 25% ratio with 1049 kg/m³. The density obtained from ZSM 100% run (1053 kg/m³) was lower than MCM 100% (1058 kg/m³) suggesting that ZSM-5 was a much stronger catalyst. But the result propose otherwise and were however much higher in general as compared to Al-MCM-41 as a primary catalyst. This occurrence explains that the primary catalyst is subjected to carbon deposition or coking faster than the secondary catalyst.

It is interesting to see that the lowest density was obtained when Al-MCM-41 was the primary catalyst. This illustrates that Al-MCM-41 has acted as a guard bed to crack the heavy compounds prior to the pyrolysis vapour coming in contact with a stronger secondary catalyst ZSM-5, thus further cracking the vapours.

8.2.2.3 Elemental analysis and heating values

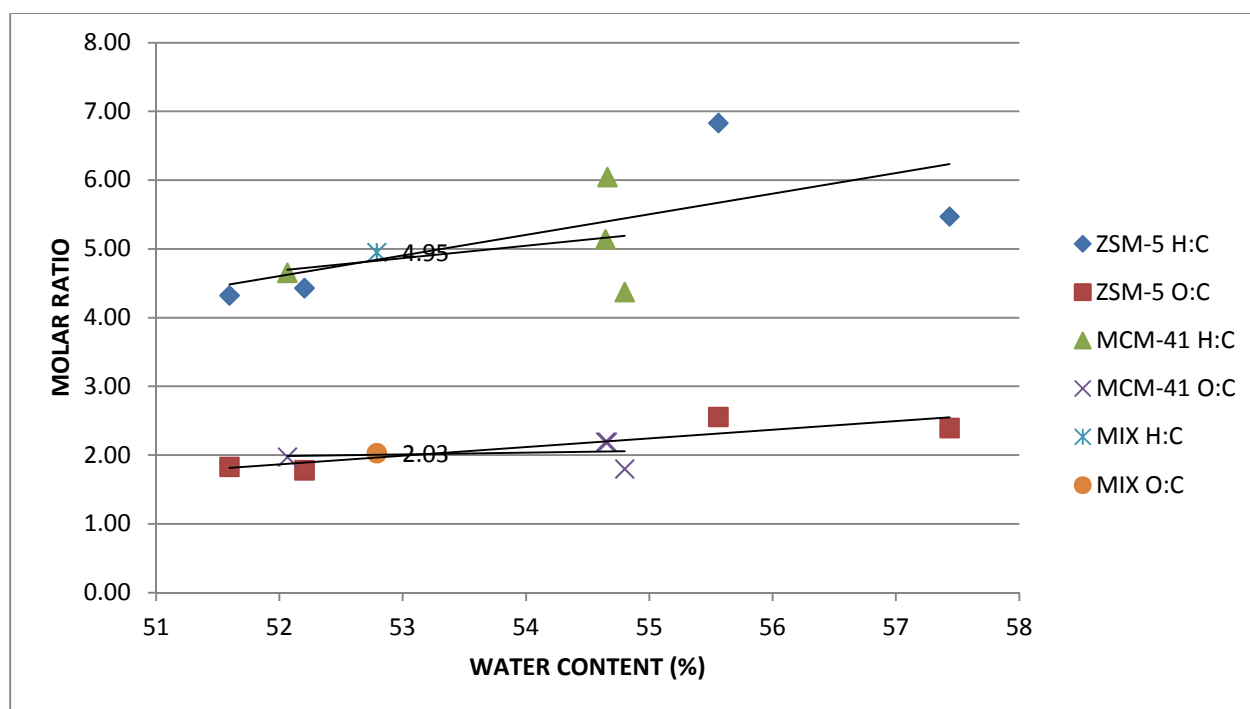
The elemental analysis, molar ratio and the HHV values for the optimisation experiments may be seen in Table 8-4. The carbon values for the optimisation experiments range from 21.49 to 26.67 wt. %. The values of oxygen were high, ranging from 63.35 to 68.60 wt. %. HHV in a wet basis from correlation of the elemental analysis show that the values range from 11.94 to 14.41 MJ/kg. Upon conversion to HHV in dry basis i.e. the exclusion of water content, the value increases to a range from 27.66 to 31.79 MJ/kg.

A van krevelan diagram can distinguish the effects of the catalysts in altering the values for H:C and O:C by plotting the H:C as a function of O:C. But, since the water contents differ for the bio-oils, the values are not comparable due to the inclusion of hydrogen and oxygen wt. % value in water. Therefore a graph of the molar ratios as a function of water content was plotted for the optimisation runs, which can be found in Figure 8-1.

Table 8-4. Elemental analysis, molar ratio and HHV values for the optimisation experiments

Optimisation runs	Ultimate Analysis (wt. %, dry basis)				Molar ratio		HHV (MJ/kg)	
	C	H	N	O	HC	OC	Wet basis	Dry basis
ZSM 75%: MCM 25%	26.67	9.85	0.15	63.35	4.43	1.78	14.35	30.02
ZSM 50%: MCM 50%	21.49	9.80	0.12	68.60	5.47	2.39	11.94	28.05
ZSM 25%: MCM 75%	26.25	9.46	0.22	64.08	4.32	1.83	13.67	28.24
Mixtures	24.24	10.00	0.18	65.59	4.95	2.03	13.44	28.48
MCM 75%: ZSM 25%	24.84	9.64	0.18	65.35	4.65	1.97	13.26	27.66
MCM 50%: ZSM 50%	26.52	9.66	0.22	63.61	4.37	1.80	14.05	31.08
MCM 25%: ZSM 75%	22.95	9.83	0.18	67.05	5.14	2.19	12.65	27.89

The indicators for H:C and O:C are plotted with four points ranging from 25%, 50%, 75% and 100% of each as a primary catalyst, either ZSM-5 or Al-MCM-41. The molar ratios for the physically-mixed catalyst run were also plotted in the graph. A trendline is drawn for the HC and OC molar ratio to show the variation for ZSM-5 and Al-MCM-41 each as primary catalysts. As mentioned in Chapter 7, the high value for the molar ratio was due to the inclusion of the hydrogen and oxygen from water and does not correlate with the water content. Since the calculated HC value was from an as-received basis, the HC molar ratio of greater than a value of 2 was obtained.

**Figure 8-1.** H:C and O:C molar ratio vs. water content for the optimisation experiments

ZSM-5 as a primary catalyst can be seen to increase the HC molar ratio more as compared to Al-MCM-41 due to the steeper gradient. This shows that the water content was also increased. All the plots for Al-MCM-41 as a primary catalyst however show that they do not increase the water content as much as ZSM-5 100% and ZSM 50%: MCM 50%.

ZSM-5 also tends to increase the OC molar ratio which can be seen from a steeper gradient of the OC trendline. However, a higher OC molar ratio is unfavourable for the bio-oil. The HC and OC molar ratio for the physically mixed catalysts can be seen to position itself at the intersection between where the lines for ZSM-5 and Al-MCM-41 meet.

8.2.2.4 Acidity (pH)

The acidity of the bio-oil subject to the optimisation experiments range from 2.65 to 2.95. Table 8-5 shows the pH values for the optimisation runs. The highest pH was obtained for MCM 75%: ZSM 25% with 2.95 and was followed closely by ZSM 50%: MCM 50% with 2.94. The pH for the physically-mixed catalysts fared the lowest with a value of 2.65, showing the ineffectiveness in reducing acidity in the bio-oil.

From a rough inspection of the pH values, it appears that it is much better to subject Al-MCM-41 as a primary catalyst than the secondary catalyst due to the tendency of the pH values to be higher. However, a high pH value was also obtained from a similar catalyst ratio (ZSM 50%: MCM 50%) if Al-MCM-41 is to be placed as a secondary catalyst. It can therefore be concluded from the trend, that the catalyst combination with a similar ratio has significantly improved the pH value.

Table 8-5. Acidity (pH) for the optimisation experiments

Catalytic optimisation runs	pH
ZSM 75%: MCM 25%	2.68
ZSM 50%: MCM 50%	2.94
ZSM 25%: MCM 75%	2.76
Mixtures	2.65
MCM 75%: ZSM 25%	2.95
MCM 50%: ZSM 50%	2.80
MCM 25%: ZSM 75%	2.85

8.2.2.5 GC-MS analysis

The chemical peaks features a total of 102 chemicals detected and identified from the GC-MS. The chemical compounds and group, retention time, chemical formula and relative molecular mass may be found in Table 7-6 in Chapter 7. In Table 8-6, the peak area percentages with the respective peak numbers for the various chemicals from the optimisation experiments is listed.

Table 8-6. Peak area percentages of the various compounds detected from the optimisation experiments

Peak #	ZSM 25%: MCM 75%	ZSM 50%: MCM 50%	ZSM 75%: MCM 25%	Mixtures	MCM 25%: ZSM 75%	MCM 50%: ZSM 50%	MCM 75%: ZSM 25%
1	0.00	1.23	0.72	0.26	0.73	0.80	0.52
2	0.63	1.09	0.75	0.87	0.92	1.18	1.01
3	0.07	0.19	0.17	0.17	0.20	0.20	0.18
4	0.08	0.15	0.08	0.12	0.13	0.13	0.12
5	0.08	0.14	0.13	0.08	0.08	0.13	0.11
6	0.12	0.45	0.31	0.29	0.41	0.46	0.38
7	0.42	0.78	0.62	0.61	0.75	0.80	0.69
8	10.01	9.72	9.09	12.87	11.06	13.10	12.66
9	0.46	0.56	0.54	0.63	0.63	0.71	0.65
10	1.75	1.76	2.24	2.42	2.21	2.26	2.55
11	0.00	0.00	0.00	0.00	0.00	0.00	0.00
12	0.24	1.12	0.51	0.65	0.79	0.94	0.79
13	0.05	0.21	0.07	0.09	0.09	0.10	0.08
14	0.25	0.31	0.29	0.32	0.32	0.39	0.34
15	1.54	1.66	1.51	1.97	1.54	2.09	2.02
16	0.53	0.54	0.56	0.65	0.56	0.74	0.67
17	1.78	1.88	1.96	2.16	1.88	1.99	2.06
18	0.09	0.24	0.12	0.18	0.18	0.23	0.17
19	0.31	0.31	0.32	0.32	0.09	0.42	0.27
20	0.13	0.42	0.19	0.25	0.32	0.31	0.30
21	0.42	0.00	0.36	0.44	0.39	0.18	0.44
22	0.25	0.23	0.24	0.26	0.22	0.25	0.25
23	0.61	0.40	0.67	0.59	0.38	0.66	0.63
24	0.27	0.31	0.28	0.30	0.20	0.38	0.32
25	0.04	0.00	0.00	0.32	0.00	0.08	0.00
26	0.00	0.15	0.06	0.07	0.07	0.08	0.06
27	6.75	7.73	7.01	7.64	8.42	8.69	7.98
28	0.50	0.25	0.33	0.52	0.41	0.42	0.70
29	0.44	0.00	0.31	0.21	0.34	0.24	0.25
30	2.90	2.88	3.21	3.38	3.11	3.02	3.03
31	0.54	0.67	0.57	0.67	0.68	0.65	0.80
32	0.48	0.49	0.59	0.50	0.51	0.51	0.56

33	1.05	1.18	1.00	1.15	1.21	1.34	1.08
34	0.72	0.83	0.73	0.77	0.81	0.83	0.74
35	0.12	0.18	0.17	0.13	0.15	0.17	0.13
36	0.20	0.23	0.21	0.23	0.23	0.24	0.20
37	2.37	2.40	2.96	2.41	2.37	2.36	2.75
38	0.84	0.86	0.81	0.78	0.93	0.86	0.77
39	0.61	0.00	0.00	0.68	0.44	0.00	0.30
40	0.35	0.30	0.32	0.36	0.31	0.32	0.23
41	0.22	0.29	0.23	0.24	0.25	0.24	0.22
42	0.90	1.28	0.91	0.87	0.88	0.88	0.82
43	1.18	0.99	1.39	1.21	1.12	1.02	1.14
44	0.61	0.66	0.57	0.66	0.45	0.72	0.60
45	0.36	0.37	0.39	0.32	0.35	0.31	0.24
46	0.59	0.31	0.53	0.49	0.31	0.39	0.34
47	0.09	0.16	0.06	0.10	0.05	0.08	0.12
48	0.29	0.32	0.30	0.28	0.28	0.28	0.29
49	4.25	3.91	4.30	4.15	4.12	4.09	4.04
50	0.44	0.42	0.42	0.44	0.41	0.44	0.40
51	0.28	0.24	0.27	0.38	0.28	0.40	0.21
52	2.94	3.58	2.87	3.25	3.41	3.60	3.40
53	8.22	6.28	7.47	7.28	7.48	6.72	7.27
54	0.31	0.29	0.27	0.23	0.27	0.24	0.20
55	0.88	1.28	0.93	1.09	1.16	1.24	1.19
56	0.26	0.21	0.26	0.33	0.26	0.27	0.36
57	0.78	0.69	0.77	0.69	0.66	0.63	0.63
58	0.40	0.40	0.39	0.36	0.35	0.42	0.40
59	0.19	0.19	0.17	0.23	0.27	0.20	0.20
60	0.25	0.33	0.22	0.27	0.28	0.13	0.26
61	1.57	1.90	1.54	1.68	1.73	1.82	1.71
62	0.91	1.33	1.09	0.86	0.95	1.20	0.98
63	0.38	0.21	0.24	0.26	0.38	0.18	0.23
64	0.25	0.30	0.27	0.27	0.29	0.31	0.28
65	1.40	1.33	1.24	1.28	1.60	1.20	1.31
66	4.50	3.06	4.01	3.54	3.66	3.15	3.54
67	0.26	0.22	0.22	0.69	0.72	0.80	0.74
68	0.55	0.90	0.57	0.11	0.14	0.12	0.13
69	0.40	0.35	0.39	0.31	0.37	0.30	0.31
70	0.13	0.10	0.08	0.08	0.11	0.09	0.09
71	0.23	0.33	0.22	0.23	0.24	0.26	0.27
72	3.16	3.58	3.22	2.63	3.13	2.87	2.68
73	0.26	0.27	0.23	0.18	0.20	0.16	0.19
74	0.17	0.11	0.08	0.09	0.08	0.10	0.10
75	0.17	0.36	0.18	0.07	0.13	0.11	0.10
76	0.09	0.10	0.09	0.11	0.13	0.11	0.11
77	3.45	2.44	2.93	2.31	2.57	2.07	2.32

78	0.20	0.34	0.22	0.19	0.24	0.23	0.20
79	0.47	0.53	0.49	0.53	0.44	0.43	0.48
80	0.63	0.76	0.67	0.73	0.73	0.70	0.74
81	0.28	0.25	0.22	0.24	0.19	0.19	0.20
82	0.16	0.10	0.00	0.07	0.05	0.06	0.00
83	3.77	3.35	4.23	3.52	3.34	3.45	3.41
84	3.44	2.56	3.49	2.72	2.42	2.44	2.58
85	0.41	0.37	0.39	0.26	0.27	0.25	0.26
86	0.57	0.46	0.54	0.40	0.41	0.35	0.38
87	0.35	0.51	0.41	0.43	0.55	0.44	0.32
88	1.33	1.07	1.30	0.97	1.03	0.82	0.97
89	0.56	0.33	0.49	0.44	0.44	0.30	0.68
90	0.12	0.13	0.12	0.08	0.11	0.08	0.09
91	0.10	0.07	0.12	0.10	0.09	0.09	0.08
92	2.12	1.49	1.79	1.47	1.33	1.20	1.28
93	1.22	1.22	1.18	0.93	1.09	0.90	0.97
94	0.55	0.46	0.51	0.43	0.50	0.37	0.48
95	0.19	0.40	0.33	0.27	0.37	0.25	0.26
96	0.36	0.35	0.32	0.18	0.21	0.13	0.20
97	0.44	0.42	0.40	0.28	0.41	0.30	0.29
98	0.95	0.86	0.85	0.56	0.64	0.46	0.58
99	0.22	0.58	0.37	0.17	0.30	0.24	0.20
100	0.26	0.31	0.23	0.10	0.14	0.10	0.11
101	1.49	1.86	1.64	0.90	1.40	0.71	0.87
102	0.43	0.31	0.36	0.14	0.19	0.10	0.16
TOTAL	100.00	100.00	100.00	100.00	100.00	100.00	100.00

The discussion for the GC-MS will be divided into two sections: ZSM-5 and Al-MCM-41 as the primary catalyst and vice versa. The effects of the individual catalysts ZSM-5 100% and Al-MCM-41 100% on the pyrolysis vapours were included in the graph plots as a comparison. Individual chemicals of from aromatic hydrocarbons, phenols, organic acids and a selection of the major chemicals were examined.

8.2.2.5.1 ZSM-5 as the primary catalyst

This section discusses the changes in the chemical peak areas with respect to the ratio for primary ZSM-5 catalyst. Figure 8-2 shows the aromatic hydrocarbon peak areas with respect to the ZSM-5 ratio. Toluene and xylenes were the highest aromatics detected and were seen to compete in certain ratios. The production of toluene and xylene was hindered when the ratio of the catalysts was 25% for either ZSM-5 (ZSM 25: MCM 75) or for Al-MCM-41 (ZSM 75: MCM 25), and was suspected due to catalyst deactivation. One might suggest that the

coke/char may have deteriorated the aromatic hydrocarbon values. But based on a previous study by Pattiya on the catalytic pyrolysis of biomass with char, the peak areas for toluene and xylenes did not changed [24]. Therefore this can only mean the occurrence of catalyst deactivation, and excluded the effects of char on both the chemical peak areas.

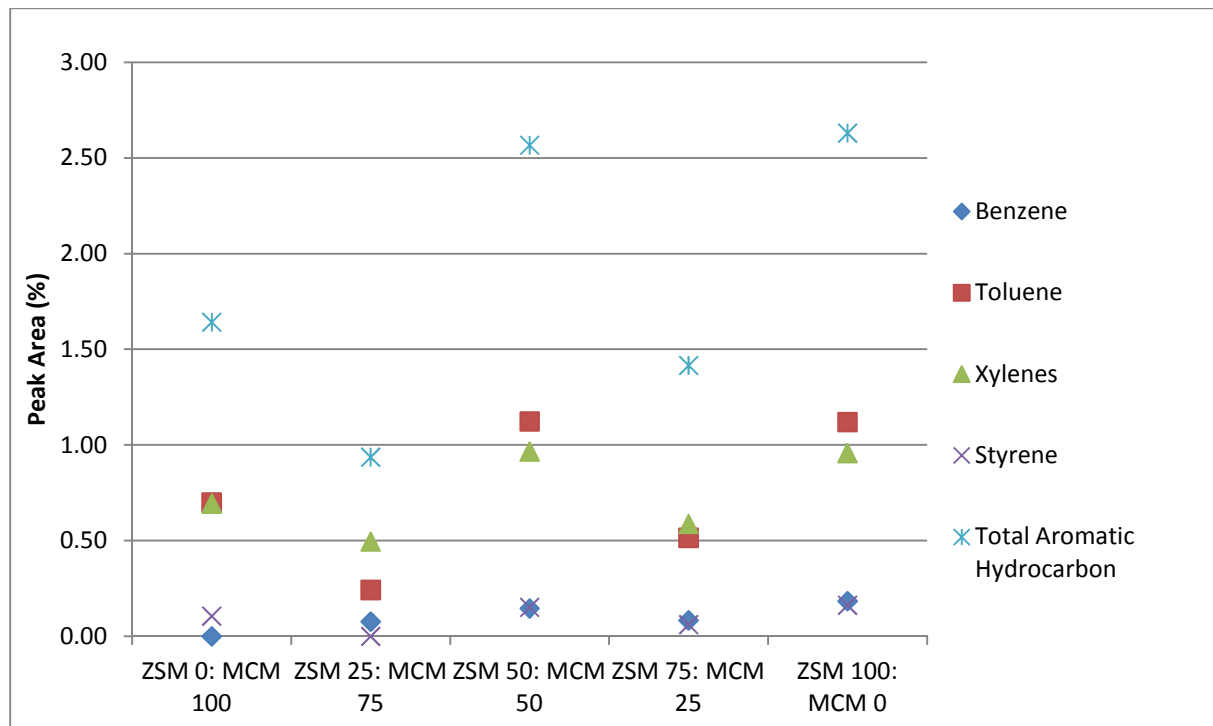


Figure 8-2. Aromatic hydrocarbon peak areas for ZSM-5 as a primary catalyst

The reduction in peak areas for toluene and xylenes was much greater for 25% ZSM-5 than 25% Al-MCM-41. This was expected due to the higher increase in aromatic hydrocarbon for ZSM-5 100% than Al-MCM-41 100%. The synergy for the 50% ratio can be seen to be almost identical to the catalytic run with ZSM 100% for the production of aromatic hydrocarbons. The total peak areas for aromatic hydrocarbons show that the changes are dominated by the varying values from toluene and xylenes.

The highest organic acid peak area was obtained for acetic acids, amongst others such as propanoic acid and o-coumaric acid. It was seen that for propanoic acid, there was no effect of increasing the ZSM-5 content. As for the acetic acid, the peak area seems to have shown a slight increase from 0 to 25%, decreasing from 25 to 75%, and an increase from 75 to 100% ratio content. The total organic acid is seen to be dominated by the peak areas from acetic acid. The individual and total organic acid peak areas for ZSM-5 primary catalyst can be seen in Figure 8-3.

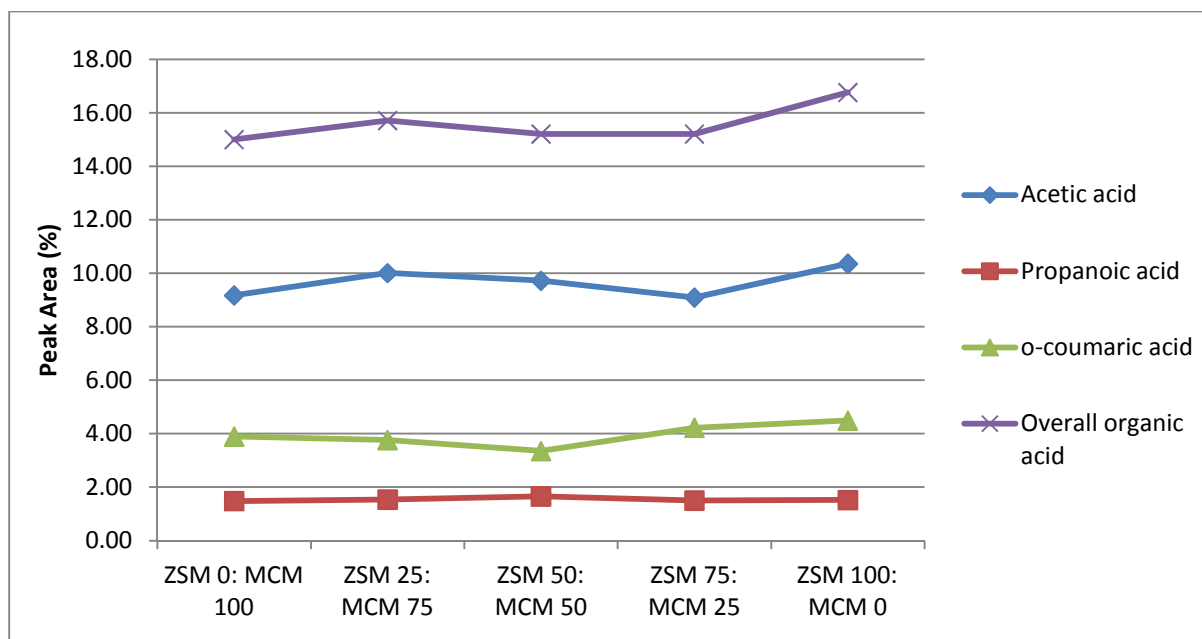


Figure 8-3. Organic acids peak areas for ZSM-5 as a primary catalyst

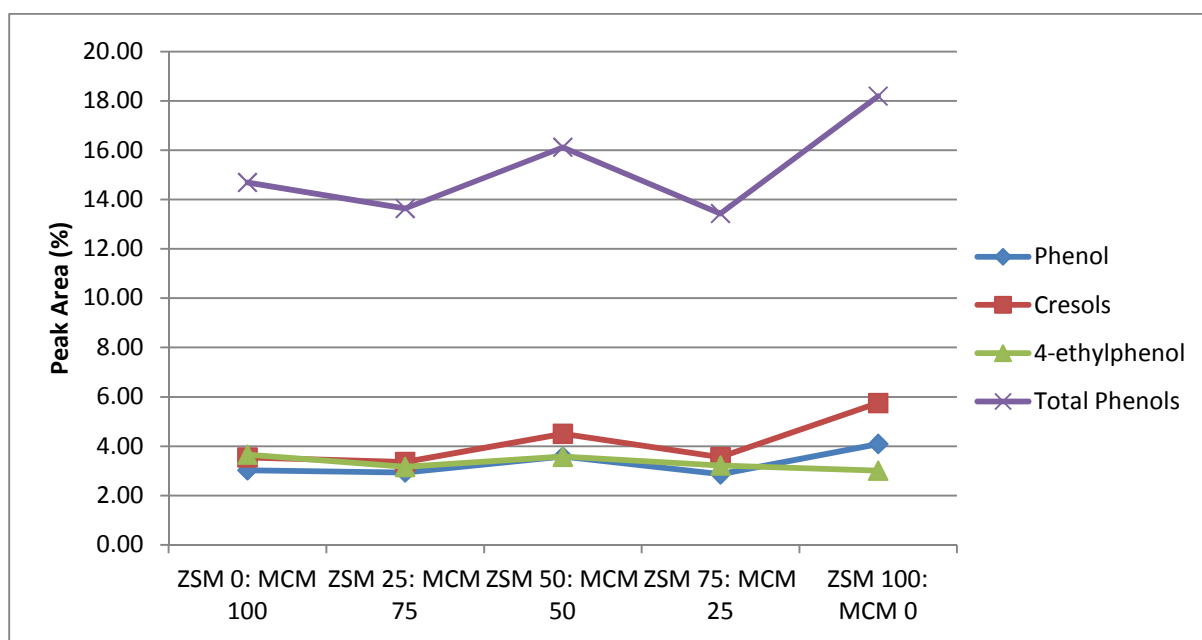


Figure 8-4. Phenols peak areas for ZSM-5 as a primary catalyst

Figure 8-4 shows the phenols peak areas for primary ZSM-5 ratios. The trend for phenol and cresols is that the peak area increases as the ratio of ZSM-5 increases. A reverse trend was shown for 4-ethylphenol instead. Cresol peak areas show the closest resemblance to the overall phenol peak area trend.

Other notable chemicals such as furfural, guaiacol, levoglucosan, 2-furanmethanol and 3-methyl-1,2-cyclopentanedione can be found in Figure 8-5. The guaiacol and furfural 'zigzag' trend shows that it is significantly affected by the catalyst deactivation. As the ratio of ZSM-5 increases, the guaiacol and levoglucosan peak area tends to decrease, and increases for furfural. The trend for 2-furan methanol shows that pure catalysts increased the peak area compared to the combined catalysts.

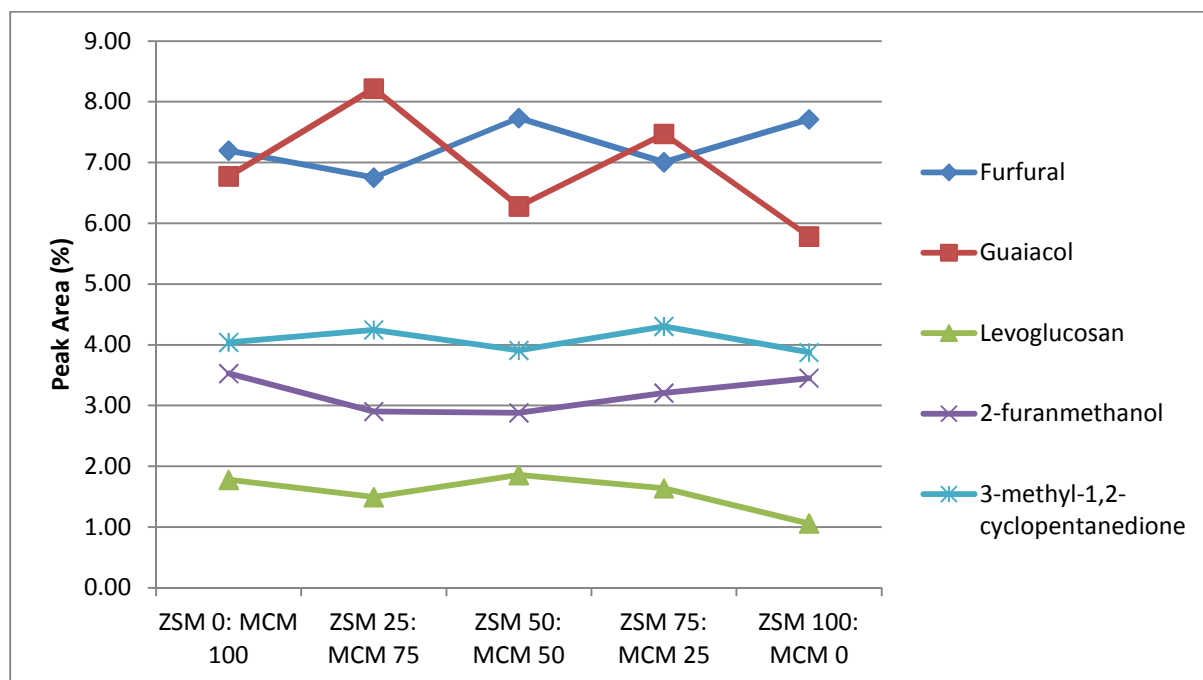


Figure 8-5. Selected chemical peak areas for ZSM-5 primary catalyst

8.2.2.5.2 Al-MCM-41 as the primary catalyst

This section discusses the changes in the chemical peak areas with respect to the ratio for primary Al-MCM-41 catalyst. The aromatic hydrocarbon peak area for Al-MCM-41 as a primary catalyst is illustrated in Figure 8-6. The peak area for overall aromatic hydrocarbon generally decreases as the ratio of Al-MCM-41 increases. The low aromatic hydrocarbon ratio of Al-MCM-41 at 25% may indicate a deactivation in the catalyst. The decrease is generally stable for the peak area for aromatic hydrocarbon from 50% to 100% Al-MCM-41.

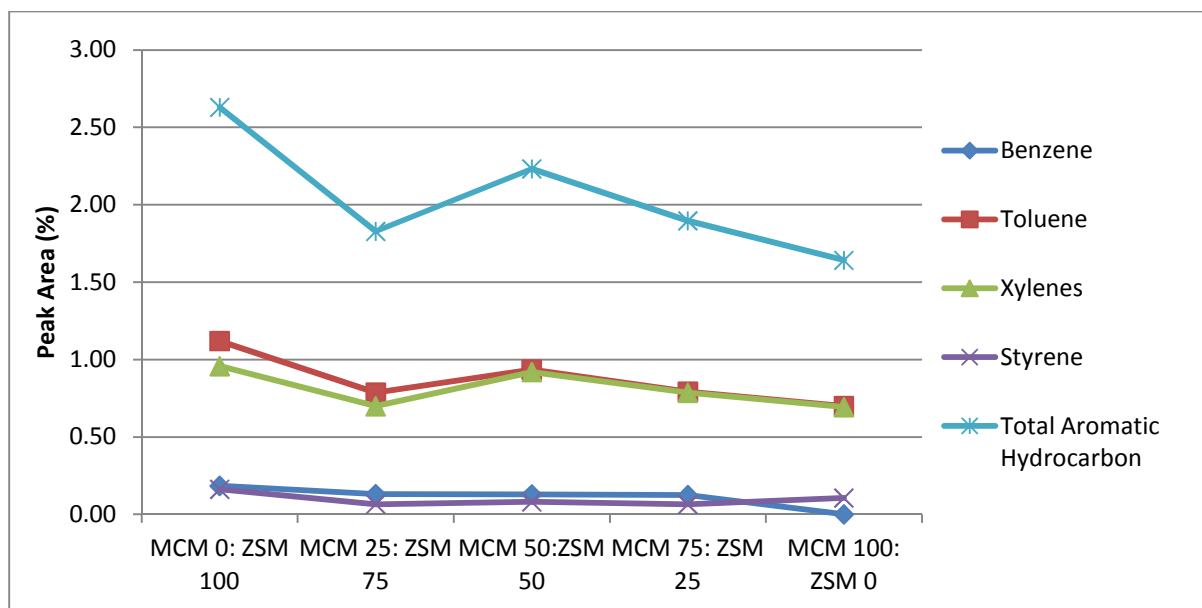


Figure 8-6. Aromatic hydrocarbon peak areas for Al-MCM-41 as a primary catalyst

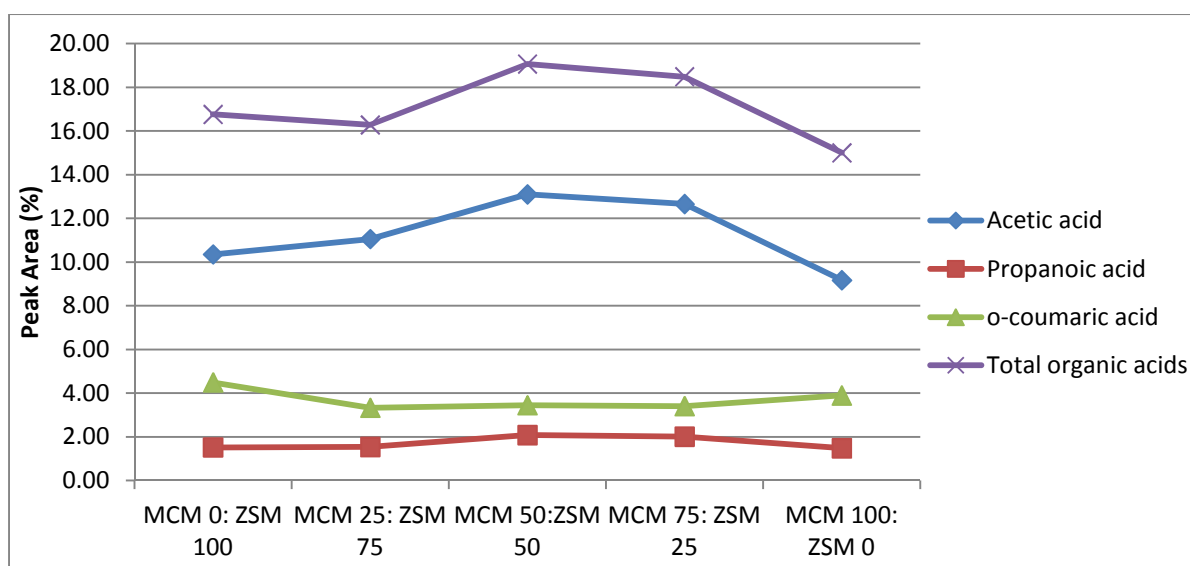


Figure 8-7. Organic acids peak area for Al-MCM-41 as a primary catalyst

The peak area for the organic acids for primary Al-MCM-41 catalyst is shown in Figure 8-7. The trend showed an increased in the organic acids peak area showing that Al-MCM-41 as a primary catalyst is deactivated easily and lost its main catalytic function. The increase in the peak area was seen from 25 to 75% ratio, with the maximum at 50% ratio. The peak area gradually decreases from 75% to 100% Al-MCM-41.

The phenol peak area is shown to decrease with the increase in the Al-MCM-41 ratio as a catalyst (Figure 8-8). A sharp decrease can be seen from 0% to 25% Al-MCM-41, then fairly constant towards the 100% Al-MCM-41 value. This shows that the secondary catalyst ZSM-5 has a very high influence on the total phenol increase. However, an increase in the Al-MCM-41 ratio increases the value of 4-ethylphenol.

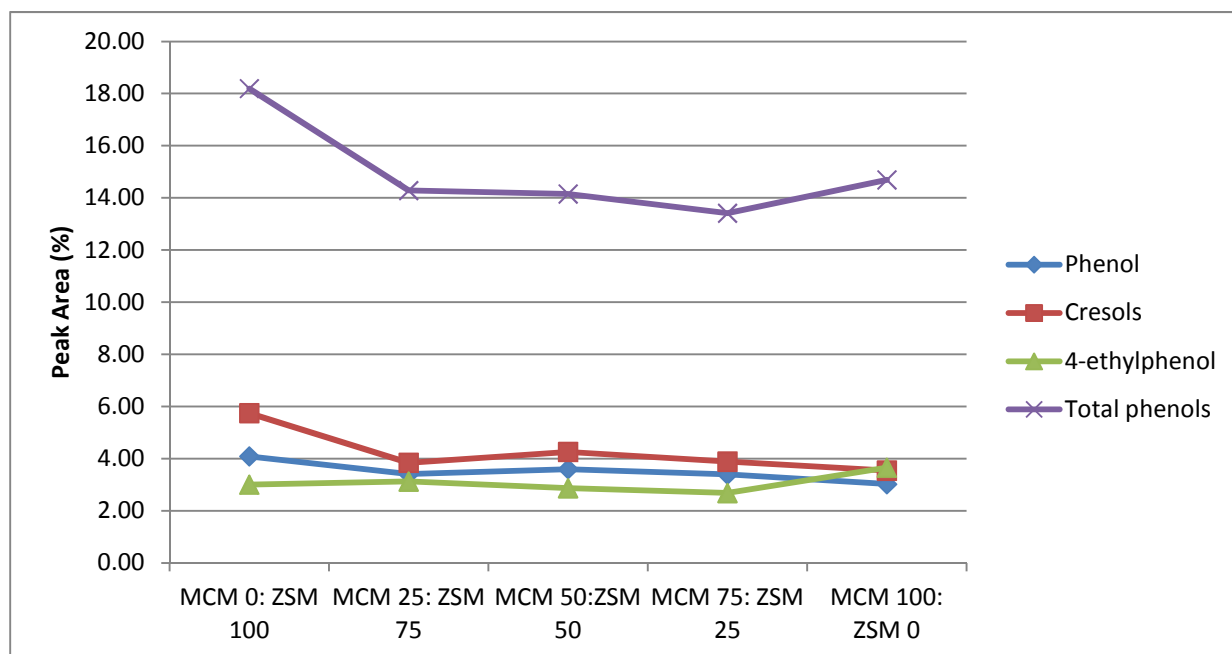


Figure 8-8. Selected phenols peak area for Al-MCM-41 as a primary catalyst

Figure 8-9 shows various chemicals as a function of the ratio increase for Al-MCM-41 as a primary catalyst. Furfural showed a steady increase from a ratio of 0% to 50% and then gradually decreasing towards the 100% ratio. This confirmed that the equal catalyst ratio combination with Al-MCM-41 as the primary catalyst favoured the production of furfural. Guaiacol value increases from 0% to 25%, and then gradually decreasing towards 100% ratio. The selected ketone 3-methyl-1,2-cyclopentanedione and alcohol 2-furanmethanol is seen to be fairly stable showing no effect towards the increase in the Al-MCM-41 ratio. Levoglucosan peak area was the lowest for the 50% value, and tends to increase the peak area towards 100% Al-MCM-41.

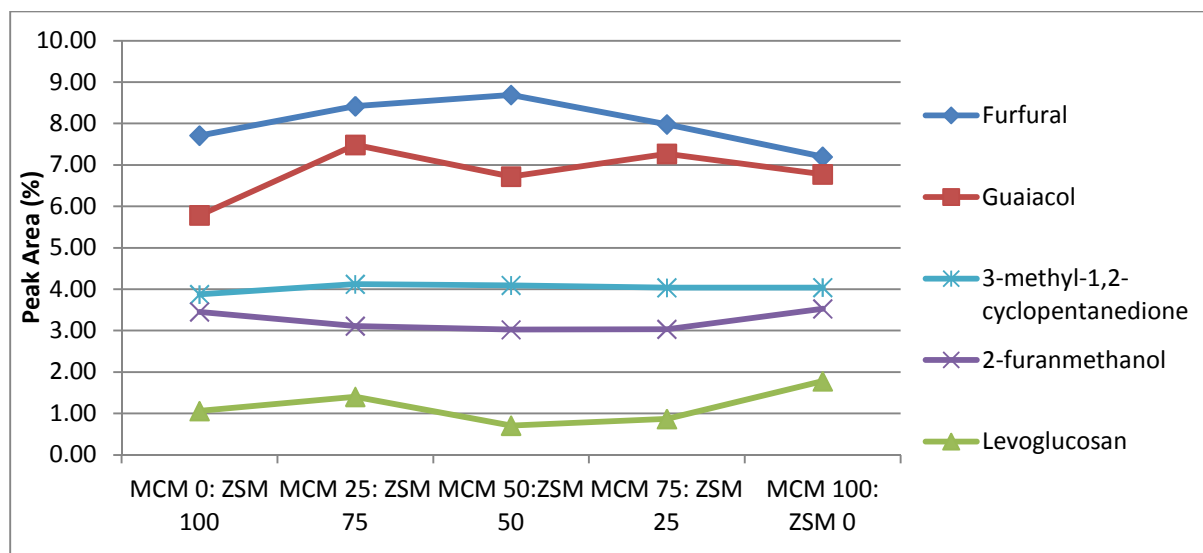


Figure 8-9. Peak area of selected chemicals for Al-MCM-41 as a primary catalyst

8.3 General remarks

8.3.1 Catalytic effects as a primary or secondary catalyst

Being the primary catalyst essentially means that it indirectly acts as a guard bed whilst performing its ability as a catalyst. There are differences in the peak areas for the various chemicals on where the catalysts are positioned. For aromatic hydrocarbons and phenols comparison, it seems sensible to portray the data with respect to ZSM-5 due to the production effectiveness of aromatic hydrocarbon and phenols by ZSM-5. As for the organic acids, the data is represented with respect to Al-MCM-41, due to the inhibiting nature of Al-MCM-41 on the organic acids. For example, if ZSM-5 is stated the primary catalyst, then by default the secondary catalyst is Al-MCM-41. This also applies to the ratio of the catalysts; if ZSM-5 25% is stated, then the ratio for Al-MCM-41 is 75%.

The production of aromatics for the 50% ZSM-5 primary results was almost similar to the 100% ZSM-5. But when it is switched as a secondary catalyst, the production of toluene was seen to decrease. However, the positioning of ZSM-5 as a primary catalyst hampered the production of aromatic hydrocarbon for the 25% and 75% ratio. Regardless of the higher or lower ratio catalyst, the production of aromatic hydrocarbon is less than with ZSM-5 50% ratio. Figure 8-10 shows the individual aromatic hydrocarbons with respect to ZSM-5 for the various ratio and position.

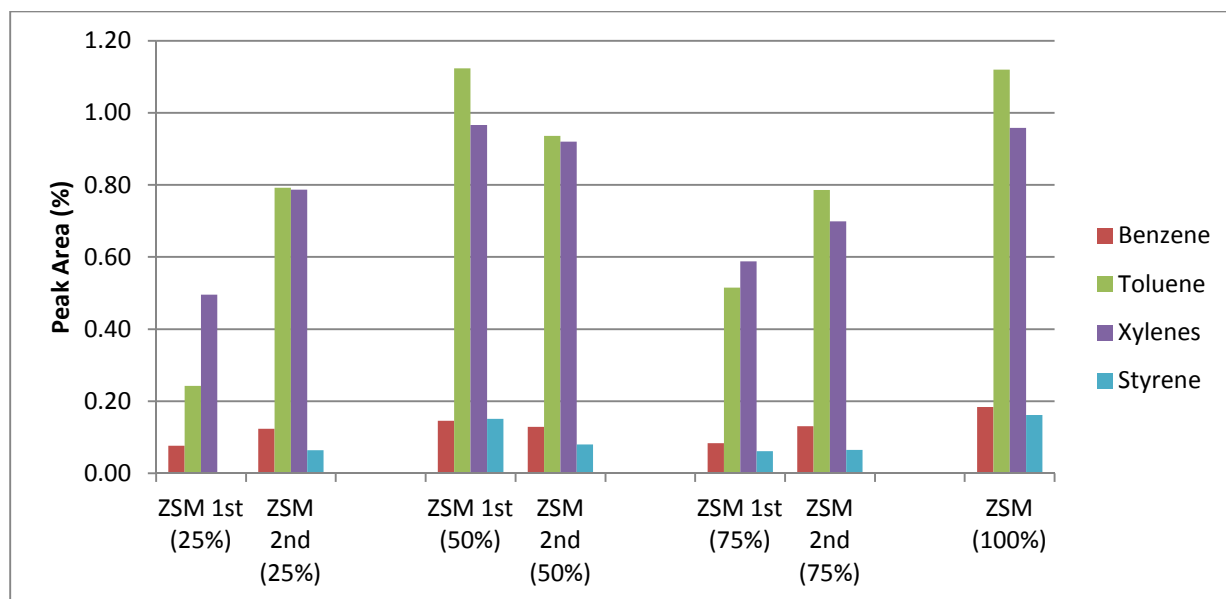


Figure 8-10. Individual aromatic hydrocarbon peak areas with respect to ZSM-5

It may be that as a catalyst deactivated, other undesirable reactions will proceed, and in this case lead to the suppression of hydrocarbon production. Coke formation is known to be a major competing reaction to aromatic production, indicating parallel pathways [63]. Therefore, a sign of catalyst deactivation can be sensed from the reduction of aromatic hydrocarbon formation. As the reactions are in series, it will be inevitable that the pyrolysis vapours will pass through whichever catalyst that is deactivated first.

By subjecting ZSM-5 as a primary catalyst, a reduction in the aromatic peak area can already be seen when compared to placing it as a secondary catalyst (Figure 8-11). The reduction in the 25% may be associated with ZSM-5 deactivation and for the 75% with Al-MCM-41 deactivation, as it is much more significant with the former than the latter. However for the equal ratio of both catalysts (50:50), a high aromatic hydrocarbon peak area was obtained almost similar to ZSM 100%. It can therefore be suggested that an imbalance in the ratio affects the catalyst activity, i.e. a lower catalyst ratio will deactivate much faster. As for secondary ZSM-5 catalyst, the increase in catalyst ratio is much stable due to the presence of Al-MCM-41 guard bed.

As for the phenols, it appears that it is better to subject ZSM-5 as a primary catalyst, due to the tendency to increase the phenols especially with the identical ratio. Although for secondary ZSM-5, the production of phenol with the combined ratio is much more stable.

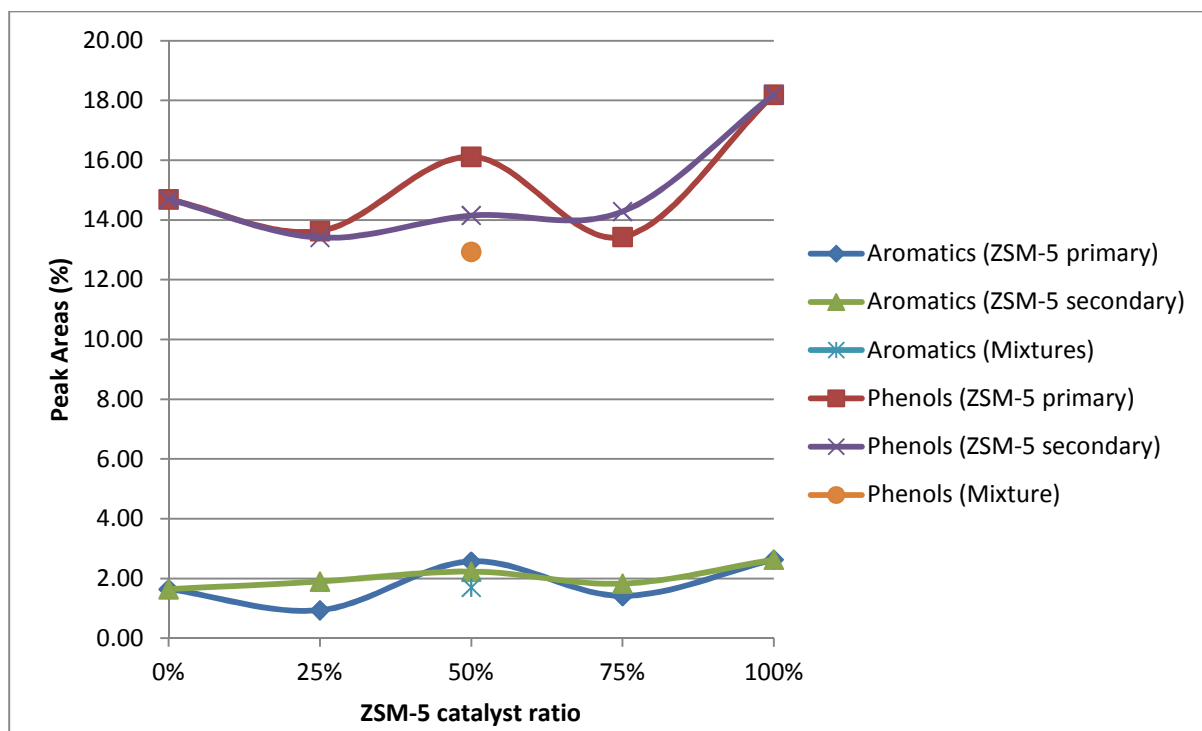


Figure 8-11. Aromatic hydrocarbon and phenols peak area with respect to ZSM-5 catalyst ratio

The individual organic acids show that majority of the changes are due to acetic acid peak area. Organic acids tend to decrease when Al-MCM-41 is positioned as a secondary catalyst as compared to the primary catalyst. Figure 8-12 shows the peak area for the individual organic acids for both primary and secondary Al-MCM-41.

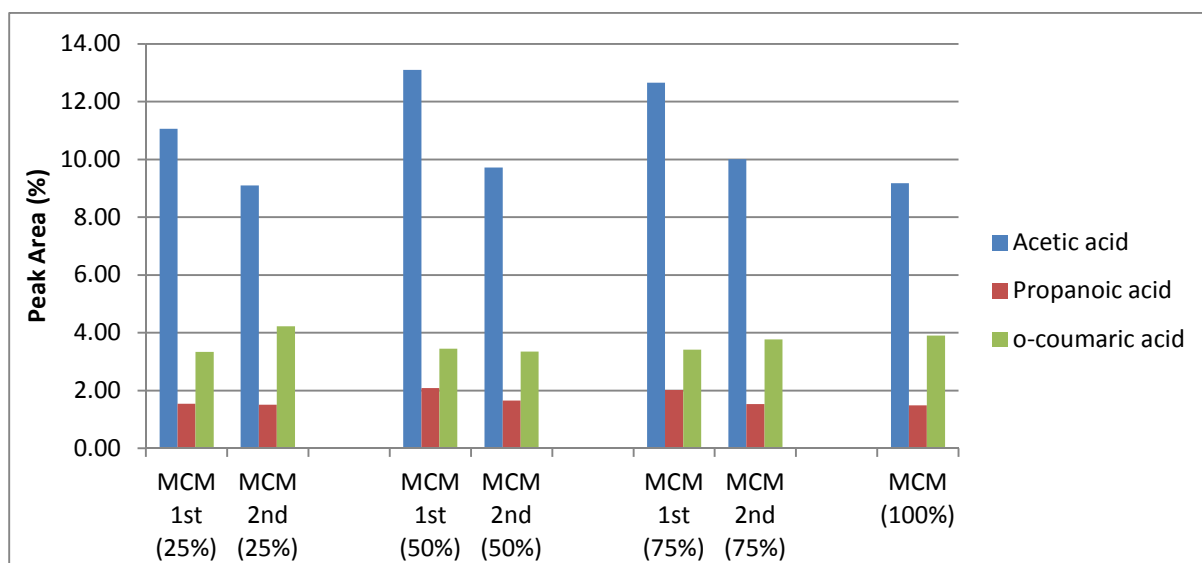


Figure 8-12. Organic acids peak areas with respect to Al-MCM-41

A closer view may also be observed from the graph (Figure 8-13) of the organic acids peak area and pH with respect to the ratio of Al-MCM-41. The pH and organic acids can be seen to correlate; as the organic acid peak area increased, the pH value of the bio-oil decreases although a difference in value is seen for the various arrangements even if it is for the same ratio.

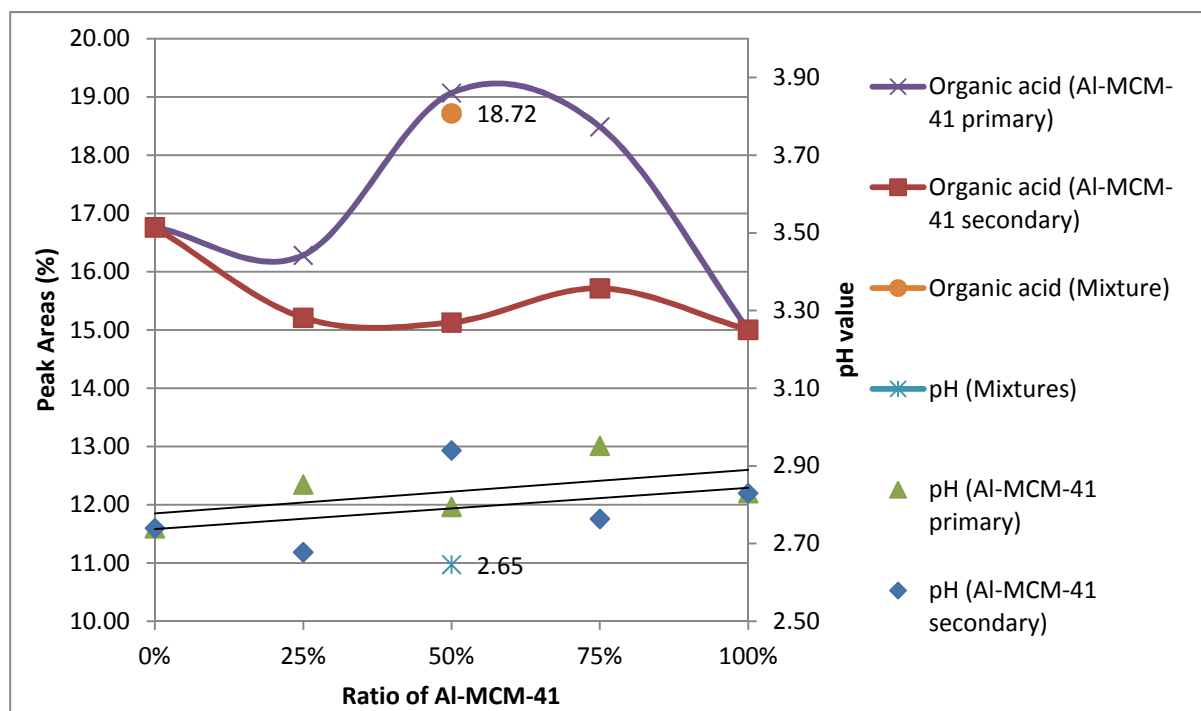


Figure 8-13. pH and organic acid peak area vs. ratios of the Al-MCM-41

The general rule for the pH value is that if the value increases, it means that the acidity is decreased. The trendline for the pH values for both primary and secondary Al-MCM-41 was drawn. It was shown to increase the pH which concluded that an increase in the Al-MCM-41 ratio increases the pH. As the acidity of the bio-oil is very likely due to the organic acids in the bio-oil, it would be suitable to discuss the peak areas of the organic acids from the aspect for the various ratios of Al-MCM-41 catalyst.

By examining Figure 8-13, we notice that Al-MCM-41 as a primary catalyst is not as effective in reducing the organic acids compared to Al-MCM-41 as a secondary catalyst. By placing Al-MCM-41 as a primary catalyst, it acts as a guard bed and loses its function to reduce the organic acid peak area. This is an indication that Al-MCM-41 deactivates easily as compared to ZSM-5 which is analysed from the high organic acid peak area from primary Al-MCM-41 compared to any of the ratios from secondary Al-MCM-41.

The gradient from 25% to 50% ratio for the primary Al-MCM-41 catalyst is much steeper as compared to the secondary catalyst run. The increase in the Al-MCM-41 ratio should show a decrease in the organic acid peak area, which is seen from both primary and secondary Al-MCM-41 for ratios from 50% to 100%. Therefore, the sharp gradient for the primary Al-MCM-41 is attributed to the catalyst deactivation.

One might also suggest that after the pyrolysis vapours pass through primary Al-MCM-41, it is subjected to further cracking by ZSM-5 which may increase the amount of organic acids in the bio-oil. But in effect, the run for ZSM-5 100% only reached a peak area of 16.76%, which was surpassed by MCM 50% with a value of 19.07%. Therefore it can be concluded that Al-MCM-41 catalyst deactivation is a major limiting factor towards the reduction of the organic acids if it were placed as a primary catalyst.

As for the physically-mixed catalyst, it can be deduced that it has almost a similar trait as Al-MCM-41 primary, and does not reduce the organic acid peak area as much as the introduction of Al-MCM-41 as a secondary catalyst.



Figure 8-14. Reaction chemistry for the catalytic pyrolysis of glucose with ZSM-5 [134]

A model proposed by Carlson et al. from the pyrolysis of glucose with HZSM-5 [134], showed a competition between dehydration and the fragmentation reaction for the formation of anhydrosugars and aromatics (Figure 8-14). Previous study by Carlson et. al showed that similar aromatic selectivity and yields were obtained for both glucose and cellulose [118]. It is therefore relevant to make a comparison, since majority of the structural component in BRH contains cellulose.

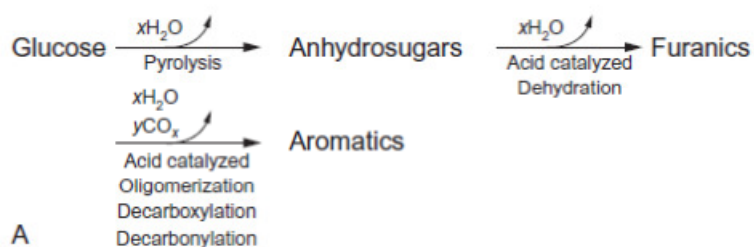


Figure 8-15. Pathway for the aromatic formation from glucose over ZSM-5

The graph for ZSM-5 as a secondary catalyst demonstrates the ideal pattern for these model, indicating the competition between both aromatics and anhydrosugars chemical groups. For the graph of ZSM-5 as primary catalyst, the pattern was shifted showing a similarity in the graphs for furans and aromatics although different in peak areas. As the primary position is susceptible to catalyst deactivation as compared to the secondary position, this due to the coke formation on the ZSM-5 catalyst.

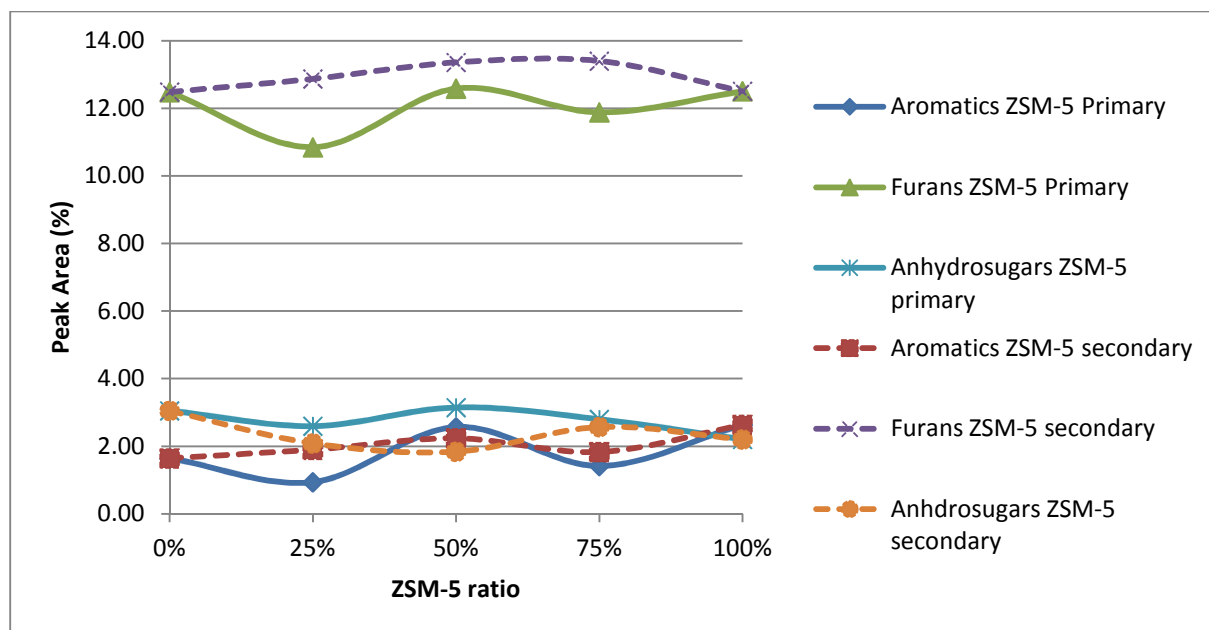


Figure 8-16. Peak areas for furans, aromatics and anhydrosugars for primary and secondary ZSM-5 catalyst

The peak areas for furans and aromatics were observed to be generally lower for primary ZSM-5 compared to secondary ZSM-5. This can be seen from the decrease in both peaks for 25% and 75% ZSM-5 ratio percentages. Therefore, the similarity in the patterns is likely due to the competition of both the furans and aromatics, with the formation of coke. A simplistic pathway can also be seen in Figure 8-15.

The individual chemicals peak area were categorised in their respective chemical groups to get an overall sense on the effect of the catalyst combination and ratio. The total peak areas of the chemical groups for the bio-oils from the catalytic optimisation runs may be found in Table 8-7.

Table 8-7. Total peak areas of the chemical groups for the bio-oils from the catalytic optimisation run

	ARH	OA	EST	FUR	ALD	KET	ALC	PHE	GU	SYR	ANH	MISC	NCC
ZSM 75%: MCM 25%	1.42	15.21	1.18	11.88	0.78	16.78	5.85	13.43	22.33	1.66	2.80	3.84	2.84
ZSM 50%: MCM 50%	2.57	15.13	1.48	12.59	0.79	16.28	5.87	16.12	18.26	1.38	3.15	4.11	2.28
ZSM 25%: MCM 75%	0.94	15.72	0.97	10.85	0.66	16.45	5.74	13.63	24.63	1.76	2.59	3.67	2.39
Mixtures	1.70	18.72	1.36	12.45	0.68	17.19	6.08	12.94	19.29	1.11	2.16	3.30	3.01
MCM 75%: ZSM 25%	1.90	18.49	1.55	12.87	0.79	16.57	5.68	13.41	19.26	1.13	2.09	3.30	2.97
MCM 50%: ZSM 50%	2.23	19.07	1.66	13.36	0.71	16.91	5.83	14.15	17.25	0.92	1.84	3.32	2.76
MCM 25%: ZSM 75%	1.83	16.28	1.38	13.40	0.64	16.87	5.74	14.28	19.73	1.21	2.57	3.47	2.60

A closer inspection for the changes in the chemical group peak area respective to the non-catalytic run can be found in Table 8-8. It is ideal to compare them collectively, rather than from individual chemicals.

Table 8-8. Changes in the peak area for chemical groups for the optimisation runs respective to the non-catalytic run

	ARH	OA	EST	FUR	ALD	KET	ALC	PHE	GU	SYR	ANH	MISC	NCC
ZSM 75%: MCM 25%	0.08	-1.80	0.04	-0.35	0.14	-0.31	-1.29	-0.46	3.26	0.16	-1.06	0.83	0.77
ZSM 50%: MCM 50%	1.23	-1.88	0.34	0.36	0.15	-0.82	-1.27	2.23	-0.81	-0.11	-0.72	1.09	0.21
ZSM 25%: MCM 75%	-0.40	-1.30	-0.17	-1.38	0.01	-0.64	-1.40	-0.26	5.57	0.26	-1.27	0.66	0.32
Mixtures	0.36	1.71	0.22	0.22	0.04	0.09	-1.06	-0.96	0.22	-0.38	-1.70	0.28	0.94
MCM 75%: ZSM 25%	0.56	1.48	0.41	0.64	0.15	-0.53	-1.46	-0.48	0.19	-0.37	-1.78	0.28	0.90
MCM 50%: ZSM 50%	0.89	2.05	0.52	1.13	0.07	-0.19	-1.31	0.26	-1.82	-0.57	-2.02	0.30	0.69
MCM 25%: ZSM 75%	0.49	-0.73	0.24	1.17	0.00	-0.23	-1.40	0.39	0.66	-0.28	-1.29	0.45	0.53

A comparison of the catalyst combination in series and physically-mixed catalyst in equal ratio (50%:50%) with respect to their chemical groups can be found in Figure 8-17. An overall sense can be deduced that the catalyst positioned in-series with ZSM-5 as a primary catalyst is the most favourable amongst the other two configuration, as it increases the aromatic hydrocarbon and phenols and reducing the organic acids the most. Al-MCM-41 as a primary catalyst loses its ability to reduce the organic acids as compared to being a secondary catalyst. The organic acid peak area for the Al-MCM-41 as a primary catalyst was almost similar to the physically-mixed catalyst. The physically-mixed catalyst can be seen to increase the amount of guaiacols and ketones. The overall effectiveness of catalyst can be concluded that the ZSM-5 primary > Al-MCM-41 primary > Physically-mixed catalyst.

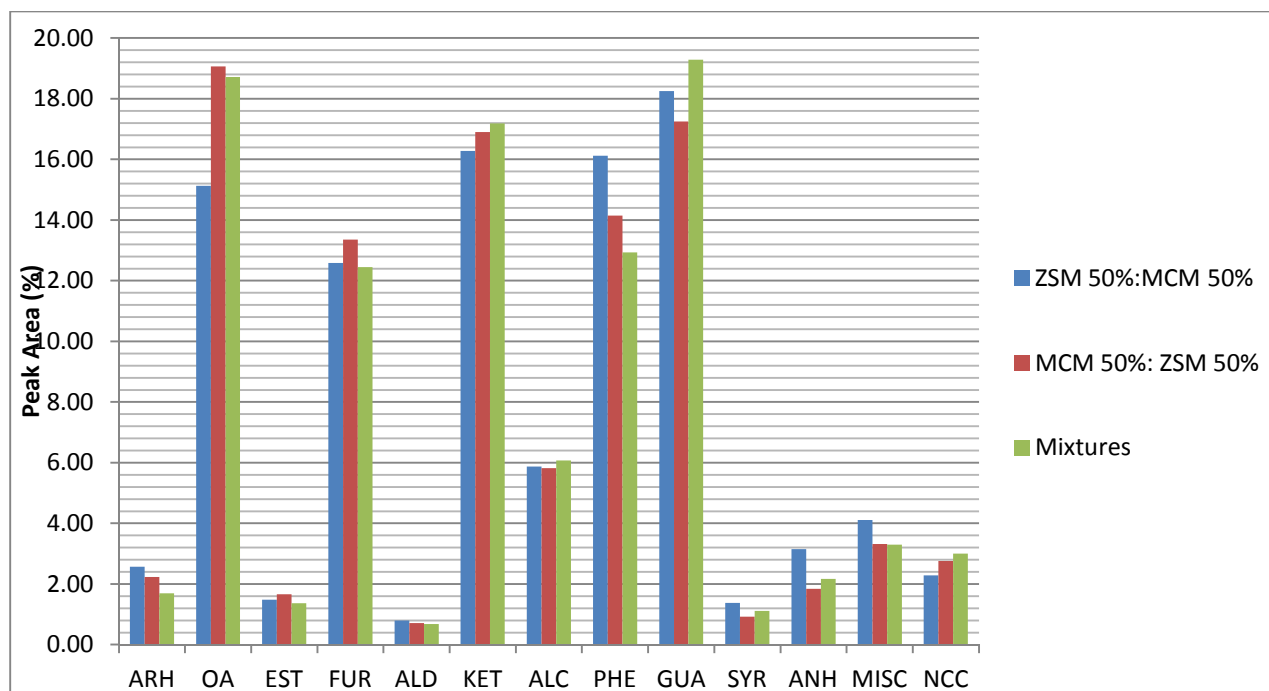


Figure 8-17. Total peak areas for the various chemical groups for the equal combination catalyst ratio

8.4 Evaluation procedures

The criteria proposed were similar to Chapter 7 and is listed below. The criteria were to evaluate which of the optimisation catalytic run was the most effective and indirectly determine a better catalyst guard bed. The leading optimisation run essentially would mean that the catalytic functions during the upgrading of the pyrolysis vapours are intact, and does not lose its ability to function.

1. Increase in aromatic hydrocarbon
2. Reduction in the organic acid
3. Increase in phenols
4. Increase in pH (lower acidity)
5. Increase in the HHV
6. Lower water content
7. Lower viscosity
8. Lower density
9. High HC molar ratio
10. Low OC molar ratio

Table 8-9. Evaluation of the best catalyst optimisation run from the various proposed criteria

Catalyst optimisation run	Criteria									
	1	2	3	4	5	6	7	8	9	10
ZSM 25%: MCM 75%		X				X				X
ZSM 50%: MCM 50%	X	X	X	X	X		X	X	X	
ZSM 75%: MCM 25%		X			X	X				X
Mixtures					X				X	
MCM 25%:ZSM 75%			X	X			X		X	
MCM 50%: ZSM 50%	X		X	X		X	X	X		
MCM 75%: ZSM 25%	X						X	X		X

Based on the evaluation criteria in Table 8-9, the best catalyst ratio was found for ZSM 50%: MCM 50%. ZSM-5 as a primary catalyst and catalytic guard bed was better as compared to Al-MCM-41 due to the ability to maintain ZSM-5 for the production of aromatic hydrocarbon and phenols, and protecting the function of Al-MCM-41 for organic acid reduction. The second best was for the similar ratio of 50%, but Al-MCM-41 as the primary catalyst. It may well be that it reduces the density of the bio-oil the most, but catalytic functions such as the crucial reduction in the organic acid were impeded, together with other criteria such as increasing the HHV and the H: C molar ratio.

The primary catalyst was prone to catalyst deactivation through coking on the catalyst surface compared to the secondary catalyst. This was proven from the reduction in the respective catalytic functions. However, these catalysts may be regenerated via combustion of the coke, as proven from Chapter 7 for ZSM-5 and Al-MCM-41. The evaluation concluded that the synergy of the catalysts has a positive effect when the catalysts are of a similar ratio. The physically-mixed catalyst is considered the least effective amongst the optimisation run.

8.5 Summary

The catalytic optimisation experiments showed that the combination of both catalysts ZSM-5 and Al-MCM-41 in different ratios and position demonstrated a difference in the upgrading qualities. Catalysts which are positioned as a primary catalyst and having a lower ratio tends to deactivate faster through coking. The synergies between catalysts with 25% ratio content were not favourable for most cases. We can conclude that the ratios and positioning between both catalysts are a critical key factor. From the evaluation procedures, it is found that the superior catalyst combination was using ZSM-5 as a primary catalyst and Al-MCM-

41 as the secondary catalyst with a ratio of 50% (ZSM 50%: MCM 50%). The effective catalyst optimisation runs may be arranged in the order of ZSM 50%: MCM 50% > MCM 50%: ZSM 50% > ZSM 75%: MCM 25%; MCM 25%: ZSM 75%; MCM 75%: ZSM 25% > ZSM 25%: MCM 75% > Mixtures.

9 CONCLUSION AND RECOMMENDATION

9.1 Conclusion

Rice Husks from Brunei (BRH) was used as a feedstock for bio-oil production by non-catalytic and catalytic intermediate pyrolysis experiments. BRH was compared in terms of biomass characterisation with another species of rice husk from West Africa (AFRH). Both of the rice husks show a high ash content and comparable to other rice husk species from other regions.

The pyrolysis of dry and wet-BRH was carried out in a bench-scale pyrolysis rig with a 100g capacity. Dry-BRH pyrolysis produced bio-oil with a single layer and wet-BRH bio-oil was shown to separate into two distinct layers of the organic and aqueous phase. Both phases of the wet BRH bio-oil and the single phase dry-BRH were characterised. Although the separation wet-BRH achieved a desirable quality in terms of acidity reduction, dry-BRH pyrolysis bio-oil was chosen due to the homogeneity and the available quantity for the essential characterisation procedures. The bio-oil was found to contain high water content, Analysis from GC-MS found that majority of the chemical groups in the bio-oil contained organic acids, furans, ketones, phenols and guaiacols.

The introduction of catalyst into the system upgraded the rice husk bio-oil. Although the catalyst-to-biomass ratio was low of about 1:100, the catalysts employed in these experiments were able to upgrade the bio-oil to some extent from the changes detected in the properties of the pyrolysis bio-oil, especially from the GC-MS analysis. ZSM-5, Al-MCM-41, Al-MSU-F and BRHA, collectively with their combinations show various changes towards the bio-oil characterisation results. The regenerated catalysts lost some of the initial catalytic properties, but still retain its catalytic ability. The combination of ZSM-5 and Al-MCM-41 catalyst in series was the favourable which met most of the criteria from the evaluation procedures. The combinations of both the catalysts lead to a positive synergy in which the functions of both of the individual catalysts are preserved, i.e. ZSM-5 for increasing the aromatics and phenols, and Al-MCM-41 for decreasing the organic acids content.

The optimisation of the process was the next step, by altering the ratio and position of ZSM-5 and Al-MCM-41. Results showed that the combination of both catalysts ZSM-5 and Al-MCM-41 in different ratios and position demonstrated a difference in the upgrading qualities and established the ratios and positioning between both catalysts are a significant key factor. Catalysts which are positioned as a primary catalyst and having a lower ratio tends to

deactivate faster through coking. The synergies between catalysts with 25% ratio content were not favourable in most cases. From the evaluation procedures, it is found that the superior catalyst combination was using ZSM-5 as a primary catalyst and Al-MCM-41 as the secondary catalyst with both with a ratio of 50%. The effective catalyst optimisation runs may be arranged in the order of ZSM 50%: MCM 50% > MCM 50%: ZSM 50% > ZSM 75%: MCM 25%; MCM 25%: ZSM 75%; MCM 75%: ZSM 25% > ZSM 25%: MCM 75% > Mixtures.

Studies in literature focus mainly towards the fast pyrolysis of rice husk but not for intermediate pyrolysis. The utilisation of rice husks from Brunei, particularly for bio-oil production has never been done before. Characterisation of the BRH leads to the suitability of the feedstock for biofuel generation, particularly towards bio-oil from pyrolysis. This could be proven useful for Brunei, in terms of diversifying the economy away from fossil fuels.

The uniqueness of this research lies from the combination of both catalysts ZSM-5 and Al-MCM-41, and altering their ratios. Both of these existing commercial zeolite catalysts have been used extensively, but not combined in any form as of yet for bio-oil upgrading. This study also hope to further increase the influx of research on the usage of catalysts combination which has the property of 'either/or' scenarios, such as using ZSM-5 which increases the hydrocarbon and phenols, and Al-MCM-41 which decreases the organic acids.

9.2 Recommendation

In the current catalytic pyrolysis setup, problems were encountered by increasing the purge gas flow rate more than 50 cm³/min, such as the build-up of pressure in the system during the pyrolysis at maximum temperature (450 °C). This could lead to a leakage in the primary reactor especially the joint between the quartz tube and the reactor head, which would disrupt the experiment. Therefore it is recommended in future experiments, a steel reactor may be used, or a bigger bore diameter for the secondary reactor. The current secondary reactor furnace only allows a maximum of 30 mm external diameter size tube.

Another possible study is the extent of coking, which was not able to be measured, i.e. the time when the catalysts are deactivated. This has been known to affect the composition of the gases, especially the difference in the amount before and after catalyst deactivation. An online continuous gas chromatograph will be useful in this case to know the concentration of gases.

The catalyst to biomass ratio was about 1:100 in this study. For future study, the catalyst amount may be increased. In this study, the amount of feed used is about 100g, which generated about 40g of bio-oil. The restriction is that if we reduce the feed amount to counter the catalyst to biomass ratio, there will not be ample bio-oil collected from this reactor for analysis requiring a larger amount such as viscosity and density. Adding a guard bed (e.g. dolomite) before the catalysts may also help to prolong the life of the zeolite catalysts.

Other pyrolysis by-products, i.e. the bio-char and the non-condensable gases may be investigated thoroughly to get a general idea of the pyrolysis process as a whole. But the limitation to this study is aimed at mainly to investigate the upgrading ability of the catalysts for the production of bio-oil.

As the bench-scale research has been proven successful, the utilisation of the rice husks on a pilot scale investigation using the pyroformer is considered for future work. This will require a large amount of rice husks shipped from Brunei, since the pyroformer has a maximum throughput of 20kg/hr. A catalytic reactor bed with the appropriate capacity for upgrading will also need to be designed and coupled to the pyroformer.

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APPENDIX A – LIST OF PUBLICATIONS

Publication made during the course of this study is listed below.

1. M.S. Abu Bakar, J.O. Titiloye. Thermochemical properties of Brunei rice husks and suitability for thermal conversion via pyrolysis process. *Brunei Darussalam Journal of Technology and Commerce*, 6 (2012).
2. M.S. Abu Bakar, J.O. Titiloye. Catalytic pyrolysis of rice husks for bio-oil production. *Journal of Analytical and Applied Pyrolysis* 103 (2013), p. 362-368.
<http://dx.doi.org/10.1016/j.jaap.2012.09.005>
3. M.S. Abu Bakar, J.O. Titiloye, T.E. Odetoeye. Catalytic pyrolysis of rice husk, jatropha curcas and parinari polyandra with ZSM-5. *Sustainable Future Energy 2012 and 10th SEE Forum*, Bandar Seri Begawan, Brunei Darussalam, 2012: A-28.
4. T.E Odetoeye, K.R. Onifade, M.S. Abu Bakar, J.O. Titiloye. Thermochemical characterisation of Parinari polyandra Benth fruit shell. *Industrial Crops and Products*, 44 (2013), p. 62-66.
5. J.O. Titiloye, M.S. Abu Bakar, T.E. Odetoeye. Thermochemical characterisation of Agricultural Wastes from West Africa. *Industrial Crops and Products*, 47 (2013), p. 199-203.
6. T.E Odetoeye, K.R. Onifade, M.S. Abu Bakar, J.O. Titiloye. Pyrolysis of Parinari polyandra Benth fruit shell for bio-oil production (In progress)

APPENDIX B – EXPERIMENTAL SET-UP SPECIFICATIONS

Experimental set-up	Specifications
Primary reactor furnace	Vertical Carbolite® wire heated tube furnace 1200 °C Maximum power of 3000 W 3 phase or universal power supply
Primary reactor head	Borosilicate glass tube head cover with 3 sockets for: a) Custom-made metal 24/29 Male stopper with thermocouple insert b) Purge gas entry – 150 mm glass tube with 9 mm neck c) Socket – Female 19/26 open end
Primary reactor tube	390 mm Quartz glass tube with internal diameter of 60 mm
Transition tube 1	15 cm Borosilicate glass tube Both 19/24 Male open ends
Adaptor to secondary reactor	19/24 Female to 24/29 Male both open end
Secondary reactor furnace	Horizontal Vectstar® tube furnace 1100 °C 3 phase or universal power supply
Secondary reactor tube	390 mm Quartz glass tube Both 24/29 Female open ends
Connector tube	10 cm borosilicate glass tube Both 24/29 Male open ends
Condenser 1	Dry-ice condenser/Cold-finger condenser 500 ml 24/29 female end for both top-left and middle-bottom socket
Oil pot connector 1	T-shaped borosilicate glass tube with female 24/29 and male 24/29 open ends, and 19/24 female neck
Oil pot tube 1	10 cm borosilicate glass tube Both 24/29 Male open ends
Oil pot 1	500 ml round bottom flask with 24/29 female socket
Condenser 2	Cold-trap type condenser 19/24 male and female connector ends
Oil pot 2	34/35 female glass tube
Isopropanol trap	Cold-trap type condenser 19/24 male and female connector ends
Tube to vent	Tygon® tubing

Other essential items	Additional information
Quartz glass wool	Preventing catalyst monolith from moving
Condensation medium	Mixture of dry-ice and acetone (approx. -70 °C)
Insulation	High-temperature glass wool insulation
Flowmeter	0-500 cm ³ /min range
Metal/Plastic tube clips	Hold connected joints
Thermocouples (x2)	Thermocouple K-type stainless steel (1.5 mm x 1.0 m)
Temperature indicator	Hand-held (for measuring the secondary furnace temperature)
Purge/sweeping gas	Nitrogen gas (99.9% purity)
Silica paste	Applied between joints so that during high temperature, glass will not 'lock' with each other and provide a good seal

APPENDIX C – MASS BALANCE SHEET

Run:	Feed	1	2	3
Date:	Moisture Content			
Sample:	Ash Content			

Pyrolysis rig				
Component	Weight before (g)	Weight after (g)	Difference	Nature
Feedstock				Feed
Primary reactor head				Char
Primary reactor tube				Char
Transition tube 1				Liquid
Adaptor to secondary reactor				Liquid
Secondary reactor tube				Char
Catalyst				Char
Quartz wool				Char
Transition tube 2				Liquid
Dry ice condenser 1				Liquid
Oil pot connector 1				Liquid
Oil pot tube 1				Liquid
Oil pot 1				Liquid
Dry ice condenser 2				Liquid
Oil pot 2				
Isopropanol system				Liquid
Isopropanol				Liquid
Liquids collected				
Char collected				
Gas (by difference)				
Yields	Weight (g)	Weight (%)		
Total Liquid			Closure (%)	
Char				
Gas (by difference)				
Liquids recovered	Weight (g)	Weight (%)		
Aqueous phase (Top)				
Oil phase (Bottom)				

Notes:

TIME (min)	CARBOLITE REACTOR TEMPERATURE (°C)	CATALYST BED TEMPERATURE (°C)
0		
5		
10		
15		
20		
25		
30		
		AVERAGE =